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50.54(f) NTTF 2.1 Seismic High Frequency Confirmation for WCGS

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EXECUTIVE SUMMARY

The purpose of this report is to provide information as requested by the Nuclear Regulatory Commission (NRC) in its March 12, 2012 letter issued to all power reactor licensees and holders of construction permits in active or deferred status [1]. In particular, this report provides information requested to address the High Frequency Confirmation requirements of Item (4), Enclosure 1, Recommendation 2.1: Seismic, of the March 12, 2012 letter [1].

Following the accident at the Fukushima Dai-ichi nuclear power plant resulting from the March 11, 2011, Great Tohoku Earthquake and subsequent tsunami, the Nuclear Regulatory Commission (NRC) established a Near Term Task Force (NTTF) to conduct a systematic review of NRC processes and regulations and to determine if the agency should make additional improvements to its regulatory system. The NTTF developed a set of recommendations intended to clarify and strengthen the regulatory framework for protection against natural phenomena [2]. Subsequently, the NRC issued a 50.54(f) letter on March 12, 2012 [1], requesting information to assure that these recommendations are addressed by all U.S. nuclear power plants. The 50.54(f) letter requests that licensees and holders of construction permits under 10 CFR Part 50 reevaluate the seismic hazards at their sites against present-day NRC requirements and guidance. Included in the 50.54(f) letter was a request that licensees perform a "confirmation, if necessary, that SSCs, which may be affected by high-frequency ground motion, will maintain their functions important to safety."

EPRI 1025287, "Seismic Evaluation Guidance: Screening, Prioritization and Implementation Details (SPID) for the resolution of Fukushima Near-Term Task Force Recommendation 2.1: Seismic" [3] provided screening, prioritization, and implementation details to the U.S. nuclear utility industry for responding to the NRC 50.54(f) letter. This report was developed with NRC participation and was subsequently endorsed by the NRC. The SPID included guidance for determining which plants should perform a High Frequency Confirmation and identified the types of components that should be evaluated in the evaluation.

Subsequent guidance for performing a High Frequency Confirmation was provided in EPRI 3002004396, "High Frequency Program, Application Guidance for Functional Confirmation and Fragility Evaluation," [4] and was endorsed by the NRC in a letter dated September 17, 2015 [5]. Final screening identifying plants needing to perform a High Frequency Confirmation was provided by NRC in a letter dated October 27, 2015 [6].

This report describes the High Frequency Confirmation evaluation undertaken for Wolf Creek Generating Station (WCGS). The objective of this report is to provide summary information describing the High Frequency Confirmation evaluations and results. The level of detail provided in the report is intended to enable NRC to understand the inputs used, the evaluations performed, and the decisions made as a result of the evaluations.

EPRI 3002004396 [4] is used for the Wolf Creek Generating Station engineering evaluations described in this report. In accordance with Reference [4], the following topics are addressed in the subsequent sections of this report:

- Process of selecting components and a list of specific components for high-frequency confirmation
- Estimation of a vertical ground motion response spectrum (GMRS)
- Estimation of in-cabinet seismic demand for subject components
- Estimation of in-cabinet seismic capacity for subject components
- Summary of subject components' high-frequency evaluations

1 INTRODUCTION

1.1 Purpose

The purpose of this report is to provide information as requested by the NRC in its March 12, 2012 50.54(f) letter issued to all power reactor licensees and holders of construction permits in active or deferred status [1]. In particular, this report provides requested information to address the High Frequency Confirmation requirements of Item (4), Enclosure 1, Recommendation 2.1: Seismic, of the March 12, 2012 letter [1].

1.2 Background

Following the accident at the Fukushima Dai-ichi nuclear power plant resulting from the March 11, 2011, Great Tohoku Earthquake and subsequent tsunami, the Nuclear Regulatory Commission (NRC) established a Near Term Task Force (NTTF) to conduct a systematic review of NRC processes and regulations and to determine if the agency should make additional improvements to its regulatory system. The NTTF developed a set of recommendations intended to clarify and strengthen the regulatory framework for protection against natural phenomena [2]. Subsequently, the NRC issued a 50.54(f) letter on March 12, 2012 [1], requesting information to assure that these recommendations are addressed by all U.S. nuclear power plants. The 50.54(f) letter requests that licensees and holders of construction permits under 10 CFR Part 50 reevaluate the seismic hazards at their sites against present-day NRC requirements and guidance. Included in the 50.54(f) letter was a request that licensees perform a "confirmation, if necessary, that SSCs, which may be affected by high-frequency ground motion, will maintain their functions important to safety."

EPRI 1025287, "Seismic Evaluation Guidance: Screening, Prioritization and Implementation Details (SPID) for the resolution of Fukushima Near-Term Task Force Recommendation 2.1: Seismic" [3] provided screening, prioritization, and implementation details to the U.S. nuclear utility industry for responding to the NRC 50.54(f) letter. This report was developed with NRC participation and is endorsed by the NRC. The SPID included guidance for determining which plants should perform a High Frequency Confirmation and identified the types of components that should be evaluated in the evaluation.

Subsequent guidance for performing a High Frequency Confirmation was provided in EPRI 3002004396, "High Frequency Program, Application Guidance for Functional Confirmation and Fragility Evaluation," [4] and was endorsed by the NRC in a letter dated September 17, 2015 [5]. Final screening identifying plants needing to perform a High Frequency Confirmation was provided by NRC in a letter dated October 27, 2015 [6].

On March 31, 2014, Wolf Creek Generating Station submitted a reevaluated seismic hazard to the NRC as a part of the Seismic Hazard and Screening Report [7]. By letter dated October 27, 2015 [6], the NRC transmitted the results of the screening and prioritization review of the seismic hazards reevaluation.

This report describes the High Frequency Confirmation evaluation undertaken for Wolf Creek Generating Station using the methodologies in EPRI 3002004396, "High Frequency Program,

Application Guidance for Functional Confirmation and Fragility Evaluation," as endorsed by the NRC in a letter dated September 17, 2015 [5].

The objective of this report is to provide summary information describing the High Frequency Confirmation evaluations and results. The level of detail provided in the report is intended to enable NRC to understand the inputs used, the evaluations performed, and the decisions made as a result of the evaluations.

1.3 Approach

EPRI 3002004396 [4] is used for the Wolf Creek Generating Station engineering evaluations described in this report. Section 4.1 of Reference [4] provided general steps to follow for the high frequency confirmation component evaluation. Accordingly, the following topics are addressed in the subsequent sections of this report:

- WCGS's SSE and GMRS Information
- Selection of components and a list of specific components for high-frequency confirmation
- Estimation of seismic demand for subject components
- Estimation of seismic capacity for subject components
- Summary of subject components' high-frequency evaluations
- Summary of Results

1.4 Plant Screening

Wolf Creek Generating Station submitted reevaluated seismic hazard information including GMRS and seismic hazard information to the NRC on March 31, 2014 [7]. In a letter dated August 12, 2015, the NRC staff concluded that the submitted GMRS adequately characterizes the reevaluated seismic hazard for the Wolf Creek Generating Station [8].

The NRC final screening determination letter [6] concluded that the Wolf Creek Generating Station GMRS to SSE comparison resulted in a need to perform a High Frequency Confirmation in accordance with the screening criteria in the SPID [3].

2 SELECTION OF COMPONENTS FOR HIGH-FREQUENCY SCREENING

The fundamental objective of the high frequency confirmation review is to determine whether the occurrence of a seismic event could cause credited equipment to fail to perform as necessary. An optimized evaluation process is applied that focuses on achieving a safe and stable plant state following a seismic event. As described in Reference [4], this state is achieved by confirming that key plant safety functions critical to immediate plant safety are preserved (reactor trip, reactor vessel inventory and pressure control, and core cooling) and that the plant operators have the necessary power available to achieve and maintain this state immediately following the seismic event (AC/DC power support systems).

Within the applicable functions, the components that would need a high frequency confirmation are contact control devices subject to intermittent states in seal-in or lockout (SILO) circuits. Accordingly, the objective of the review as stated in Section 4.2.1 of Reference [4] is to determine if seismic induced high frequency relay chatter would prevent the completion of the key functions listed in the subsequent subsections.*

Due to relevant contact device mapping as part of the recent WCGS Seismic Probabilistic Risk Assessment (SPRA), all devices controlling the equipment and components covered by the high frequency program were selected using the device/component dependency matrix (table) in the SPRA Relay Database contained in calculation 13C4152-CAL-009 [9]. This method produces a superset of contact devices containing both those devices covered by the high frequency program, and those devices which would screen out functionally from the program because they are not SILO candidates. This is a conservative approach to the device list.

2.1 Reactor Trip/SCRAM

The reactor trip/SCRAM function is identified as a key function in Reference [4] to be considered in the High Frequency Confirmation. The same report also states that, "the design requirements preclude the application of seal-in or lockout circuits that prevent reactor trip/SCRAM functions" and that "No high-frequency review of the reactor trip/SCRAM systems is necessary."

2.2 Reactor Vessel Inventory Control

The concern for this category of the EPRI 3002004396 [4] program is the actuation of valves that have the potential to cause a loss-of-coolant accident (LOCA). A LOCA following a seismic event could provide a challenge to the mitigation strategies and lead to core damage. The contact devices identified in the SPRA Relay Database from Reference [9] as controlling the Pressurizer Power Operated Relief Valves (PORVs) as well as other *included*[†] Reactor Coolant System (RCS) valves in Table 2-1 were selected for high frequency program screening.

^{*} The selection of components for high frequency screening was performed by report 16C4405-RPT-001 [12] and is summarized herein.

[†] Unless otherwise noted, these are the valves tagged as either "Yes" or "Potentially" in the "To be Evaluated" field.

Selection of Valves

The process and criteria for assessing potential reactor coolant leak-path valves is to review all P&IDs attached to the Reactor Coolant System (RCS) and include all active[‡] isolation valves and any active second valve upstream or downstream that is assumed to be required to be closed during normal operation or close upon an initiating event (LOCA or Seismic). Manual valves that are normally closed are assumed to remain closed and a second simple check valve[§] is assumed to function and not be a Multiple Spurious Failure. Instrument lines that are 1 inch in diameter or less are presumed to have restricting orifices that are designed to mitigate any leakage due to make up, and thus are not analyzed.

| Table | Table 2-1: Potential Reactor Coolant Leak Path Valves | | | | |
|------------|---|---|--|--|--|
| Component | Description | Comment | | | |
| BB8010A | Pressurizer Safety Relief Valve | | | | |
| BB8010B | Pressurizer Safety Relief Valve | | | | |
| BB8010C | Pressurizer Safety Relief Valve | | | | |
| BBHV8000A | PORV Block Valve | | | | |
| BBHV8000B | PORV Block Valve | | | | |
| BBHV8032 | Reactor Vessel Flange Leakoff Valve | HV Valve | | | |
| BBPCV0455A | Pressurizer Power Operated Relief Valve | Normally would only be a potential Leak Path HV8000A fails to be closed | | | |
| BBPCV0456A | Pressurizer Power Operated Relief Valve | Normally would only be a potential Leak Path HV8000B fails to be closed | | | |
| BBPV8702A | RCS Hot Leg 1 to RHR Pump A Suction | PV Valve | | | |
| BBPV8702B | RCS Hot Leg 4 to RHR Pump B Suction | PV Valve | | | |
| BGHV8153A | Excess Letdown Isolation | Potentially Normally would only be a potential Leak Path HV8154A fails to be closed | | | |
| BGHV8153B | Excess Letdown Isolation | Potentially Normally would only be a potential Leak Path HV8153A fails to be closed | | | |
| BGHV8154A | Excess Letdown Isolation | | | | |
| BGHV8154B | Excess Letdown Isolation - D Loop | | | | |
| BGLCV0459 | RCS Letdown to Regenerative Heat Exchanger | Normally would only be a potential Leak Path LCV0460 fails to be closed | | | |

[‡] Active: A component in which mechanical movement or change of state must occur to accomplish the function of the component.

[§] Simple Check Valve: A valve which closes upon reverse fluid flow only.

| Table 2-1: Potential Reactor Coolant Leak Path Valves | | | | |
|---|--|--|--|--|
| Component | Description | Comment | | |
| BGLCV0460 | RCS Letdown to Regenerative Heat Exchanger | | | |
| EJHV8701A | RCS Hot Leg 1 to RHR Pump A Suction | Normally would only be a potential Leak Path if PV8702A fails to be closed | | |
| EJHV8701B | RCS Hot Leg 4 to RHR Pump B Suction | Normally would only be a potential Leak Path if PV8702B fails to be closed | | |
| SJHV0005 | RCS Liquid Sample Inner Containment Isolation Valve | Normally would only be a potential Leak Path if HV0006 and HV0027 fails to be closed | | |
| SJHV0006 | RCS Liquid Sample Outer Containment Isolation Valve | | | |
| SJHV0127 | RCS Liquid Sample Outer Containment Isolation Bypass Valve | This is a Normally closed Valve | | |
| SJHV0128 | Pressurizer/RCS Liquid Sample Inner Containment Isolation Valve | Normally would only be a potential Leak Path if HV0129 and HV0130 fails to be closed | | |
| SJHV0129 | Pressurizer/RCS Liquid Sample Outer Containment Isolation Valve | This is a Normally closed Valve | | |
| SJHV0130 | Pressurizer/RCS Liquid Sample Outer Containment Isolation Bypass Valve | This is a Normally closed Valve | | |

2.3 Reactor Vessel Pressure Control

The reactor vessel pressure control function is identified as a key function in Reference [4] to be considered in the High Frequency Confirmation. The same report also states that "required post event pressure control is typically provided by passive devices" and that "no specific high frequency component chatter review is required for this function."

2.4 Core Cooling

EPRI 3002004396 [4] requires confirmation that one train of AC-independent cooling is not challenged by a SILO device. The steam turbine-driven auxiliary feedwater (TDAFW) pump was the train chosen for this analysis. TDAFW pump PAL02 is controlled indirectly via valves in the steam supply lines feeding the turbine, and thus the selection of components for core cooling is limited to the valves associated with the turbine steam supply, pump suction, and pump discharge. Table 2-2 is the list of valves associated with the TDAFW system. The contact devices identified in the SPRA Relay Database from Reference [9] as controlling these valves were selected for high frequency program screening.

| | Table 2-2: Core Cooling Components | | | | | |
|-----------|--|--|--|--|--|--|
| Component | Description | Function | | | | |
| ABHV0005 | Main Steam Loop 2 to TDAFW Pump | Valve needs to open to provide steam to turbine | | | | |
| ABHV0006 | Main Steam Loop 3 to TDAFW Pump | Valve needs to open to provide steam to turbine | | | | |
| ABPV0001 | Steam Generator A Atmospheric Relief Valve | Valve needs to remain open (throttled) to discharge steam | | | | |
| ABPV0002 | Steam Generator B Atmospheric Relief Valve | Valve needs to remain open (throttled) to discharge steam | | | | |
| ABPV0003 | Steam Generator C Atmospheric Relief Valve | Valve needs to remain open (throttled) to discharge steam | | | | |
| ABPV0004 | Steam Generator D Atmospheric Relief Valve | Valve needs to remain open (throttled) to discharge steam | | | | |
| ALHV0006 | TDAFW Pump Discharge to Steam Generator D | Valve needs to remain open (throttled) to maintain pump discharge to SG | | | | |
| ALHV0008 | TDAFW Pump Discharge to Steam Generator A | Valve needs to remain open (throttled) to maintain pump discharge to SG | | | | |
| ALHV0010 | TDAFW Pump Discharge to Steam Generator B | Valve needs to remain open (throttled) to maintain pump discharge to SG | | | | |
| ALHV0012 | TDAFW Pump Discharge to Steam Generator C | Valve needs to remain open (throttled) to maintain pump discharge to SG | | | | |
| ALHV0036 | Condensate Storage to TDAFW Pump 10" Gate Valve | Valve needs to remain open to maintain pump suction from CST | | | | |
| FCFV0313 | TDAFW Pump Turbine Speed Governing Valve | Valve needs to regulate steam flow to turbine | | | | |
| FCHV0312 | TDAFW Pump Turbine Mechanical Trip/Throttle Valve | Valve needs to remain open and un- tripped to provide steam to turbine | | | | |

2.5 AC/DC Power Support Systems

The AC and DC power support systems were reviewed for contact control devices in seal-in and lockout circuits that prevent the availability of DC and AC power sources. The following AC and DC power support systems were reviewed:

- Emergency Diesel Generators,
- Battery Chargers and Inverters,
- Diesel Generator Ancillary Systems, and
- Switchgear, Load Centers, and MCCs.

Electrical power, especially DC, is necessary to support achieving and maintaining a stable plant condition following a seismic event. DC power relies on the availability of AC power to recharge the batteries. The availability of AC power is dependent upon the Diesel Generators (DGs) and their ancillary support systems. EPRI 3002004396 [4] requires confirmation that the supply of emergency power is not challenged by a SILO device. The tripping of lockout devices or circuit breakers is expected to require some level of diagnosis to determine if the trip was spurious due to contact chatter or in response to an actual system fault. The actions taken to diagnose the fault condition could substantially delay the restoration of emergency power.

To ensure contact chatter cannot compromise the emergency power system, contact control devices identified in the SPRA Relay Database from Reference [9] as controlling the DGs, Battery Chargers, Vital AC Inverters, and Switchgear/Load Centers/MCCs as necessary to distribute power from the DGs to the Battery Chargers and EDG Ancillary Systems were selected for high frequency program screening. Wolf Creek has two (2) DGs which provide emergency power for their two (2) divisions of Class 1E loads, with one DG for each division [10, pp. 8.3-5, 8.3-10]. Four (4) battery chargers provide DC power and battery recharging functions [10, pp. 8.3-37]. These components are listed in Table 2-3.

In response to bus under-voltage relaying detecting the LOOP, the Class 1E control systems must automatically shed loads, start the DGs, and sequentially load the diesel generators as designed. Ancillary systems required for DG operation as well as Class 1E battery chargers and inverters must function as necessary. The goal of this analysis is to identify any vulnerable contact devices that could chatter during the seismic event, seal-in or lock-out, and prevent these systems from performing their intended safety-related function of supplying electrical power during the LOOP.

Diesel Generators

The contact devices identified in the SPRA Relay Database from Reference [9] as controlling the diesel engine as well as protective relaying for the generator and its output circuit breaker were selected for high frequency program screening.

Battery Chargers

The protective relaying identified in the SPRA Relay Database from Reference [9] as controlling the low-voltage AC circuit breakers supplying 480V AC power to the battery chargers, as well as the breakers themselves, were selected for high frequency program screening. Analysis of schematics for the battery chargers revealed no SILO contact devices and thus no contact devices controlling the chargers themselves are selected for analysis.

Inverters

Analysis of schematics for the inverters revealed no SILO contact devices and thus no contact devices controlling the inverters are selected for analysis.

DG Ancillary Systems

The Diesel Generators require several components and systems to start and operate. When identifying electrical contact devices, only systems and components which are electrically controlled are analyzed.

Starting Air

Based on Diesel Generator availability as an initial condition the passive air reservoirs are presumed pressurized and the only active components in this system required to operate are the air start solenoids, which are covered under the DG engine control analysis above.

Combustion Air Intake and Exhaust

The combustion air intake and exhaust for the Diesel Generators are passive systems, which do not rely on electrical control.

Lube Oil

The Diesel Generators utilize engine-driven mechanical lubrication oil pumps which do not rely on electrical control.

Fuel Oil

The Diesel Generators utilize engine-driven mechanical pumps and DC-powered booster pumps to supply fuel oil to the engines from the day tanks. The day tanks are re-supplied using AC-powered Diesel Oil Transfer Pumps which are identified in Table 2-3. Relaying identified in the SPRA Relay Database from Reference [9] as controlling the transfer pumps have been selected for evaluation.

Cooling Water

The Diesel Generator Cooling Water System consists of three cooling loops, jacket water, intercooler, and Essential Service Water (ESW). Engine driven pumps are credited for the jacket water and intercooler when the engine is operating. These mechanical pumps do not rely on electrical control. The ESW pumps, valves, screens, and strainers required to provide cooling water to the diesel generator heat exchangers are indicated in Table 2-3. The contact devices identified in the SPRA Relay Database from Reference [9] as controlling these components were selected for high frequency program screening.

Ventilation

The fans and dampers necessary to provide ventilation to the Diesel Generator Building are indicated in Table 2-3. The contact devices identified in the SPRA Relay Database from Reference [9] as controlling these components were selected for high frequency program screening.

Switchgear, Load Centers, and MCCs

Power distribution from the DGs to the necessary electrical loads (Battery Chargers, Inverters, ESW components, Fuel Oil Pumps, and DG Ventilation Fans) was traced to identify power distribution components and their associated protective relaying included in this analysis.

The main (152NB00112, 152NB00212) and alternate (152NB00109, 152NB00209) power feed circuit breakers for the class 1E 4160V AC switchgear are not included in this analysis as the diesel generator is the preferred source of electrical power since offsite power cannot be assured following the seismic event. Based on initial conditions prior to the seismic event, normal power is being fed to these busses, which means 152NB00112 and 152NB00212 are closed, and 152NB00109 and 152NB00209 are tripped. Contact devices in the undervoltage and load shed circuits are included in the selection due to the dependence of the diesel generator breaker on these function. Evaluation of these contact devices ensures that proper signaling to these breakers is not compromised in the selexit event. Auxiliary contacts from these breakers are permissives to close the diesel generator breakers 152NB00111 and 152NB0021. Chatter in the auxiliary contacts of 152NB00112, 152NB00212, 152NB00109, or 152NB00209 may delay

closure of the diesel generator circuit breaker, however breaker closure capability would be restored once strong shaking subsides. Improper DG loading due to a double failure of the main feed breaker to trip while falsely indicating (via its auxiliary contacts) it has tripped is not considered in this analysis due to the unlikely nature of this specific chain of events. The main and auxiliary feed breaker closing circuits are controlled by hand switches only. These normally-open rugged hand switches prevent spurious breaker closure. Based on this analysis, circuit breakers 152NB00112, 152NB00212, 152NB00109, and 152NB00209 do not meet the selection criteria.

Medium- and Low-Voltage AC Distribution

The medium- and low-voltage circuit breakers in 4160V and 480V AC Switchgear supplying power to loads identified in this section (battery chargers, DG ancillary systems, etc.) have been identified in Table 2-3 for evaluation. In addition to the protective relaying identified in the SPRA Relay Database from Reference [9] as controlling these circuit breakers, the circuit breakers themselves were selected for high frequency program screening as well.

| | Table 2-3: Electrical Power Components | | | | | |
|------------|---|--|--|--|--|--|
| Component | Description | Function | | | | |
| 152NB00110 | XNG03 Primary Circuit Breaker | Feeds Electrical Power to Transformer | | | | |
| 152NB00111 | DG01 Circuit Breaker | Feeds Electrical Power to MV Switchgear | | | | |
| 152NB00113 | XNG01 Primary Circuit Breaker | Feeds Electrical Power to Transformer | | | | |
| 152NB00115 | Essential Service Water Pump A Circuit Breaker | Feeds Electrical Power to Pump | | | | |
| 152NB00116 | XNG05 Primary Circuit Breaker | Feeds Electrical Power to Transformer | | | | |
| 152NB00210 | XNG04 Primary Circuit Breaker | Feeds Electrical Power to Transformer | | | | |
| 152NB00211 | DG02 Circuit Breaker | Feeds Electrical Power to MV Switchgear | | | | |
| 152NB00213 | XNG02 Primary Circuit Breaker | Feeds Electrical Power to Transformer | | | | |
| 152NB00215 | Essential Service Water Pump B Circuit Breaker | Feeds Electrical Power to Pump | | | | |
| 152NB00216 | XNG06 Primary Circuit Breaker | Feeds Electrical Power to Transformer | | | | |
| 52NG00101 | XNG01 Secondary Circuit Breaker | Feeds Electrical Power to LV Switchgear | | | | |
| 52NG00103 | NK021 Feeder Circuit Breaker | Feeds Electrical Power to Battery Charger | | | | |
| 52NG00106 | NG001A Feeder Circuit Breaker | Feeds Electrical Power to MCC | | | | |
| 52NG00201 | XNG02 Secondary Circuit Breaker | Feeds Electrical Power to LV Switchgear | | | | |
| 52NG00203 | NK024 Feeder Circuit Breaker | Feeds Electrical Power to Battery Charger | | | | |
| 52NG00206 | NG002A Feeder Circuit Breaker | Feeds Electrical Power to MCC | | | | |
| 52NG00301 | XNG03 Secondary Circuit Breaker | Feeds Electrical Power to LV Switchgear | | | | |
| 52NG00303 | NK023 Feeder Circuit Breaker | Feeds Electrical Power to Battery Charger | | | | |
| 52NG00307 | NG003D Feeder Circuit Breaker | Feeds Electrical Power to MCC | | | | |
| 52NG00401 | XNG03 Secondary Circuit Breaker | Feeds Electrical Power to LV | | | | |

| Table 2-3: Electrical Power Components | | | | | |
|--|---------------------------------------|---|--|--|--|
| Component | Description | Function | | | |
| | | Switchgear | | | |
| 52NG00403 | NK022 Feeder Circuit Breaker | Feeds Electrical Power to Battery Charger | | | |
| 52NG00407 | NG004D Feeder Circuit Breaker | Feeds Electrical Power to MCC | | | |
| 52NG005EAF1 | XNG05 Secondary Circuit Breaker | Feeds Electrical Power to MCC | | | |
| 52NG006EAF1 | XNG06 Secondary Circuit Breaker | Feeds Electrical Power to MCC | | | |
| CGM01A | DG01 Ventilation Supply Fan | Provides Room Ventilation for Diesel Generator | | | |
| CGM01B | DG02 Ventilation Supply Fan | Provides Room Ventilation for Diesel Generator | | | |
| EFHV0037 | ESW to UHS Isolation Valve | Throttled valve needs to open for DG Cooling | | | |
| EFHV0038 | ESW to UHS Isolation Valve | Throttled valve needs to open for DG Cooling | | | |
| EFHV0091 | Screen Wash Water Valve | Valve needs to operate to support DG Cooling | | | |
| EFHV0092 | Screen Wash Water Valve | Valve needs to operate to support DG Cooling | | | |
| EFPDV0019 | Self-Cleaning Strainer Trash Valve | Valve needs to operate to support DG Cooling | | | |
| EFPDV0020 | Self-Cleaning Strainer Trash Valve | Valve needs to operate to support DG Cooling | | | |
| FEF01A | Travelling Screen | Screen needs to operate for DG Cooling | | | |
| FEF01B | Travelling Screen | Screen needs to operate for DG Cooling | | | |
| FEF02A | Self-Cleaning Strainer | Strainer needs to operate for DG Cooling | | | |
| FEF02B | Self-Cleaning Strainer | Strainer needs to operate for DG Cooling | | | |
| GMHZ0009 | DG Room Ventilation Exhaust Damper | Damper needs to open to support DG Ventilation | | | |
| GMHZ0019 | DG Room Ventilation Exhaust Damper | Damper needs to open to support DG Ventilation | | | |
| GMTZ0001A | DG Room Ventilation Supply Damper | Damper needs to open to support DG Ventilation | | | |
| GMTZ0011A | DG Room Ventilation Supply Damper | Damper needs to open to support DG Ventilation | | | |
| KKJ01A | Diesel Engine | Provides Emergency Motive Power | | | |
| KKJ01B | Diesel Engine | Provides Emergency Motive Power | | | |
| NE001 | Generator | Converts Mechanical Power to Electrical | | | |
| NE002 | Generator | Converts Mechanical Power to Electrical | | | |
| PEF01A | Essential Service Water Pump A | Provides Cooling for Diesel Generator | | | |
| PEF01B | Essential Service Water Pump B | Provides Cooling for Diesel Generator | | | |
| PJE01A | Fuel Oil Transfer Pump A | Provides Fuel for Diesel Generator | | | |
| PJE01B | Fuel Oil Transfer Pump B | Provides Fuel for Diesel Generator | | | |

| Table 2-3: Electrical Power Components | | | | |
|--|--|--|--|--|
| Component | Description | Function | | |
| XNG01 | 4160V to 480V Step Down Transformer | Converts 4160V AC Electrical Power to 480V AC | | |
| XNG02 | 4160V to 480V Step Down Transformer | Converts 4160V AC Electrical Power to 480V AC | | |
| XNG03 | 4160V to 480V Step Down Transformer | Converts 4160V AC Electrical Power to 480V AC | | |
| XNG04 | 4160V to 480V Step Down Transformer | Converts 4160V AC Electrical Power to 480V AC | | |
| XNG05 | 4160V to 480V Step Down Transformer | Converts 4160V AC Electrical Power to 480V AC | | |
| XNG06 | 4160V to 480V Step Down Transformer | Converts 4160V AC Electrical Power to 480V AC | | |

480V AC MCCs, 120V AC, 250 VDC, and 125V DC Distribution

The 480V MCCs, and the 120V AC, 250 VDC, and 125V DC Distribution all use either Molded-Case Circuit Breakers [10, pp. 8.3-9] or fused disconnect switches, both of which are seismically rugged [11]. For this reason, these devices are not included in the device table. Contactors, and auxiliary and protective relays within the MCCs are covered under the components they control.

2.6 Summary of Selected Components

The investigation of high-frequency contact devices as described above was performed in Ref. [12]. A list of the contact devices requiring a high frequency confirmation is provided in Appendix B, Table B-1.

3 SEISMIC EVALUATION**

3.1 Horizontal Seismic Demand

Per Reference [4], Section 4.3, the basis for calculating high-frequency seismic demand on the subject components in the horizontal direction is the Wolf Creek Generating Station horizontal ground motion response spectrum (GMRS), which was generated as part of the WCGS Seismic Hazard and Screening Report [7] submitted to the NRC on March 31, 2014, and accepted by the NRC on August 12, 2015 [8].

It is noted in Reference [4] that a Foundation Input Response Spectrum (FIRS) may be necessary to evaluate buildings whose foundations are supported at elevations different than the Control Point elevation. However, for sites founded on rock, per Reference [4], "The Control Point GMRS developed for these rock sites are typically appropriate for all rock-founded structures and additional FIRS estimates are not deemed necessary for the high frequency confirmation effort." For sites founded on soil, the soil layers will shift the frequency range of seismic input towards the lower frequency range of the response spectrum by engineering judgment. Therefore, for purposes of high-frequency evaluations in this report, the GMRS is an adequate substitute for the FIRS for sites founded on soil.

The applicable buildings at WCGS are founded on soil and have only the Control Point GMRS defined; therefore, the Control Point GMRS is conservatively used as the input at the building foundation.

The horizontal GMRS values are provided in Table 3-2.

3.2 Vertical Seismic Demand

As described in Section 3.2 of Reference [4], the horizontal GMRS and site soil conditions are used to calculate the vertical GMRS (VGMRS), which is the basis for calculating high-frequency seismic demand on the subject components in the vertical direction.

The site's soil mean shear wave velocity vs. depth profile is provided in Reference [7], Table 2.3.2-2 and reproduced below in Table 3-1.

^{**} The high frequency screening was performed by report 16C4405-CAL-001 [16] and is summarized herein.

| | Table 3 | -1: Soil Mean She | ar Wave | Velocity vs | . Depth Profile | |
|-------|---------------|-----------------------------------|---------------------------|----------------------------------|-------------------------------------|----------------|
| Layer | Depth (ft) | Thickness, t _i (ft) | Vs _i (ft/s) | t _i / Vs _i | $\sum \left[t_i / V_{S_i} \right]$ | Vs30 (ft/s) |
| 1 | 5.0 | 5.0 | 550 | 0.0091 | 0.0091 | |
| 2 | 10.0 | 5.0 | 550 | 0.0091 | 0.0182 | |
| 3 | 15.0 | 5.0 | 1,450 | 0.0034 | 0.0216 | |
| 4 | 20.0 | 5.0 | 1,450 | 0.0034 | 0.0251 | |
| 5 | 25.0 | 5.0 | 1,450 | 0.0034 | 0.0285 | |
| 6 | 30.0 | 5.0 | 1,450 | 0.0034 | 0.0320 | |
| 7 | 36.0 | 6.0 | 1,450 | 0.0041 | 0.0361 | |
| 8 | 42.0 | 6.0 | 6,200 | 0.0010 | 0.0371 | |
| 9 | 48.0 | 6.0 | 6,200 | 0.0010 | 0.0380 | |
| 10 | 54.0 | 6.0 | 3,500 | 0.0017 | 0.0398 | 1983 |
| 11 | 60.0 | 6.0 | 3,500 | 0.0017 | 0.0415 | |
| 12 | 64.0 | 4.0 | 3,500 | 0.0011 | 0.0426 | |
| 13 | 70.0 | 6.0 | 6,200 | 0.0010 | 0.0436 | |
| 14 | 76.0 | 6.0 | 6,200 | 0.0010 | 0.0446 | |
| 15 | 82.0 | 6.0 | 6,200 | 0.0010 | 0.0455 | |
| 16 | 85.0 | 3.0 | 4,000 | 0.0008 | 0.0463 | |
| 17 | 98.4 | 13.4 | 4,000 | 0.0034 | 0.0496 | |

Using the shear wave velocity vs. depth profile, the velocity of a shear wave traveling from a depth of 30m (98.4ft) to the surface of the site (Vs30) is calculated per the methodology of Reference [4], Section 3.5.

- The time for a shear wave to travel through each soil layer is calculated by dividing the layer depth (di) by the shear wave velocity of the layer (Vsi).
- The total time for a wave to travel from a depth of 30m to the surface is calculated by adding the travel time through each layer from depths of 0m to 30m (Σ [di/Vsi]).
- The velocity of a shear wave traveling from a depth of 30m to the surface is therefore the total distance (30m) divided by the total time;
 i.e., Vs30 = (30m)/Σ[di/Vsi].

The site's soil class is determined by using the site's shear wave velocity (Vs30) and the peak ground acceleration (PGA) of the GMRS and comparing them to the values within Reference [4], Table 3-1. Based on the PGA of 0.288g and the shear wave velocity of 1983ft/s, the site soil class is A-Hard.

Once a site soil class is determined, the mean vertical vs. horizontal GMRS ratios (V/H) at each frequency are determined by using the site soil class and its associated V/H values in Reference [4], Table 3-2.

The vertical GMRS is then calculated by multiplying the mean V/H ratio at each frequency by the horizontal GMRS acceleration at the corresponding frequency. It is noted that Reference [4], Table 3-2 values are constant between 0.1Hz and 15Hz.

The V/H ratios and VGMRS values are provided in Table 3-2 of this report.

Figure 3-1 below provides a plot of the horizontal GMRS, V/H ratios, and vertical GMRS for WCGS.

| Response Spectra | | | | | |
|------------------|-------|-----------|-------|--|--|
| Frequency | HGMRS | V/H Ratio | VGMRS | | |
| (Hz) | (g) | | (g) | | |
| 100 | 0.288 | 0.78 | 0.225 | | |
| 90 | 0.290 | 0.81 | 0.235 | | |
| 80 | 0.294 | 0.85 | 0.250 | | |
| 70 | 0.301 | 0.89 | 0.268 | | |
| 60 | 0.313 | 0.90 | 0.282 | | |
| 50 | 0.341 | 0.88 | 0.300 | | |
| 40 | 0.383 | 0.84 | 0.322 | | |
| 35 | 0.417 | 0.79 | 0.329 | | |
| 30 | 0.460 | 0.74 | 0.340 | | |
| 25 | 0.526 | 0.69 | 0.363 | | |
| 20 | 0.589 | 0.67 | 0.395 | | |
| 15 | 0.683 | 0.67 | 0.458 | | |
| 12.5 | 0.727 | 0.67 | 0.487 | | |
| 10 | 0.706 | 0.67 | 0.473 | | |
| 9 | 0.674 | 0.67 | 0.452 | | |
| 8 | 0.628 | 0.67 | 0.421 | | |
| 7 | 0.579 | 0.67 | 0.388 | | |
| 6 | 0.505 | 0.67 | 0.338 | | |
| 5 | 0.438 | 0.67 | 0.293 | | |
| 4 | 0.329 | 0.67 | 0.220 | | |
| 3.5 | 0.265 | 0.67 | 0.178 | | |
| 3 | 0.214 | 0.67 | 0.143 | | |
| 2.5 | 0.171 | 0.67 | 0.115 | | |
| 2 | 0.160 | 0.67 | 0.107 | | |
| 1.5 | 0.134 | 0.67 | 0.090 | | |
| 1.25 | 0.119 | 0.67 | 0.080 | | |
| 1 | 0.095 | 0.67 | 0.064 | | |
| 0.9 | 0.087 | 0.67 | 0.059 | | |
| 0.8 | 0.081 | 0.67 | 0.054 | | |
| 0.7 | 0.075 | 0.67 | 0.050 | | |
| 0.6 | 0.069 | 0.67 | 0.046 | | |
| 0.5 | 0.064 | 0.67 | 0.043 | | |
| 0.4 | 0.052 | 0.67 | 0.035 | | |
| 0.35 | 0.045 | 0.67 | 0.030 | | |
| 0.3 | 0.039 | 0.67 | 0.026 | | |
| 0.25 | 0.032 | 0.67 | 0.022 | | |
| 0.2 | 0.026 | 0.67 | 0.017 | | |
| 0.15 | 0.019 | 0.67 | 0.013 | | |
| 0.125 | 0.016 | 0.67 | 0.011 | | |
| 0.1 | 0.013 | 0.67 | 0.009 | | |





Figure 3-1: Plot of the Horizontal and Vertical Ground Motions Response Spectra and V/H Ratios

3.3 Component Horizontal Seismic Demand

Per Reference [4] the peak horizontal acceleration is amplified using the following two factors to determine the horizontal in-cabinet response spectrum:

- Horizontal in-structure amplification factor AF_{SH} to account for seismic amplification at floor elevations above the host building's foundation
- Horizontal in-cabinet amplification factor AF_c to account for seismic amplification within the host equipment (cabinet, switchgear, motor control center, etc.)

The in-structure amplification factor AF_{SH} is derived from Figure 4-3 in Reference [4]. The incabinet amplification factor, AF_c is associated with a given type of cabinet construction. The three general cabinet types are identified in Reference [4] and Appendix I of EPRI NP-7148 [13] assuming 5% in-cabinet response spectrum damping. EPRI NP-7148 [13] classified the cabinet types as high amplification structures such as switchgear panels and other similar large flexible panels, medium amplification structures such as motor control panels and control room benchboard panels and low amplification structures such as motor control centers. All of the electrical cabinets containing the components subject to high frequency confirmation (see Table B-1 in Appendix B) can be categorized into one of the in-cabinet amplification categories in Reference [4] as follows:

- Typical motor control center cabinets consisting of a lineup of several interconnected sections. Each section is a relatively narrow cabinet structure with height-to-depth ratios of about 4.5 that allow the cabinet framing to be efficiently used in flexure for the dynamic response loading, primarily in the front-to-back direction. This results in higher frame stresses and hence more damping which lowers the cabinet response. In addition, the subject components are not located on large unstiffened panels that could exhibit high local amplifications. These cabinets qualify as low amplification cabinets.
- Switchgear cabinets are large cabinets consisting of a lineup of several interconnected sections typical of the high amplification cabinet category. Each section is a wide box-type structure with height-to-depth ratios of about 1.5 and may include wide stiffened panels. This results in lower stresses and hence less damping which increases the enclosure response. Components can be mounted on the wide panels, which results in the higher in-cabinet amplification factors.
- Control cabinets are in a lineup of several interconnected sections with moderate width. Each section consists of structures with height-to-depth ratios of about 3 which results in moderate frame stresses and damping. The response levels are mid-range between MCCs and switchgear and therefore these cabinets can be considered in the medium amplification category.

3.4 Component Vertical Seismic Demand

The component vertical demand is determined using the peak acceleration of the VGMRS between 15 Hz and 40 Hz and amplifying it using the following two factors:

- Vertical in-structure amplification factor AF_{SV} to account for seismic amplification at floor elevations above the host building's foundation
- Vertical in-cabinet amplification factor AF_c to account for seismic amplification within the host equipment (cabinet, switchgear, motor control center, etc.)

The in-structure amplification factor AF_{SV} is derived from Figure 4-4 in Reference [4]. The incabinet amplification factor, AF_c is derived in Reference [4] and is 4.7 for all cabinet types.

4 CONTACT DEVICE EVALUATIONS

Seismic Screening Evaluation

Per Reference [4], seismic capacities (the highest seismic test level reached by the contact device without chatter or other malfunction) for each subject contact device are determined by the following procedures:

- (1) If a contact device was tested as part of the EPRI High Frequency Testing program [11], then the component seismic capacity from this program is used.
- (2) If a contact device was not tested as part of [11], then one or more of the following means to determine the component capacity were used:
 - (a) Device-specific seismic test reports (either from the station or from the SQURTS testing program.
 - (b) Generic Equipment Ruggedness Spectra (GERS) capacities per [14] and [15].
 - (c) Assembly (e.g. electrical cabinet) tests where the component functional performance was monitored.

The high-frequency capacity of each device was evaluated with the component mounting point demand from Section 3 using the criteria in Section 4.5 of Reference [4]. The high-frequency seismic screening evaluations as described above are discussed in detail in Ref. [16].

Functional Screening Evaluation

Given the methodology undertaken for this report due to the recent completion of contact device mapping as part of the ongoing WCGS SPRA (refer to Section 2 of this report), the aforementioned seismic screening evaluation was performed on a superset of all contact devices associated with control of components important to the high frequency program. This superset contains devices covered by the high frequency program and those devices that screen out from consideration because they do not meet the functional selection criteria of Reference [4].

Accordingly, contact devices that did not seismically screen based upon sufficient capacity in exceedance of GMRS demand underwent a functional screening as documented in report 16C4405-RPT-003 [17]. The functional screening of relays and switches for high frequency seismic evaluation under EPRI 3002004396 [4] involves the examination of control subsystems in a three-step process: (1) functional analysis, (2) circuit analysis, and (3) chatter analysis. Each of these steps was performed on the control circuits containing devices that were not seismically screened, using established guidance for this type of analysis. Those devices which cannot be seismically or functionally screened are considered outliers in the High Frequency Program

A summary of the high-frequency evaluation conclusions is provided in Table B-1 in Appendix B.

5 CONCLUSIONS

5.1 General Conclusions

Wolf Creek Generating Station has performed a High Frequency Confirmation evaluation in response to the NRC's 50.54(f) letter [1] using the methods in EPRI report 3002004396 [4].

The evaluation identified a total of 527 components that required evaluation. As summarized in Table B-1 in Appendix B, 452 of the devices have adequate seismic capacity demonstrated by seismic screening, 37 screened functionally, and 38 components required resolution following the criteria in Section 4.6 of Reference [4].

For the 38 components requiring resolution, three options are being explored to adequately resolve potential seismic concern. In order to demonstrate sufficient seismic capacity in exceedance of GMRS demand, more detailed approaches for mounting point seismic demand and seismic capacity (including additional component testing) are being considered. Should the demonstration of adequate seismic screening for the GMRS not be feasible, actions will be identified that can adequately resolve potential seismic concerns.

5.2 Identification of Follow-Up Actions

The scoping of analytical and/or testing efforts for 38 components requiring resolution as identified in Table B-1 is being performed as a follow-up action of this report. Should the demonstration of adequate seismic screening for the GMRS not be feasible, operator actions have been identified that can adequately resolve potential seismic concerns. The final documentation of seismic adequacy of these 38 components by analytical, testing, or operator action approaches are expected to be completed 30 days after completion of WCGS Refueling Outage 22.

6 **REFERENCES**

- [1] NRC (E. Leeds and M. Johnson) Letter to All Power Reactor Licensees et al., "Request for Information Pursuant to Title 10 of the Code of Federal Regulations 50.54(f) Regarding Recommendations 2.1, 2.3 and 9.3 of the Near-Term Task Force Review of Insights from the Fukushima Dai-Ichi Accident," ADAMS Accession Number ML12053A340, March 12, 2012.
- [2] NRC Report, "Recommendations for Enhancing Reactor Safety in the 21st Century," ADAMS Accession Number ML111861807, July 12, 2011.
- [3] EPRI Report 1025287, "Seismic Evaluation Guidence: Screening, Prioritization, and Implimentation Details (SPID) for the Resolution of Fukushima Near-Term Task Force Recommendation 2.1: Seismic," Final Report, February 2013.
- [4] EPRI Report 3002004396, "High Frequency Program: Application Guidance for Functional Confirmation and Fragility Evaluation," Final Report, July 2015.
- [5] NRC (J. Davis) Letter to Nuclear Energy Institute (A. Mauer), "Endorsement of Electric Power Research Institute Final Draft Report 3002004396, 'High Frequency Program: Application Guidance for Functional Confirmation and Fragility.'," ADAMS Accession Number ML15218A569, September 17, 2015.
- [6] NRC (W. Dean) Letter to the Power Reactor Licensees on the Enclosed List, "Final Determination of Licensee Seismic Probabilistic Risk Assessments Under the Request for Information Pursuant to Title 10 of the Code of Federal Regulations 50.54(f) Regarding Recommendation 2.1 'Seismic' of the Near-Term Task Force Review...," ADAMS Accession Number ML15194A015, October 27, 2015.
- [7] WCNOC Letter (WO 14-0042) to NRC, "Wolf Creek Nuclear Operating Corporation's Seismic Hazard and Screening Report (CEUS Sites), Response NRC Request for Information Pursuant to 10 CFR 50.54(f) Regarding Recommendation 2.1 of the Near-Term Task Force Review of Insights from the Fukushima...," ADAMS Accession Number ML14097A020, March 31, 2014.
- [8] NRC (F. Vega) Letter to WCNOC (A. Heflin), "Wolf Creek Generating Station Staff Assessment of Information Provided Pursuant to Title 10 of the Code of Federal Regulations Part 50, Section 50.54(f), Seismic Hazard Reevaluations for Recommendation 2.1 of the Near-Term Task Force Review of...," ADAMS Accession Number ML15216A320, August 12, 2015.
- [9] Stevenson & Associates Calculation 13C4152-CAL-009 Rev. 1, "Summary of Relay

Screening for WCGS S-PRA.".

- [10] Wolf Creek Report, "Updated Safety Analysis Report (USAR)," Rev. 26, March 11, 2013.
- [11] EPRI Report 3002002997, "High Frequency Program: High Frequency Testing Summary," Final Report, September 2014.
- [12] Stevenson & Associates Report 16C4405-RPT-001, Rev. 0, "Selection of Relays and Switches for High Frequency Seismic Evaluation.".
- [13] EPRI Report NP-7148-SL, "Procedure for Evaluating Nuclear Power Plant Relay Seismic Functionality," Final Report December 1990.
- [14] EPRI Report NP-7147-SL, "Seismic Ruggedness of Relays," Final Report August 1991.
- [15] SQUG Advisory 2004-02, "Relay GERS Corrections," September 7, 2004.
- [16] Stevenson & Associates Calculation 16C4405-CAL-001, Rev. 0, "High Frequency Functional Confirmation and Fragility Evaluation of Relays.".
- [17] Stevenson & Associates Report 16C4405-RPT-003 Rev. 0, "Functional Screening of Relays and Switches for High Frequency Seismic Evaluation at WCGS.".

A. REPRESENTATIVE SAMPLE COMPONENT EVALUATIONS

A detailed example analysis of two components is provided within this section and reproduced from Ref. [16]. This example is intended to illustrate each step of the high frequency analysis methodology given in Section 4 [4].

A.1. High Frequency Seismic Demand

Calculate the high-frequency seismic demand on the components per the methodology from Reference [4].

Sample calculations for the high-frequency seismic demand of components 150G @ NB00215 (contained in NB002) and 186/T @ NB00210 (contained in NB002) located in the Control Building. Ref. [16] calculates the high-frequency seismic demand for all of the subject components.

A.1.1 Horizontal Seismic Demand

The horizontal site-specific GMRS for WCGS GMRS data can be found in Section 2 of Ref. [16]

Determine the peak acceleration of the horizontal GMRS between 15 Hz and 40 Hz.

Peak acceleration of horizontal GMRS SA_{GMRS} = 0.683g (at 15 Hz) between 15 Hz and 40 Hz (see Table 6.2 of Ref. [16]):

Calculate the horizontal in-structure amplification factor based on the distance between the bottom of the foundation elevation and the subject floor elevation.

| Bottom of Deepest Foundatio Elevation: | n $EL_{found} = 1968 \text{ ft}$ | |
|---|----------------------------------|---|
| Component Floor Elevation | $EL_{comp} = 2000 \text{ ft}$ | |
| the function state which and defined and the second | | 4 |

Components 150G @ NB00215 and 186/T @ NB00210 are both located in the Control Building at Elevation 2000'-0"

| Distance Between Component Floor | $h_{comp} = EL_{comp} - EL_{found} = 32 \text{ ft}$ |
|----------------------------------|---|
| and Foundation Elevation: | |

Work the distance between the component floor and foundation with Ref. [4], Fig. 4-3 to calculate the horizontal in-structure amplification factor:

| Slope of Amplification Factor Line, | $m_{\rm h} = \frac{2.1 - 1.2}{40 f t - 0 f t} = 0.225 \frac{1}{f t}$ |
|---|--|
| $0 ft < h_{comp} < 40 ft$ | |
| Intercept of Amplification Factor Line, | b _h 1.2 |
| 0 ft < hcomp < 40 ft | |
| Horizontal In-Structure Amplification Factor (Ref. [4], p.4-13): | $AF_{SH}(h_{comp}) = (m_h * h_{comp} + b_h)$ if $h_{comp} \ll 40$ ft |
| | 2.1 otherwise |
| | $AF_{SH}(h_{comp}) = 1.92$ |

Calculate the horizontal in-cabinet amplification factor based on the type of cabinet that contains the subject component.

| Type of Cabinet | cab = "Switchgear" | | | | |
|---|--------------------|--------------------------------|--|--|--|
| (enter "MCC", "Switchgear", "Control | | | | | |
| Cabinet", or "Rigid"): | | | | | |
| Cabinet", or "Rigid"): Horizontal In-Cabinet Amplification Factor (Ref. [4], p. 4-13):: | $AF_{c.h}(cab) =$ | 3.6 if cab = "MCC" | | | |
| | | 7.2 if cab = "Switchgear" | | | |
| | | 4.5 if cab = "Control Cabinet" | | | |
| | | 1.0 if cab = "Rigid" | | | |
| | $AF_{c.h}(cab) =$ | 7.2 | | | |
| | | | | | |

Multiply the peak horizontal GMRS acceleration between by the horizontal in-structure and incabinet amplification factors to determine the in-cabinet response spectrum demand on the components.

| Horizontal In-Cabinet Response | $ICRSc.h = AF_{SH} * AF_{c.h} * SAH_{GMRS} = 9.44g$ |
|--------------------------------|---|
| Spectrum: | |

Note that the horizontal seismic demand is the same for both components, but the In-Cabinet Amplification Factor is not applied when the capacity is calculated per Section 6.3.1 of Ref. [16].

A.1.2 Vertical Seismic Demand

Determine the peak acceleration of the horizontal GMRS between 15 Hz and 40 Hz.

Peak acceleration of horizontal GMRS SA_{GMRS} = 0.683g (at 15 Hz) between 15 Hz and 40 Hz (see Table 6.2 of Ref. [16]):

Obtain the peak ground acceleration (PGA) of the horizontal GMRS (See Table 6.2 of Ref. [16]).

Peak Ground Acceleration (GMRS) $PGA_{GMRS} = 0.727g$

Calculate the shear wave velocity traveling from a depth of 30m to the surface of the site (Vs30) from Ref. [4]

Shear Wave Velocity:

| V = | (3 | 30m) |
|--------|----|------|
| *s30 = | - | di |
| | 4 | Vsi |

where,

d_i: Thickness of the layer (ft), V_{si}: Shear wave velocity of the layer (ft/s)

Per Table 6.1 of Ref. [16], the sum of thickness of the layer over shear wave velocity of the layer is 0.0496 sec.

Shear Wave Velocity:

 $VS_{30} = 30 \text{ m} / 0.0496 \text{sec} = 1983 \text{ ft/sec}$

Work the PGA and shear wave velocity with Ref. [4], Table 3-1 to determine the soil class of the site. Based on the PGA of 0.727g and shear wave velocity of 1983 ft/sec at Wolf Creek, the site soil class is A-Hard. Work the site soil class with Ref. [4], Table 3-2 to determine the mean vertical vs. horizontal GMRS ratios (V/H) at each spectral frequency. Multiply the V/H ratio at each frequency between 15Hz and 40Hz by the corresponding horizontal GMRS acceleration at each frequency between 15Hz and 40Hz to calculate the vertical GMRS. Table 6.2 of Ref. [16] calculates the vertical GMRS (equal to (V/H) x horizontal GMRS).

Determine the peak acceleration of the vertical GMRS (SAVGMRS) between frequencies of 15Hz and 40Hz.

V/H Ratio at 15Hz (See Table 6.2 of VH = 0.67 Ref. [16]):

| Horizontal GMRS at Frequency of Peak Vertical GMRS (at 15Hz) (See Table 6.2 of Ref. [16]): | HGMRS = 0.683g |
|--|---|
| Peak Acceleration of Vertical GMRS | $SAV_{GMRS} = VH * HGMRS = 0.458g$ (at 15 |

Calculate the vertical in-structure amplification factor based on the distance between the plant foundation elevation and the subject floor elevation.

Hz)

Distance Between Component Floor $h_{comp} = 32$ ft and Foundation:

Between 15 Hz and 40 Hz:

Work the distance between the component floor and foundation with Ref. [4], Fig. 4-4 to calculate the vertical in-structure amplification factor.

| Slope of Amplification Factor Line | $M_{v} = \frac{2.7 - 1.0}{100 f t - 0 f t} = 0.017 \frac{1}{f t}$ |
|--|---|
| Intercept of Amplification Factor Line | B _v 1.0 |
| Vertical In-Structure Amplification Factor: | $AF_{sv}(h_{comp}) = (m_v * h_{comp} + b_v)$ if $h_{comp} \leq 40$ ft |
| | 2.1 otherwise |
| | $AF_{SV}(h_{comp}) = 1.54$ |

Per Ref. [4] the vertical in-cabinet amplification factor is 4.7 regardless of cabinet type.

Vertical In-Cabinet Amplification $AF_{c.v} = 4.7$ Factor:

Multiply the peak vertical GMRS acceleration between by the vertical in-structure and in-cabinet amplification factors to determine the in-cabinet response spectrum demand on the component.

Vertical In-Cabinet Response Spectrum ICRSc.v = $AF_{SV} * AF_{c.v} * SAV_{GMRS} = 3.32g$ (Ref. [4], p. 4-12, Eq. 4-1b):

Note that the vertical seismic demand is the same for both components, but the In-Cabinet Amplification Factor is not applied when the capacity is calculated per Section 6.3.1.

A.2. High Frequency Capacity

A sample calculation for the high-frequency seismic capacity of components 150G @ NB00215 (contained in NB002) and 186/T @ NB00210 (contained in NB002) is presented here. A table that calculates the high-frequency seismic capacities for all the subject components listed in Table 1.1 of Ref. [16]. Table 6.3 of Ref. 16 contains the demands for all plant locations that contain essential relays.

A.2.1 Seismic Test Capacity

The high frequency seismic capacity of a component can be determined from the EPRI High Frequency Testing Program or other broad banded low frequency capacity data such as the Generic Equipment Ruggedness Spectra (GERS) or other qualification reports.

The model for component 150G @ NB00215, a General Electric 12PJC11AV1A relay per Table 1.1 of Ref. [16], was not tested as part of the high-frequency testing program. Section 6.3.1.4 of Ref. [16] provides a high-frequency seismic capacity estimation relay based on WCGS seismic qualification. The seismic capacity was calculated in Section 6.3.1.4 of Ref. [16] to be 3.03g horizontal and 2.08g vertical for component 150G @ NB00215.

The model for component 186/T @ NB00210 is a General Electric 12HEA61B235 relay per Table 1.1 of Ref. [16], was not tested as part of the high-frequency testing program. High Frequency capacity was determined to be 21.8g per 16C4405-RPT-001 [12].

A.2.2 Seismic Capacity Knockdown Factor

Determine the seismic capacity knockdown factor for the subject relay based on the type of testing used to determine the seismic capacity of the relay. Using table 4-2 of Ref. [4], the knockdown factors are chosen as:

| Seismic capacity knockdown factor: | Fk = 1.2 | (150G @ NB00215) | | |
|------------------------------------|----------|-------------------|--|--|
| | Fk = 1.5 | (186/T @ NB00210) | | |

A.2.3 Seismic Testing Single-Axis Correction Factor

Determine the seismic testing single-axis correction factor of the subject relay, which is based on whether the equipment housing to which the relay is mounted has well-separated horizontal and vertical motion or not. Per Ref. [4], pp. 4-17 to 4-18, relays mounted within cabinets that are

braced, bolted together in a row, mounted to both floor and wall, etc. will have a correction factor of 1.00. Relays mounted within cabinets that are bolted only to the floor or otherwise not well-braced will have a correction factor of 1.2. Per Ref. [4], pp. 4-18, conservatively take the FMS value as 1.0.

Single-axis correction factor (Ref. [4], $F_{MS} = 1.0$ pp. 4-17 to 4-18):

A.2.4 Effective Wide-Band Component Capacity Acceleration

Calculate the effective wide-band component capacity acceleration per Ref. [4], Eq. 4-5.

| Effective wide-band component capacity acceleration (Ref. [4], Eq. 4-5) | $TRS = \frac{SAt}{Fk} *$ Fms = | | | | |
|--|-----------------------------------|-------------------|--|--|--|
| | TRS = 1.73g | (150G @ NB00215) | | | |
| | TRS = 14.53g | (186/T @ NB00210) | | | |

A.2.5 Component Margin

Calculate the high-frequency seismic margin for relays per Ref. [4], Eq. 4-6. A sample calculation for the high-frequency seismic demand of relay components 150G @ NB00215 and 186/T @ NB00210 is presented here. A table that calculates the high-frequency seismic margin for all of the subject relays listed in Table 1.1 of Ref. [16] is provided in Table 6.3 of Ref. [16].

| Horizontal seismic margin (Ref. [4], Eq. 4-6): | $\frac{TRS}{ICRSc.h} =$ | 1.32 > 1.0, OK NB00215) | (150G @ |
|---|-------------------------|----------------------------|----------|
| | | 1.54 > 1.0, OK NB00210) | (186/T @ |
| Vertical seismic margin (Ref. [4], Eq. 4-6): | $\frac{TRS}{ICRSc.v} =$ | 2.45 > 1.0, OK NB00215) | (150G @ |
| | | 4.38> 1.0, OK NB00210) | (186/T @ |

B. COMPONENTS IDENTIFIED FOR HIGH FREQUENCY CONFIRMATION

| | Table B-1 Components Identified for High Frequency Confirmation | | | | | | | | | |
|-----|---|--------------------|-----------------------|-------------------------|----------|--------------------|----------|---------------|-----------------------------|-------------------------|
| | | Component | | E | nclosure | | Floor | Component | Evaluation | |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 1 | 72 @ BB007 | Relay | Gould | P102D12 | BB007 | Control Cabinet | AUX | 2026-00 | Not Available | Functionally Screens |
| 2 | AR @ BB007 | Relay | Struthers & Dunn | 219BBX221NE (ND, NO) | BB007 | Control Cabinet | AUX | 2026-00 | GERS | Functionally Screens |
| 3 | 72 @ BB008 | Relay | Gould | P102D12 | BB008 | Control Cabinet | AUX | 2026-00 | Not Available | Functionally Screens |
| 4 | AR @ BB008 | Relay | Struthers & Dunn | 219BBX221NE (ND, NO) | BB008 | Control Cabinet | AUX | 2026-00 | GERS | Functionally Screens |
| 5 | EFPDS0019A @ EF155 | Pressure Switch | SOR | 103AS-B803-NX | EF155 | Control Cabinet | ESW | 2014-11 | WCGS report | Cap > Dem |
| 6 | EFPDS0020A @ EF156 | Pressure Switch | SOR | 103AS-B803-NX | EF156 | Control Cabinet | ESW | 2014-06 | Not Available | Functionally Screens |
| 7 | 42C @ FC0219 | Relay | Schneider Electric | LADN31 | FC0219 | Wall Mounted | AUX | 2002-00 | WCGS report | Cap > Dem |
| 8 | 42O @ FC0219 | Relay | Schneider Electric | LADN31 | FC0219 | Wall Mounted | AUX | 2002-00 | WCGS report | Cap > Dem |
| 9 | 5(CON1) @ FC0219 | Relay | Schneider Electric | LADN31 | FC0219 | Wall Mounted | AUX | 2002-00 | WCGS report | Cap > Dem |
| 10 | CR2 @ FC0219 | Relay | IDEC | RH4B-UL | FC0219 | Wall Mounted | AUX | 2002-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 11 | CR3 @ FC0219 | Relay | IDEC | RH4B-UL | FC0219 | Wall Mounted | AUX | 2002-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 12 | CR4 @ FC0219 | Relay | IDEC | RH4B-UL | FC0219 | Wall Mounted | AUX | 2002-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 13 | CR7 @ FC0219 | Relay | IDEC | RH4B-UL | FC0219 | Wall Mounted | AUX | 2002-00 | SQUG Advisory 2004-02 | Cap > Dem |

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| | Table B-1 Components Identified for High Frequency Confirmation | | | | | | | | | |
|-----|---|-----------|--------------|--------------------|-----------|--------------------|----------|---------------|-----------------------------|-------------------------|
| | | Component | | | Enclosure | | | Floor | Component Evaluation | |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 14 | CR8 @ FC0219 | Relay | IDEC | RH4B-UL | FC0219 | Wall Mounted | AUX | 2002-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 15 | FCSC0313 @ FC0219 | Relay | Dresser-Rand | 890354-001 | FC0219 | Wall Mounted | AUX | 2002-00 | WCGS report | Cap > Dem |
| 16 | FCZC0313 @ FC0219 | Relay | Dresser-Rand | 890265-010 | FC0219 | Wall Mounted | AUX | 2002-00 | WCGS report | Cap > Dem |
| 17 | 4A @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 18 | 4B @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 19 | 5A @ KJ0121 | Relay | Agastat | 7022PE (ND, ALL) | KJ0121 | Control Cabinet | DGB | 2000-00 | GERS | Functionally Screens |
| 20 | 5B @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 21 | 5E @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 22 | ASR @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 23 | BDR @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 24 | CC2 @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 25 | CC3 @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 26 | CC4 @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 27 | CT1 @ KJ0121 | Relay | ITE/Gould | J14P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |

| | |] | Table B-1 Comp | onents Identified f | or High Fr | requency C | onfirmati | on | | |
|-----|--------------|-------|----------------|---------------------|------------|--------------------|-----------|---------------|-----------------------------|------------------------|
| | | 1 | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 28 | CT2 @ KJ0121 | Relay | ITE/Gould | J14P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 29 | CT3 @ KJ0121 | Relay | ITE/Gould | J14P4012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 30 | СТ4 @ КЈ0121 | Relay | ITE/Gould | J14P4012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 31 | EOR @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 32 | ESA @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 33 | ESB @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 34 | HSR @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 35 | LSR @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 36 | OP1 @ KJ0121 | Relay | ITE/Gould | J14P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 37 | OP2 @ KJ0121 | Relay | ITE/Gould | J14P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 38 | OP3 @ KJ0121 | Relay | ITE/Gould | J14P4012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 39 | OP4 @ KJ0121 | Relay | ITE/Gould | J14P4012 | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 40 | SDR @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 41 | SFR @ KJ0121 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |

| | |] | Table B-1 Comp | onents Identified fo | or High Fi | requency C | Confirmati | ion | | |
|-----|---------------|-------|----------------|----------------------|------------|--------------------|------------|---------------|-----------------------------|-------------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 42 | T2A @ KJ0121 | Relay | Agastat | 7012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 43 | T2B @ KJ0121 | Relay | Agastat | 7012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 44 | TACH @ KJ0121 | Relay | Dynalco | SST-2400A | KJ0121 | Control Cabinet | DGB | 2000-00 | WCGS report | Cap > Dem |
| 45 | TD3 @ KJ0121 | Relay | Agastat | 7014 | KJ0121 | Control Cabinet | DGB | 2000-00 | GERS | Cap > Dem |
| 46 | TD3A @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 47 | TSR @ KJ0121 | Relay | ITE/Gould | J13P2012 | KJ0121 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 48 | 4A @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 49 | 4B @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 50 | 5A @ KJ0122 | Relay | Agastat | 7022PE (ND, ALL) | KJ0122 | Control Cabinet | DGB | 2000-00 | GERS | Functionally Screens |
| 51 | 5B @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 52 | 5E @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 53 | ASR @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 54 | BDR @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 55 | CC2 @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory | Cap > Dem |

| | |] | Table B-1 Comp | onents Identified f | or High Fi | requency C | onfirmati | on | | |
|-----|--------------|-------|----------------|---------------------|------------|--------------------|-----------|---------------|-----------------------------|------------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| | | | | | | | | | 2004-02 | |
| 56 | CC3 @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 57 | CC4 @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 58 | CT1 @ KJ0122 | Relay | ITE/Gould | J14P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 59 | CT2 @ KJ0122 | Relay | ITE/Gould | J14P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 60 | CT3 @ KJ0122 | Relay | ITE/Gould | J14P4012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 61 | CT4 @ KJ0122 | Relay | ITE/Gould | J14P4012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 62 | EOR @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 63 | ESA @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 64 | ESB @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 65 | HSR @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 66 | LSR @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 67 | OP1 @ KJ0122 | Relay | ITE/Gould | J14P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 68 | OP2 @ KJ0122 | Relay | ITE/Gould | J14P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |

| | | Ta | able B-1 Comp | onents Identified fo | or High F | requency Co | onfirmati | ion | | |
|-----|------------------------|--------------------|---------------|----------------------------|-----------|--------------------|-----------|---------------|-----------------------------|------------------------|
| | | C | omponent | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 69 | OP3 @ KJ0122 | Relay | ITE/Gould | J14P4012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 70 | OP4 @ KJ0122 | Relay | ITE/Gould | J14P4012 | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Requires Resolution |
| 71 | SDR @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 72 | SFR @ KJ0122 | Relay | ITE/Gould | J13P3012 (Class J) | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 73 | T2A @ KJ0122 | Relay | Agastat | 7012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 74 | T2B @ KJ0122 | Relay | Agastat | 7012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 75 | TACH @ KJ0122 | Relay | Dynalco | SST-2400A | KJ0122 | Control Cabinet | DGB | 2000-00 | WCGS report | Cap > Dem |
| 76 | TD3 @ KJ0122 | Relay | Agastat | 7014 | KJ0122 | Control Cabinet | DGB | 2000-00 | GERS | Cap > Dem |
| 77 | TD3A @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 78 | TSR @ KJ0122 | Relay | ITE/Gould | J13P2012 | KJ0122 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 79 | EOS @ TVKJ01 | Micro Switch | Micro-Switch | BZV6-2RQ2 | KKJ01A | Unknown | DGB | 2000-00 | WCGS report | Cap > Dem |
| 80 | KJPS0062 @ TVKJ19 | Pressure Switch | SOR | 4N6-B5-NX-C1A- JJTTX12 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 81 | KJPSH0023B @ TVKJ01 | Pressure Switch | SOR | 12N6-B45-NX-C1A- JJTTX7 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 82 | KJPSH0023C @ TVKJ01 | Pressure Switch | SOR | 12N6-B45-NX-C1A- JJTTX7 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 83 | KJPSH0023D @ TVKJ01 | Pressure Switch | SOR | 12N6-B45-NX-C1A- JJTTX7 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |

| | | Ta | able B-1 Com | oonents Identified fo | or High F | requency Co | onfirmati | ion | | |
|-----|------------------------|-----------------------|------------------------|----------------------------|-----------|--------------|-----------|---------------|-----------------------|----------------------|
| | | C | omponent | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 84 | KJPSL0026A @ TVKJ01 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 85 | KJPSL0026B @ TVKJ01 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 86 | KJPSL0026C @ TVKJ01 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 87 | KJPSL0026D @ TVKJ01 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01A | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 88 | KJTSH0059A @ TVKJ01 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01A | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 89 | KJTSH0059B @ TVKJ01 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01A | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 90 | KJTSH0059C @ TVKJ01 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01A | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 91 | KJTSH0059D @ TVKJ01 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01A | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 92 | EOS @ TVKJ02 | Micro Switch | Micro-Switch | BZV6-2RQ2 | KKJ01B | Unknown | DGB | 2000-00 | WCGS report | Cap > Dem |
| 93 | KJPS0162 @ TVKJ20 | Pressure Switch | SOR | 4N6-B5-NX-C1A- JJTTX12 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 94 | KJPSH0123B @ TVKJ02 | Pressure Switch | SOR | 12N6-B45-NX-C1A- JJTTX7 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 95 | KJPSH0123C @ TVKJ02 | Pressure Switch | SOR | 12N6-B45-NX-C1A- JJTTX7 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 96 | KJPSH0123D @ TVKJ02 | Pressure Switch | SOR | 12N6-B45-NX-C1A- JJTTX7 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 97 | KJPSL0126A @ TVKJ02 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 98 | KJPSL0126B @ TVKJ02 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 99 | KJPSL0126C @ TVKJ02 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |

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| | | T | able B-1 Comp | onents Identified fo | or High F | requency Co | onfirmati | ion | | |
|-----|--------------------------|-----------------------|------------------------|----------------------|-----------|--------------|-----------|---------------|-----------------------|----------------------|
| | | С | omponent | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 100 | KJPSL0126D @ TVKJ02 | Pressure Switch | Detroit Switch Inc. | 222-1024-NB4 | KKJ01B | Skid Mounted | DGB | 2000-00 | GERS | Cap > Dem |
| 101 | KJTSH0159A @ TVKJ02 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01B | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 102 | KJTSH0159B @ TVKJ02 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01B | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 103 | KJTSH0159C @ TVKJ02 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01B | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 104 | KJTSH0159D @ TVKJ02 | Temperature Switch | SOR | 201TA-B125-JJTTX9 | KKJ01B | Skid Mounted | DGB | 2000-00 | Vendor report | Cap > Dem |
| 105 | 103CL @ NB00111 | Relay | GE | HGA111J2 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 106 | 125F @ NB00109 | Relay | Basler Electric | M1GA6PN5S3F | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 107 | 125F @ NB00112 | Relay | Basler Electric | M1GA6PN5S3F | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 108 | 127-1DG @ NB00101 | Relay | GE | 12NGV28B1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 109 | 127-2DG @ NB00113 | Relay | GE | 12NGV28B1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 110 | 127-2F(109) @ NB00111 | Relay | GE | 12NGV13B25A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 111 | 127-2F(112) @ NB00111 | Relay | GE | 12NGV13B25A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 112 | 127-3DG @ NB00117 | Relay | GE | 12NGV28B1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 113 | 127-4DG @ NB00116 | Relay | GE | 12NGV28B1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 114 | 150-151/T-A @ NB00110 | Relay | GE | 121AC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 115 | 150-151/T-A @ NB00113 | Relay | GE | 121AC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |

| | ······· |] | Table B-1 Compo | onents Identified f | for High F | requency C | onfirmati | ion | | |
|-----|--------------------------|-------|-----------------|---------------------|------------|------------|-----------|---------------|-----------------------|----------------------|
| | | | Component | | Er | iclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 116 | 150-151/T-A @ NB00116 | Relay | GE | 12IAC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 117 | 150-151/T-B @ NB00110 | Relay | GE | 12IAC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 118 | 150-151/T-B @ NB00113 | Relay | GE | 12IAC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 119 | 150-151/T-B @ NB00116 | Relay | GE | 12IAC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 120 | 150-151/T-C @ NB00110 | Relay | GE | 121AC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 121 | 150-151/T-C @ NB00113 | Relay | GE | 121AC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 122 | 150-151/T-C @ NB00116 | Relay | GE | 12IAC53B812A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 123 | 150-151-A @ NB00115 | Relay | GE | 121AC66K8A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 124 | 150-151-B @ NB00115 | Relay | GE | 12IAC66K8A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 125 | 150-151-C @ NB00115 | Relay | GE | 12IAC66K8A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 126 | 150G @ NB00115 | Relay | GE | 12PJC11AV1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 127 | 151DG-A@ NB00111 | Relay | GE | 121AC66A2A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 128 | 151DG-B@ NB00111 | Relay | GE | 121AC66A2A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 129 | 151DG-C@ NB00111 | Relay | GE | 121AC66A2A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 130 | 151F-A @ NB00109 | Relay | GE | 121AC53A803A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 131 | 151F-A @ NB00112 | Relay | GE | 12IAC53A803A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |

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| | | Т | able B-1 Comp | onents Identified fo | or High F | requency C | onfirmati | ion | | |
|-----|-------------------------|--------------------|---------------|-----------------------------|-----------|------------|-----------|---------------|-----------------------|------------------------|
| | | (| Component | | Er | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 132 | 151F-B @ NB00109 | Relay | GE | 12IAC53A803A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 133 | 151F-B @ NB00112 | Relay | GE | 12IAC53A803A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 134 | 151F-C @ NB00109 | Relay | GE | 12IAC53A803A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 135 | 151F-C @ NB00112 | Relay | GE | 12IAC53A803A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 136 | 151G/T @ NB00110 | Relay | GE | 12PJC11AV1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 137 | 151G/T @ NB00113 | Relay | GE | 12PJC11AV1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 138 | 151G/T @ NB00116 | Relay | GE | 12PJC11AV1A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 139 | 151G-F @ NB00109 | Relay | GE | 12IAC53A801A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 140 | 151G-F @ NB00112 | Relay | GE | 12IAC53A801A | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 141 | 151N/T @ NB00116 | Relay | Not Available | Not Available | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 142 | 152NB00110@ NB00110 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 1200-78 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 143 | 152NB00111@ NB00111 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 2000-78 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 144 | 152NB00113 @ NB00113 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 2000-78 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 145 | 152NB00115 @ NB00115 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 1200-78 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 146 | 152NB00116@ NB00116 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 1200-78 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 147 | 186/T @ NB00110 | Relay | GE | 12HEA61B235 | NB001 | Switchgear | СВ | 2000-00 | EPRI HF Test | Cap > Dem |

| | | | Table B-1 Com | ponents Identified fo | r High F | requency C | onfirmati | ion | | |
|-----|--------------------------|-------|-----------------|-----------------------|----------|------------|-----------|---------------|-----------------------|----------------------|
| 1 | | | Component | | Er | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 148 | 186/T @ NB00113 | Relay | GE | 12HEA61B235 | NB001 | Switchgear | СВ | 2000-00 | EPRI HF Test | Cap > Dem |
| 149 | 186/T @ NB00116 | Relay | GE | 12HEA61B235X2 | NB001 | Switchgear | СВ | 2000-00 | EPRI HF Test | Cap > Dem |
| 150 | 186F @ NB00109 | Relay | GE | HEA61B234 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 151 | 186F @ NB00112 | Relay | GE | HEA61B234 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 152 | 186M @ NB00115 | Relay | GE | HEA61A224 | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 153 | 286-1T1 @ NB00112 | Relay | GE | HEA99AL or HEA61BA | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 154 | 286-2T2 @ NB00109 | Relay | GE | HEA99AL or HEA61BA | NB001 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 155 | 103CL @ NB00211 | Relay | GE | HGA111J2 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 156 | 103CL @ NB00215 | Relay | GE | HGA111J2 | NB002 | Switchgear | CB | 2000-00 | WCGS report | Cap > Dem |
| 157 | 125F @ NB00209 | Relay | Basler Electric | MIGA6PN5S3F | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 158 | 125F @ NB00212 | Relay | Basler Electric | MIGA6PN5S3F | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 159 | 127-1DG @ NB00210 | Relay | GE | 12NGV28B1A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 160 | 127-2DG @ NB00216 | Relay | GE | 12NGV28B1A | NB002 | Switchgear | CB | 2000-00 | WCGS report | Cap > Dem |
| 161 | 127-2F(209) @ NB00211 | Relay | GE | 12NGV13B25A | NB002 | Switchgear | CB | 2000-00 | WCGS report | Cap > Dem |
| 162 | 127-2F(212) @ NB00211 | Relay | GE | 12NGV13B25A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 163 | 127-3DG @ NB00217 | Relay | GE | 12NGV28B1A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |

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| | | 1 | Table B-1 Compo | onents Identified f | for High F | requency C | onfirmati | ion | | 6 |
|-----|--------------------------|-------|-----------------|---------------------|------------|------------|-----------|---------------|-----------------------|----------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 164 | 127-4DG @ NB00201 | Relay | GE | 12NGV28B1A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 165 | 150-151/T-A @ NB00210 | Relay | GE | 12IAC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 166 | 150-151/T-A @ NB00213 | Relay | GE | 121AC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 167 | 150-151/T-A @ NB00216 | Relay | GE | 121AC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 168 | 150-151/Т-В @ NB00210 | Relay | GE | 121AC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 169 | 150-151/T-B @ NB00213 | Relay | GE | 12IAC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 170 | 150-151/T-B @ NB00216 | Relay | GE | 12IAC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 171 | 150-151/T-C @ NB00210 | Relay | GE | 12IAC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 172 | 150-151/T-C @ NB00213 | Relay | GE | 12IAC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 173 | 150-151/T-C @ NB00216 | Relay | GE | 12IAC53B812A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 174 | 150-151-A @ NB00215 | Relay | GE | 12IAC66K8A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 175 | 150-151-B @ NB00215 | Relay | GE | 12IAC66K8A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 176 | 150-151-C @ NB00215 | Relay | GE | 12IAC66K8A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 177 | 150G @ NB00215 | Relay | GE | 12PJC11AVIA | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 178 | 151DG-A @ NB00211 | Relay | GE | 12IAC66A2A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 179 | 151DG-B @ NB00211 | Relay | GE | 12IAC66A2A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |

| | |] | able B-1 Com | onents Identified fo | or High F | requency C | onfirmati | ion | | |
|-----|-------------------------|--------------------|---------------|---------------------------------------|-----------|------------|-----------|---------------|-----------------------|------------------------|
| - | | (| Component | · · · · · · · · · · · · · · · · · · · | Er | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 180 | 151DG-C @ NB00211 | Relay | GE | 121AC66A2A | NB002 | Switchgear | CB | 2000-00 | WCGS report | Cap > Dem |
| 181 | 151F-A @ NB00209 | Relay | GE | 121AC53A803A | NB002 | Switchgear | CB | 2000-00 | WCGS report | Cap > Dem |
| 182 | 151F-A @ NB00212 | Relay | GE | 12IAC53A803A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 183 | 151F-B @ NB00209 | Relay | GE | 121AC53A803A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 184 | 151F-B @ NB00212 | Relay | GE | 12IAC53A803A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 185 | 151F-C @ NB00209 | Relay | GE | 12IAC53A803A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 186 | 151F-C @ NB00212 | Relay | GE | 121AC53A803A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 187 | 151G/T @ NB00210 | Relay | GE | 12PJC11AV1A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 188 | 151G/T @ NB00213 | Relay | GE | 12PJC11AV1A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 189 | 151G/T @ NB00216 | Relay | GE | 12PJC11AV1A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 190 | 151G-F @ NB00209 | Relay | GE | 121AC53A801A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 191 | 151G-F @ NB00212 | Relay | GE | 121AC53A801A | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 192 | 151N/T @ NB00216 | Relay | Not Available | Not Available | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 193 | 152NB00210 @ NB00210 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 1200-78 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 194 | 152NB00211@ NB00211 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 2000-78 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 195 | 152NB00213 @ NB00213 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 2000-78 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |

| | | 1 | able B-1 Com | ponents Identified fo | r High F | requency C | onfirmati | ion | | |
|-----|-------------------------|--------------------|---------------|-----------------------------|----------|--------------------|-----------|---------------|-----------------------------|-------------------------|
| | | (| Component | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 196 | 152NB00215 @ NB00215 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 1200-78 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 197 | 152NB00216 @ NB00216 | Circuit Breaker | Siemens | 5KV-3AF-GER-350- 1200-78 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Requires Resolution |
| 198 | 186/T @ NB00210 | Relay | GE | 12HEA61B235 | NB002 | Switchgear | СВ | 2000-00 | EPRI HF Test | Cap > Dem |
| 199 | 186/T @ NB00213 | Relay | GE | 12HEA61B235 | NB002 | Switchgear | СВ | 2000-00 | EPRI HF Test | Cap > Dem |
| 200 | 186/T @ NB00216 | Relay | GE | 12HEA61B235X2 | NB002 | Switchgear | СВ | 2000-00 | EPRI HF Test | Cap > Dem |
| 201 | 186F @ NB00209 | Relay | GE | HEA61B234 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 202 | 186F @ NB00212 | Relay | GE | HEA61B234 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 203 | 186M @ NB00215 | Relay | GE | HEA61A224 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 204 | 195 @ NB00201 | Relay | GE | 12HEA61B232 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 205 | 195 @ NB00210 | Relay | GE | 12HEA61B232 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 206 | 195 @ NB00211 | Relay | GE | 12HEA61B232 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 207 | 195 @ NB00213 | Relay | GE | 12HEA61B232 | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 208 | 195 @ NB00215 | Relay | Not Available | Not Available | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 209 | 286-1T2 @ NB00209 | Relay | GE | HEA99AL or HEA61BA | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 210 | 286-2T1 @ NB00212 | Relay | GE | HEA99AL or HEA61BA | NB002 | Switchgear | СВ | 2000-00 | WCGS report | Cap > Dem |
| 211 | 102DG @ NE106 | Relay | ABB | 293B301A16A (Type: TD-5) | NE106 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Functionally Screens |

| | | 1 | Table B-1 Com | ponents Identified fo | r High Fi | requency C | onfirmati | ion | | |
|-----|------------------------|-------|-----------------|--------------------------------------|-----------|--------------------|-----------|---------------|-----------------------------|-------------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 212 | 124DG @ NE106 | Relay | GE | 12STV11A5A | NE106 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Requires Resolution |
| 213 | 125DG @ NE106 | Relay | Basler Electric | MIGA6PN5S3F | NE106 | Control Cabinet | DGB | 2000-00 | WCGS report | Functionally Screens |
| 214 | 127-1DG @ NE106 | Relay | GE | 12NGV23A1A | NE106 | Control Cabinet | DGB | 2000-00 | WCGS report | Functionally Screens |
| 215 | 132DG @ NE106 | Relay | GE | 290B038A09 (Type: CRN-1) (ND, NO) | NE106 | Control Cabinet | DGB | 2000-00 | GERS | Cap > Dem |
| 216 | 140DG @ NE106 | Relay | Westinghouse | 290B481A09 (Type: KLF) | NE106 | Control Cabinet | DGB | 2000-00 | SQURTS test | Functionally Screens |
| 217 | 151-127DG-A @ NE106 | Relay | GE | 12IJCV51A13A | NE106 | Control Cabinet | DGB | 2000-00 | Vendor report | Cap > Dem |
| 218 | 151-127DG-B @ NE106 | Relay | GE | 12IJCV51A13A | NE106 | Control Cabinet | DGB | 2000-00 | Vendor report | Cap > Dem |
| 219 | 151-127DG-C @ NE106 | Relay | GE | 12IJCV51A13A | NE106 | Control Cabinet | DGB | 2000-00 | Vendor report | Cap > Dem |
| 220 | 151N-DG @ NE106 | Relay | Westinghouse | 264C901A01 (Type: CO-9) | NE106 | Control Cabinet | DGB | 2000-00 | SQURTS test | Requires Resolution |
| 221 | 181DG @ NE106 | Relay | GE | 291B995A10 (Type: CF- 1) (ND, NO) | NE106 | Control Cabinet | DGB | 2000-00 | GERS | Cap > Dem |
| 222 | 186-1DG @ NE106 | Relay | GE | 12HEA61C238 | NE106 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 223 | 186-2DG @ NE106 | Relay | GE | 12HEA61B235 | NE106 | Control Cabinet | DGB | 2000-00 | EPRI HF Test | Cap > Dem |
| 224 | ESD @ NE106 | Relay | ITE/Gould | J13P3012 (Class J) | NE106 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 225 | ESX @ NE106 | Relay | ITE/Gould | J13P2012 | NE106 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 226 | UPR @ NE106 | Relay | Allen-Bradley | 700DC-R530Z1 (Type- R) | NE106 | Control Cabinet | DGB | 2000-00 | WCGS report | Functionally Screens |

| | | 7 | Table B-1 Com | ponents Identified fo | r High Fi | requency C | onfirmati | ion | | |
|-----|------------------------|-------|-----------------|--------------------------------------|-----------|--------------------|-----------|---------------|---------------------------------|-------------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 227 | 102DG @ NE107 | Relay | ABB | 293B301A16A (Type: TD-5) | NE107 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Functionally Screens |
| 228 | 124DG @ NE107 | Relay | GE | 12STV11A5A | NE107 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Requires Resolution |
| 229 | 125DG @ NE107 | Relay | Basler Electric | M1GA6PN5S3F (BEI- 25) | NE107 | Control Cabinet | DGB | 2000-00 | WCGS report | Functionally Screens |
| 230 | 127-1DG @ NE107 | Relay | GE | 12NGV13B25A | NE107 | Control Cabinet | DGB | 2000-00 | SQURTS test | Functionally Screens |
| 231 | 132DG @ NE107 | Relay | GE | 290B038A09 (Type: CRN-1) (ND, NO) | NE107 | Control Cabinet | DGB | 2000-00 | GERS | Cap > Dem |
| 232 | 140DG @ NE107 | Relay | Westinghouse | 1342D88A01 (Type: KLF) | NE107 | Control Cabinet | DGB | 2000-00 | ABB Relay Selection Guide | Cap > Dem |
| 233 | 151-127DG-A @ NE107 | Relay | GE | 12IJCV51A13A | NE107 | Control Cabinet | DGB | 2000-00 | Vendor report | Cap > Dem |
| 234 | 151-127DG-B @ NE107 | Relay | GE | 12IJCV51A13A | NE107 | Control Cabinet | DGB | 2000-00 | Vendor report | Cap > Dem |
| 235 | 151-127DG-C @ NE107 | Relay | GE | 12IJCV51A13A | NE107 | Control Cabinet | DGB | 2000-00 | Vendor report | Cap > Dem |
| 236 | 151N-DG @ NE107 | Relay | Westinghouse | 264C901A01 (Type: CO-9) | NE107 | Control Cabinet | DGB | 2000-00 | SQURTS test | Requires Resolution |
| 237 | 181DG @ NE107 | Relay | Westinghouse | 291B995A10 (Type: CF- 1) | NE107 | Control Cabinet | DGB | 2000-00 | GERS | Cap > Dem |
| 238 | 186-1DG @ NE107 | Relay | GE | 12HEA61C238 | NE107 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 239 | 186-2DG @ NE107 | Relay | GE | 12HEA61B235 | NE107 | Control Cabinet | DGB | 2000-00 | EPRI HF Test | Cap > Dem |
| 240 | ESD @ NE107 | Relay | ITE/Gould | J13P3012 (Class J) | NE107 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 241 | ESX @ NE107 | Relay | ITE/Gould | J13P2012 | NE107 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |

| | |] | Table B-1 Comp | onents Identified f | or High Fi | requency C | onfirmati | on | | |
|-----|----------------|-------|---------------------|---------------------|------------|--------------------|-----------|---------------|-----------------------------|----------------------|
| | | | Component | | Ene | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 242 | UPR @ NE107 | Relay | ITE/Gould | J13P3012 (Class J) | NE107 | Control Cabinet | DGB | 2000-00 | SQUG Advisory 2004-02 | Cap > Dem |
| 243 | K1101 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 244 | K1102 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 245 | K1117 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 246 | K1121 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 247 | K1138 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 248 | K1148 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 249 | K1149 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 250 | K1173 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 251 | K4101 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 252 | K4102 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 253 | K4117 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 254 | K4122 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 255 | K4138 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 256 | K4148 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 257 | K4149 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |

| | | Т | able B-1 Com | oonents Identified fo | or High F | requency Co | onfirmati | on | | |
|-----|------------------------|--------------------|---------------------|-----------------------|-----------|-------------------------|-----------|---------------|-----------------------|-------------------------|
| | | (| Component | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 258 | K4173 @ NF039C | Relay | Struthers & Dunn | 219BBX210 | NF039C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 259 | 151N/T @ NG00101 | Relay | GE | 12IAC53A803A | NG001 | Switchgear | CB/CC | 2000-00 | GERS | Requires Resolution |
| 260 | 52NG00101@ NG00101 | Circuit Breaker | GE | AKR5A50 | NG001 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 261 | 52NG00103 @ NG00103 | Circuit Breaker | GE | AKR5A30 | NG001 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 262 | 52NG00106@ NG00106 | Circuit Breaker | GE | AKR5A30 | NG001 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 263 | 52XX @ NG00116 | Relay | GE | HFA51A (ND-DC NC) | NG001 | Switchgear | CB/CC | 2000-00 | GERS | Functionally Screens |
| 264 | 86X/FTS @ NG00103 | Relay | GE | HMA11 (ND-DC NC) | NG001 | Switchgear | CB/CC | 2000-00 | GERS | Functionally Screens |
| 265 | 42C @ NG001AER1 | Relay | Not Available | Not Available | NG001A | Motor Control Center | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 266 | 42O @ NG001AER1 | Relay | Not Available | Not Available | NG001A | Motor Control Center | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 267 | 42C @ NG001BBR3 | Relay | Not Available | Not Available | NG001B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 268 | 42C @ NG001BDF3 | Relay | Not Available | Not Available | NG001B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 269 | 42C @ NG001BEF2 | Relay | Not Available | Not Available | NG001B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 270 | 42O @ NG001BBR3 | Relay | Not Available | Not Available | NG001B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 271 | 420 @ NG001BDF3 | Relay | Not Available | Not Available | NG001B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 272 | 420 @ NG001BEF2 | Relay | Not Available | Not Available | NG001B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 273 | 151N/T @ NG00201 | Relay | GE | 12IAC53A803A | NG002 | Switchgear | CB/CC | 2000-00 | GERS | Requires Resolution |

| | | Т | able B-1 Com | oonents Identified for | r High F | requency Co | onfirmati | ion | | |
|-----|------------------------|--------------------|---------------|------------------------|----------|-------------------------|-----------|---------------|-----------------------|-------------------------|
| | | (| Component | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 274 | 52NG00201 @ NG00201 | Circuit Breaker | GE | AKR5A50 | NG002 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 275 | 52NG00203 @ NG00203 | Circuit Breaker | GE | AKR5A30 | NG002 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 276 | 52NG00206@ NG00206 | Circuit Breaker | GE | AKR5A30 | NG002 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 277 | 52XX @ NG00216 | Relay | GE | HFA51A (ND-DC NC) | NG002 | Switchgear | CB/CC | 2000-00 | GERS | Functionally Screens |
| 278 | 86X/FTS @ NG00203 | Relay | GE | HMAII (ND-DC NC) | NG002 | Switchgear | CB/CC | 2000-00 | GERS | Functionally Screens |
| 279 | 42C @ NG002AHF3 | Relay | Not Available | Not Available | NG002A | Motor Control Center | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 280 | 42O @ NG002AHF3 | Relay | Not Available | Not Available | NG002A | Motor Control Center | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 281 | 42C @ NG002BCF2 | Relay | Not Available | Not Available | NG002B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 282 | 42C @ NG002BDF1 | Relay | Not Available | Not Available | NG002B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 283 | 420 @ NG002BCF2 | Relay | Not Available | Not Available | NG002B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 284 | 42O @ NG002BDF1 | Relay | Not Available | Not Available | NG002B | Motor Control Center | AUX | 2026-00 | WCGS report | Cap > Dem |
| 285 | 151N/T @ NG00301 | Relay | GE | 12IAC53A803A | NG003 | Switchgear | CB/CC | 2000-00 | GERS | Requires Resolution |
| 286 | 52NG00301 @ NG00301 | Circuit Breaker | GE | AKR5A50 | NG003 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 287 | 52NG00303 @ NG00303 | Circuit Breaker | GE | AKR5A30 | NG003 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 288 | 52NG00307 @ NG00307 | Circuit Breaker | GE | AKR5A30 | NG003 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 289 | 86X/FTS @ NG00303 | Relay | GE | HMA11 (ND-DC NC) | NG003 | Switchgear | CB/CC | 2000-00 | GERS | Functionally Screens |

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| | | Т | able B-1 Com | oonents Identified fo | or High F | requency Co | onfirmati | ion | | |
|-----|------------------------|--------------------|---------------|-----------------------|-----------|-------------------------|-----------|---------------|-----------------------|-------------------------|
| | | (| Component | | E | nclosure | - | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 290 | 42C @ NG003CEF4 | Relay | Not Available | Not Available | NG003C | Motor Control Center | AUX | 2047-06 | WCGS report | Cap > Dem |
| 291 | 42O @ NG003CEF4 | Relay | Not Available | Not Available | NG003C | Motor Control Center | AUX | 2047-06 | WCGS report | Cap > Dem |
| 292 | 42 @ NG003DBF6 | Relay | Not Available | Not Available | NG003D | Motor Control Center | DGB | 2000-00 | WCGS report | Cap > Dem |
| 293 | 42 @ NG003DEF4 | Relay | Not Available | Not Available | NG003D | Motor Control Center | DGB | 2000-00 | WCGS report | Cap > Dem |
| 294 | 50G @ NG003DBF6 | Relay | Gould | GRM-FC | NG003D | Motor Control Center | DGB | 2000-00 | GERS | Cap > Dem |
| 295 | 151N/T @ NG00401 | Relay | GE | 121AC53A803A | NG004 | Switchgear | CB/CC | 2000-00 | GERS | Requires Resolution |
| 296 | 52NG00401 @ NG00401 | Circuit Breaker | GE | AKR5A50 | NG004 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 297 | 52NG00403 @ NG00403 | Circuit Breaker | GE | AKR5A30 | NG004 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 298 | 52NG00407 @ NG00407 | Circuit Breaker | GE | AKR5A30 | NG004 | Switchgear | CB/CC | 2000-00 | WCGS report | Cap > Dem |
| 299 | 86X/FTS @ NG00403 | Relay | GE | HMA11 (ND-DC NC) | NG004 | Switchgear | CB/CC | 2000-00 | GERS | Functionally Screens |
| 300 | 42 @ NG004DBF6 | Relay | Not Available | Not Available | NG004D | Motor Control Center | DGB | 2000-00 | WCGS report | Cap > Dem |
| 301 | 42 @ NG004DDF3 | Relay | Not Available | Not Available | NG004D | Motor Control Center | DGB | 2000-00 | WCGS report | Cap > Dem |
| 302 | 50G @ NG004DBF6 | Relay | Gould | GRM-FC | NG004D | Motor Control Center | DGB | 2000-00 | GERS | Cap > Dem |
| 303 | 3XEF55 @ NG005ECF1 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 304 | 3XEF57@ NG005ECF1 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 305 | 42 @ NG005EFF3 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |

| | |] | Table B-1 Compo | nents Identified | for High F | requency Co | onfirmati | on | | |
|-----|-------------------------|-------|-----------------|------------------|------------|-------------------------|-----------|---------------|-----------------------|----------------------|
| | | | Component | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 306 | 42C @ NG005EDF2 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 307 | 42C @ NG005EEF3 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 308 | 42F @ NG005EDF4 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 309 | 42O @ NG005EDF2 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 310 | 42O @ NG005EEF3 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 311 | 42S @ NG005EDF4 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 312 | 62TDDEF19@ NG005ECF1 | Relay | Agastat | E7022AE004 | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 313 | CRF @ NG005EDF4 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 314 | CRS @ NG005EDF4 | Relay | Not Available | Not Available | NG005E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 315 | 3XEF56 @ NG006ECF1 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 316 | 3XEF58 @ NG006ECF1 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 317 | 42 @ NG006EFF3 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 318 | 42C @ NG006EDF2 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 319 | 42C @ NG006EEF3 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 320 | 42F @ NG006EDF4 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 321 | 42O @ NG006EDF2 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |

| | | 1 | Table B-1 Compo | nents Identified | for High F | requency Co | onfirmati | on | | |
|-----|---------------------------|-------|--------------------|------------------|------------|-------------------------|-----------|---------------|-----------------------|----------------------|
| | | | Component | | E | nclosure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 322 | 420 @ NG006EEF3 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 323 | 42S @ NG006EDF4 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 324 | 62TDDEF20 @ NG006ECF1 | Relay | Agastat | E7022AE004 | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 325 | CRF @ NG006EDF4 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 326 | CRS @ NG006EDF4 | Relay | Not Available | Not Available | NG006E | Motor Control Center | ESW | 2000-00 | WCGS report | Cap > Dem |
| 327 | ABHS0001 2/4 @ RP053AB | Relay | Foxboro Company | 2AX+DSR | RP053A | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 328 | ALHS0006 2/3 @ RP053AB | Relay | Foxboro Company | 2AX+DSR | RP053A | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 329 | ALHS0008 2/3 @ RP053AB | Relay | Foxboro Company | 2AX+DSR | RP053A | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 330 | GMTSL0001 @ RP053AC | Relay | Foxboro Company | 2AO-L2C-R | RP053A | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 331 | JELSH0001B @ RP053AC | Relay | Foxboro Company | 2AO-L2C-R | RP053A | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 332 | JELSL0001C @ RP053AC | Relay | Foxboro Company | 2AO-L2C-R | RP053A | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 333 | ABHS0004 3/5 @ RP053BB | Relay | Foxboro Company | 2AX+DSR | RP053B | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 334 | ALHS0012 2/3 @ RP053BB | Relay | Foxboro Company | 2AX+DSR | RP053B | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 335 | GMTSL0011 @ RP053BC | Relay | Foxboro Company | 2AO-L2C-R | RP053B | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 336 | JELSH0021B @ RP053BC | Relay | Foxboro Company | 2AO-L2C-R | RP053B | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 337 | JELSL0021C @ RP053BC | Relay | Foxboro Company | 2AO-L2C-R | RP053B | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |

| | | 1 | Table B-1 Com | oonents Identified fo | or High Fi | requency C | onfirmati | on | | |
|-----|---------------------------|-------|---------------------|-----------------------|------------|--------------------|-----------|---------------|-----------------------|-------------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 338 | ABHS0002 3/6 @ RP053DA | Relay | Foxboro Company | 2AX+DSR | RP053D | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 339 | ABHS0003 2/3 @ RP053DB | Relay | Foxboro Company | 2AX+DSR | RP053D | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 340 | FCHS0313 3/3 @ RP053DA | Relay | Foxboro Company | 2AX+DSR | RP053D | Control Cabinet | СВ | 2047-06 | WCGS report | Cap > Dem |
| 341 | 1XEF31 @ RP139 | Relay | Struthers & Dunn | 219BBX221 (ND, NO) | RP139 | Control Cabinet | СВ | 2000-00 | EPRI NP-7147 | Cap > Dem |
| 342 | 1XEF33 @ RP139 | Relay | Struthers & Dunn | 219BBX221 (NE, NO) | RP139 | Control Cabinet | СВ | 2000-00 | GERS | Cap > Dem |
| 343 | 1XEF35 @ RP139 | Relay | Struthers & Dunn | 219BBX221 (ND, NO) | RP139 | Control Cabinet | СВ | 2000-00 | EPRI NP-7147 | Cap > Dem |
| 344 | 62XBB001 @ RP139 | Relay | Agastat | E7022AB (ND,ALL) | RP139 | Control Cabinet | СВ | 2000-00 | GERS | Functionally Screens |
| 345 | 62XBB003 @ RP139 | Relay | Agastat | E7022AB (ND,ALL) | RP139 | Control Cabinet | CB | 2000-00 | GERS | Functionally Screens |
| 346 | 1XEF32 @ RP140 | Relay | Struthers & Dunn | 219BBX221 (ND, NO) | RP140 | Control Cabinet | CB | 2000-00 | EPRI NP-7147 | Cap > Dem |
| 347 | 1XEF34 @ RP140 | Relay | Struthers & Dunn | 219BBX221 (NE, NO) | RP140 | Control Cabinet | CB | 2000-00 | GERS | Cap > Dem |
| 348 | 1XEF36 @ RP140 | Relay | Struthers & Dunn | 219BBX221 (ND, NO) | RP140 | Control Cabinet | CB | 2000-00 | EPRI NP-7147 | Cap > Dem |
| 349 | 62XBB002 @ RP140 | Relay | Agastat | 7022 (ND, ALL) | RP140 | Control Cabinet | СВ | 2000-00 | GERS | Functionally Screens |
| 350 | 62XBB004 @ RP140 | Relay | Agastat | 7022 (ND, ALL) | RP140 | Control Cabinet | СВ | 2000-00 | GERS | Functionally Screens |
| 351 | ABHS0002 2/6 @ RP147A | Relay | Foxboro Company | 2AX+DSR | RP147A | Control Cabinet | CB | 2000-00 | WCGS report | Cap > Dem |
| 352 | FCHS0313 2/3 @ RP147A | Relay | Foxboro Company | 2AX+DSR | RP147A | Control Cabinet | СВ | 2000-00 | WCGS report | Cap > Dem |
| 353 | ABHS0004 2/5 @ RP147B | Relay | Foxboro Company | 2AX+DSR | RP147B | Control Cabinet | CB | 2000-00 | WCGS report | Cap > Dem |

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| | |] | Table B-1 Com | ponents Identified fo | r High F | requency (| onfirmat | ion | | |
|-----|--------------------------|-------|---------------------|-------------------------|----------|--------------------|----------|---------------|-----------------------|-------------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 354 | ALHS0010 2/3 @ RP147B | Relay | Foxboro Company | 2AX+DSR | RP147B | Control Cabinet | СВ | 2000-00 | WCGS report | Cap > Dem |
| 355 | 3XSJ01 @ RP209 | Relay | Struthers & Dunn | 219FXX114NE (ND, NO) | RP209 | Control Cabinet | AUX | 2000-00 | GERS | Functionally Screens |
| 356 | 3XSJ03 @ RP209 | Relay | Struthers & Dunn | 219DXB119NE (ND, NO) | RP209 | Control Cabinet | AUX | 2000-00 | GERS | Functionally Screens |
| 357 | 3XSJ05 @ RP209 | Relay | Struthers & Dunn | 219DXB119NE (NE, NC) | RP209 | Control Cabinet | AUX | 2000-00 | GERS | Cap > Dem |
| 358 | 3XSJ02 @ RP210 | Relay | Struthers & Dunn | 219FXX114 (ND, NO) | RP210 | Control Cabinet | AUX | 2026-00 | GERS | Functionally Screens |
| 359 | 3XSJ04 @ RP210 | Relay | Struthers & Dunn | 219DXB119 (ND, NO) | RP210 | Control Cabinet | AUX | 2026-00 | GERS | Functionally Screens |
| 360 | 3XSJ06 @ RP210 | Relay | Struthers & Dunn | 219DXB119NE (NE, NC) | RP210 | Control Cabinet | AUX | 2026-00 | GERS | Cap > Dem |
| 361 | 45XJE01 @ RP330 | Relay | Struthers & Dunn | 219BBX221NE (ND, NC) | RP330 | Control Cabinet | AUX | 2000-00 | GERS | Functionally Screens |
| 362 | 45XJE02 @ RP331 | Relay | Struthers & Dunn | 219BBX221NE (ND, NC) | RP331 | Control Cabinet | AUX | 2026-00 | GERS | Functionally Screens |
| 363 | 3XSJ25 @ RP332 | Relay | Struthers & Dunn | 219DXB119 (ND, NC) | RP332 | Control Cabinet | AUX | 2000-00 | GERS | Requires Resolution |
| 364 | 3XSJ27 @ RP332 | Relay | Struthers & Dunn | 219DXB119NE (NE, NO) | RP332 | Control Cabinet | AUX | 2000-00 | GERS | Cap > Dem |
| 365 | 3XSJ31 @ RP332 | Relay | Struthers & Dunn | 219FXX114 (ND, NO) | RP332 | Control Cabinet | AUX | 2000-00 | GERS | Functionally Screens |
| 366 | 3XSJ33 @ RP332 | Relay | Struthers & Dunn | 219DXB119NE (ND, NC) | RP332 | Control Cabinet | AUX | 2000-00 | GERS | Requires Resolution |
| 367 | 3XSJ35 @ RP332 | Relay | Struthers & Dunn | 219DXB119NE (NE, NO) | RP332 | Control Cabinet | AUX | 2000-00 | GERS | Cap > Dem |
| 368 | 62TDENB01 @ RP332 | Relay | Struthers & Dunn | 236ABX139-NE | RP332 | Control Cabinet | AUX | 2000-00 | SQURTS test | Functionally Screens |
| 369 | 62TDENB02 @ RP332 | Relay | Struthers & Dunn | 236ABX139-NE | RP332 | Control Cabinet | AUX | 2000-00 | SQURTS test | Functionally Screens |

| | |] | Table B-1 Comp | onents Identified fo | r High Fi | requency C | onfirmati | ion | | |
|-----|----------------------|-------|---------------------|-------------------------|-----------|--------------------|-----------|---------------|-----------------------|-------------------------|
| | | | Component | | End | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 370 | 3XSJ26 @ RP333 | Relay | Struthers & Dunn | 219DXB119 (ND, NC) | RP333 | Control Cabinet | AUX | 2026-00 | GERS | Requires Resolution |
| 371 | 3XSJ28 @ RP333 | Relay | Struthers & Dunn | 219DXB119NE (NE, NO) | RP333 | Control Cabinet | AUX | 2026-00 | GERS | Cap > Dem |
| 372 | 3XSJ32 @ RP333 | Relay | Struthers & Dunn | 219FXX114 (ND, NO) | RP333 | Control Cabinet | AUX | 2026-00 | GERS | Functionally Screens |
| 373 | 3XSJ34 @ RP333 | Relay | Struthers & Dunn | 219DXB119NE (ND, NC) | RP333 | Control Cabinet | AUX | 2026-00 | GERS | Requires Resolution |
| 374 | 3XSJ36 @ RP333 | Relay | Struthers & Dunn | 219DXB119NE (NE, NO) | RP333 | Control Cabinet | AUX | 2026-00 | GERS | Cap > Dem |
| 375 | 62TDENB03 @ RP333 | Relay | Struthers & Dunn | 236ABX139-NE | RP333 | Control Cabinet | AUX | 2026-00 | SQURTS test | Functionally Screens |
| 376 | 62TDENB04 @ RP333 | Relay | Struthers & Dunn | 236ABX139-NE | RP333 | Control Cabinet | AUX | 2026-00 | SQURTS test | Functionally Screens |
| 377 | 86XRP1 @ RP334 | Relay | Electroswitch | 7828GD | RP334 | Control Cabinet | СВ | 2000-00 | Vendor report | Cap > Dem |
| 378 | 86XRP2 @ RP334 | Relay | Electroswitch | 7828GD | RP334 | Control Cabinet | СВ | 2000-00 | Vendor report | Cap > Dem |
| 379 | 86XRP3 @ RP334 | Relay | Electroswitch | 7828GD | RP334 | Control Cabinet | СВ | 2000-00 | Vendor report | Cap > Dem |
| 380 | K122 @ SA036A | Relay | Struthers & Dunn | 219 Series (ND, NO) | SA036A | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 381 | K142 @ SA036A | Relay | Struthers & Dunn | 219 Series (ND, NO) | SA036A | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 382 | K151 @ SA036B | Relay | Struthers & Dunn | 219 Series (ND, NO) | SA036B | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 383 | K101 @ SA036C | Relay | Struthers & Dunn | 219 Series (ND, NC) | SA036C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 384 | K102 @ SA036C | Relay | Struthers & Dunn | 219 Series (ND, NC) | SA036C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 385 | K103 @ SA036C | Relay | Struthers & Dunn | 219 Series (ND, NO) | SA036C | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |

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| | |] | Fable B-1 Compo | nents Identified | for High Fr | equency (| Confirmati | ion | | |
|-----|---------------|-------|------------------------|------------------|-------------|--------------------|------------|---------------|-----------------------|----------------------|
| | | | Component | | En | closure | | Floor | Componen | t Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 386 | K118 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 387 | K119 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 388 | K131 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 389 | K133 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 390 | K134 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 391 | K137 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 392 | K141 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 393 | K154 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 394 | K156 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 395 | K161 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 396 | K201 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 397 | K203 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 398 | K204 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 399 | K216 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 400 | K217 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 401 | K224 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |

| | | 7 | Fable B-1 Compo | nents Identified | for High Fr | equency C | onfirmati | ion | | |
|-----|---------------|-------|------------------------|------------------|-------------|--------------------|-----------|---------------|-----------------------|----------------------|
| | | 1 | Component | | Enc | closure | | Floor | Componen | t Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 402 | K247 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 403 | K248 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 404 | K256 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 405 | K317 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 406 | K318 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 407 | K324 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 408 | K329 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 409 | K330 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 410 | K344 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 411 | K356 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 412 | K417 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 413 | K418 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 414 | K429 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 415 | K430 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 416 | K435 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 417 | K444 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |

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| | |] | Fable B-1 Compo | nents Identified | for High Fr | equency C | onfirmati | ion | | |
|-----|---------------|-------|------------------------|------------------|-------------|--------------------|-----------|---------------|-----------------------------|----------------------|
| | | | Component | | Enc | losure | | Floor | Componen | t Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 418 | K456 @ SB029A | Relay | Midtex/Aemco | 156-14C300 | SB029A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 419 | K505 @ SB029C | Relay | Midtex/Aemco | 156-14D200 | SB029C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 420 | K519 @ SB029C | Relay | Midtex/Aemco | 156-14D200 | SB029C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 421 | K521 @ SB029C | Relay | Midtex/Aemco | 156-14D200 | SB029C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 422 | K522 @ SB029C | Relay | Midtex/Aemco | 156-14D200 | SB029C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 423 | K525 @ SB029C | Relay | Midtex/Aemco | 156-14D200 | SB029C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 424 | K526 @ SB029C | Relay | Midtex/Aemco | 156-14D200 | SB029C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 425 | K527 @ SB029C | Relay | Midtex/Aemco | 156-14D200 | SB029C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 426 | K602 @ SB029C | Relay | Potter & Brumfield | MDR 4103-1 | SB029C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 427 | K609 @ SB029C | Relay | Potter & Brumfield | MDR 4103-1 | SB029C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 428 | K615 @ SB029C | Relay | Potter & Brumfield | MDR 4103-1 | SB029C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 429 | K617 @ SB029C | Relay | Potter & Brumfield | MDR 4103-1 | SB029C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 430 | K629 @ SB029C | Relay | Potter & Brumfield | MDR 4103-1 | SB029C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 431 | K631 @ SB029C | Relay | Potter & Brumfield | MDR 4103-1 | SB029C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 432 | K645 @ SB029C | Relay | Potter & Brumfield | MDR 4103-1 | SB029C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory | Cap > Dem |

| | | 7 | Table B-1 Compo | nents Identified | for High Fr | equency C | onfirmati | on | | |
|-----|---------------|-------|-----------------------|------------------|-------------|--------------------|-----------|---------------|-----------------------------|----------------------|
| | | | Component | | End | losure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| | | | | | | | | | 2004-02 | |
| 433 | K713 @ SB029D | Relay | Potter & Brumfield | MDR 4103-1 | SB029D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 434 | K734 @ SB029D | Relay | Potter & Brumfield | MDR 4103-1 | SB029D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 435 | K750 @ SB029D | Relay | Potter & Brumfield | MDR 4103-1 | SB029D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 436 | K751 @ SB029D | Relay | Potter & Brumfield | MDR 4103-1 | SB029D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 437 | K752 @ SB029D | Relay | Potter & Brumfield | MDR 4103-1 | SB029D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 438 | K811 @ SB030A | Relay | Potter & Brumfield | MDR 66-4 | SB030A | Control Cabinet | CB | 2047-06 | WCGS report | Cap > Dem |
| 439 | K118 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 440 | K119@SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 441 | K131 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 442 | K133 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 443 | K134 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 444 | K137 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 445 | K141 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 446 | K156 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |

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| - | |] | Table B-1 Compo | nents Identified | for High Fr | requency C | onfirmati | on | | |
|-----|---------------|-------|-----------------|------------------|-------------|--------------------|-----------|---------------|-----------------------|----------------------|
| | | | Component | | End | closure | | Floor | Componen | t Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 447 | K161 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 448 | K201 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 449 | K203 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 450 | K204 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 451 | K216 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 452 | K217 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 453 | K224 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 454 | K247 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 455 | K248 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 456 | K254 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 457 | K256 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 458 | K317 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 459 | K318 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 460 | K324 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 461 | K329 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 462 | K330 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |

| | | 1 | Table B-1 Compo | nents Identified | for High Fr | equency C | onfirmati | on | | |
|-----|---------------|-------|-----------------|------------------|-------------|--------------------|-----------|---------------|-----------------------|----------------------|
| | | | Component | | Enc | losure | | Floor | Componen | t Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 463 | K344 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 464 | K356 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 465 | K417 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 466 | K418 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 467 | K429 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 468 | K430 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 469 | K435 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 470 | K444 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 471 | K456 @ SB032A | Relay | Midtex/Aemco | 156-14C300 | SB032A | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 472 | K217 @ SB032C | Relay | Midtex/Aemco | 156-14C300 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 473 | K330 @ SB032C | Relay | Midtex/Aemco | 156-14C300 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 474 | K430 @ SB032C | Relay | Midtex/Aemco | 156-14C300 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 475 | K502 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 476 | K505 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 477 | K519 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 478 | K521 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |

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| | | 1 | Fable B-1 Compo | nents Identified | for High Fr | equency (| onfirmati | ion | | |
|-----|---------------|-------|------------------------|------------------|-------------|--------------------|-----------|---------------|-----------------------------|----------------------|
| | | | Component | | End | closure | | Floor | Componen | t Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 479 | K522 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 480 | K525 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 481 | K526 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 482 | K527 @ SB032C | Relay | Midtex/Aemco | 156-14D200 | SB032C | Control Cabinet | CB/CC | 2047-06 | GERS | Cap > Dem |
| 483 | K602 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 484 | K609 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 485 | K615 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 486 | K617 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 487 | K629 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 488 | K630 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 489 | K631 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 490 | K645 @ SB032C | Relay | Potter & Brumfield | MDR 4103-1 | SB032C | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 491 | K713 @ SB032D | Relay | Potter & Brumfield | MDR 4103-1 | SB032D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 492 | K734 @ SB032D | Relay | Potter & Brumfield | MDR 4103-1 | SB032D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |

| | |] | Table B-1 Compo | nents Identified | for High Fr | equency C | onfirmati | on | | |
|-----|--------------------|-------|-----------------------|------------------|-------------|--------------------|-----------|---------------|-----------------------------|----------------------|
| | | | Component | | Enc | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 493 | K750 @ SB032D | Relay | Potter & Brumfield | MDR 4103-1 | SB032D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 494 | K751 @ SB032D | Relay | Potter & Brumfield | MDR 4103-1 | SB032D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 495 | K752 @ SB032D | Relay | Potter & Brumfield | MDR 4103-1 | SB032D | Control Cabinet | CB/CC | 2047-06 | SQUG Advisory 2004-02 | Cap > Dem |
| 496 | K811 @ SB033A | Relay | Potter & Brumfield | MDR 66-4 | SB033A | Control Cabinet | CB | 2047-06 | WCGS report | Cap > Dem |
| 497 | PS/457D @ SB037 | Relay | Westinghouse | 739B194H01 | SB037 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 498 | PS/457E @ SB037 | Relay | Westinghouse | 739B194H01 | SB037 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 499 | PS/526A @ SB037 | Relay | Westinghouse | 739B194H01 | SB037 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 500 | PS/536A @ SB037 | Relay | Westinghouse | 739B194H01 | SB037 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 501 | PS/935A @ SB037 | Relay | Westinghouse | 739B194H01 | SB037 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 502 | PS/935B @ SB037 | Relay | Westinghouse | 739B194H01 | SB037 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 503 | PS/405A @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 504 | PS/405E @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 505 | PS/455D @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 506 | PS/455E @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 507 | PS/514A @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |

| | |] | Fable B-1 Compo | nents Identified | for High F | requency C | onfirmati | on | | |
|-----|--------------------|-------|------------------------|------------------|------------|--------------------|-----------|---------------|-----------------------|----------------------|
| | | | Component | | En | closure | | Floor | Component | Evaluation |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Canacity | Evaluation Result |
| 508 | PS/524A @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 509 | PS/534A @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 510 | PS/544A @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 511 | PS/937A @ SB038 | Relay | Westinghouse | 739B194H01 | SB038 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 512 | PS/458D @ SB041 | Relay | Westinghouse | 739B194H01 | SB041 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 513 | PS/458E @ SB041 | Relay | Westinghouse | 739B194H01 | SB041 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 514 | PS/516A @ SB041 | Relay | Westinghouse | 739B194H01 | SB041 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 515 | PS/546A @ SB041 | Relay | Westinghouse | 739B194H01 | SB041 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 516 | PS/934A @ SB041 | Relay | Westinghouse | 739B194H01 | SB041 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 517 | PS/934B @ SB041 | Relay | Westinghouse | 739B194H01 | SB041 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 518 | PS/403A @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 519 | PS/403E @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 520 | PS/456D @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 521 | PS/456E @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 522 | PS/515A @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 523 | PS/525A @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |

| | |] | Table B-1 Compo | nents Identified | for High Fi | requency C | onfirmati | on | | |
|-----|--------------------|-------|-----------------|------------------|-------------|--------------------|-----------|---------------|-----------------------|----------------------|
| | Component | | | | | Enclosure | | Floor | Component Evaluation | |
| No. | Device ID | Туре | Manufacturer | Model | ID | Туре | Building | Elev. (ft) | Basis for Capacity | Evaluation Result |
| 524 | PS/535A @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 525 | PS/545A @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 526 | PS/936A @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |
| 527 | PS/936B @ SB042 | Relay | Westinghouse | 739B194H01 | SB042 | Control Cabinet | CB/CC | 2047-06 | WCGS report | Cap > Dem |