



International Agreement Report

Transient Analysis of the Research Reactor MARIA MC Fuel Elements Using RELAP5 Mod 3.3

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ABSTRACT

The new fuel type in the Research Reactor 'Maria' is undergoing a test procedure. Thermal-hydraulic calculations using RELAP have been applied in order to cross-check the results obtained using a specialized thermal-hydraulic 'SN' code. Nodalization of the fuel element has been developed and calculations have been performed. LOFA and RIA cases have been analysed and compared showing good agreement between the two codes.

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EXECUTIVE SUMMARY

In accordance with the international agreement on GTRI (Global Threat Reduction Initiative) Poland agreed to change the fuel type in the MARIA research reactor in Świerk from Highly Enriched Uranium (HEU) fuel to Low Enriched Uranium fuel (LEU). The new fuel MC5-485 – in short MC fuel - consists of 19,75% of ²³⁵U. At this stage several new MC elements have been inserted into the reactor core and are under a test procedure.

Prior to this test, thermal-hydraulic effects have been calculated by the operator using a specialized computer code called 'SN'. The SN code is capable of performing thermal-hydraulic calculations of the fuel elements behaviour and has been verified and validated for the research reactor MARIA only.

The Polish National Atomic Energy Agency (PAA) has decided to try to cross-check the results of the analysis using the RELAP5 code although it is aware that the results of the analysis at this stage might need further elaboration and additional calculations. However an important aim is to gain experience in performing analysis using RELAP5 and to judge whether it is applicable and to what extent to the analysis of the research reactor.

The National Centre for Nuclear Research who is the operator of the research reactor MARIA has provided the results of two types of accidents: a Reactivity Initiated Accident (RIA) and Loss of Flow Accident (LOFA). The analysis of RIA was divided into four scenarios: two for reactor low power level operation (possible during start-up of the reactor or during work with low power level – 10 kW) and two for normal operation with maximum allowed power. Both cases were performed for slow and fast reactivity insertion. The SN code models the fuel element only. It does not include the possibility to model the whole reactor together with the safety systems. As a consequence of this limitation no analyses of the Loss Of Coolant Accident (LOCA) have been supplied as yet. Using RELAP should change this and enable the regulatory body to perform a LOCA analysis as well.

The Regulatory Body has cross checked the analyses made and presented by the operator and has provided the comparison of results in this report. Due to other limitations of the SN code, the comparison is rather limited. Only a small number of parameters is included in the SN output. Thus, only those could be compared.

The presented results of calculations do not include errors and sensitivity studies. However the scenario analysed for the purpose of this document was made with conservative assumptions. The model used for this calculation was limited to a model of the fuel element only. Other elements of the reactor systems were not included. As a consequence it was necessary to:

- omit influence of reactivity coefficients of the coolant in reactor pool and beryllium blocks positioned around the analysed fuel channel; the omitted thermal reactivity coefficients are positive but during postulated accidents, the increase of the temperature of the beryllium blocks and water of pool is very low,
- omit heat transfer between the fuel channel and water of the reactor pool; the influence of this factor is very small due to the very small difference in temperatures between

water in the outer part of the fuel channel and the water in the pool (i.e. heated water flows in the internal part of fuel channel).

Following an introduction in chapter 1, the report covers a short description of the Research Reactor 'Maria' including the fuel channel and the fuel element presented in chapter 2. Additional information concerning the RR Maria is supplied in Appendix A.

The nodalization model is presented in chapter 3 and includes a description of the fuel channel and heat structures. The input data file is attached in Appendix B.

The results of the calculations are presented in chapter 4 mostly on figures. They begin with the steady state evaluation which is followed by a loss of flow in the fuel channel analysis. Further analyses cover the slow reactivity insertion accident on low power level, fast reactivity insertion accident on low power level, slow reactivity insertion accident during reactor normal operation and finally fast reactivity insertion accident during reactor normal operation. In chapter 5 a brief information on run statistics is presented.

Finally a summary of the results is presented in chapter 6.

As already mentioned, initial calculations were performed for steady-state conditions. The newly created model of the reactor with the new fuel elements for RELAP was used and compared with the results of steady state calculations received from the SN code. The limitations of the SN code does not allow to perform detailed comparisons however peak cladding temperatures and heat flux were compared.

The steady state was calculated for the reactor normal operation deviated from full power.

The conditions that were used in the simulation were chosen to simulate work of the fuel channel during normal operation with safety parameters equal to warning signals. In order to have such conditions the mass flow was reduced to 90% of nominal value and thermal power was increased to 110% of the nominal value.

The results received were satisfactory.

Loss of flow in the fuel channel cooling system is possible in case of the loss of power in the pump system. As a result a sudden decrease of pressure occurs in the cooling channel that leads to the initiation of the emergency signal and shutdown of the reactor. Furthermore, after the loss of flow a rapid increase of fuel clad temperature and cooling temperature in gaps between fuel pipes occurs. According to the scenario a few seconds after the loss of power in the pump system, the work of a backup pump should be initiated powered by accumulator batteries however operating at a lower speed – 1500 r/s. After the reactor shutdown and before the flow is stabilized another small temperature jump can be detected.

The highest outer clad temperature calculated with the RELAP5 code was 432K (outer layer temperature – 440K). The temperature calculated with the SN code was 433.4K. Both codes calculated the highest temperature in the same place – on the internal side of pipe number 6.

In case when the operator undertakes incorrect actions or a malfunction of the reactivity regulation system occurs, it is possible that as a result, positive reactivity is inserted into the core with the maximum reactivity speed 0.04\$/s. This scenario was checked for low power level conditions. This scenario has the lowest impact on the fuel elements. The temperature peaks of

water and clad are very small - smaller than fluctuations of temperature during normal operation of the reactor.

One of the important scenarios addressed in the supplementary document is the fast inflow of cold water into the core resulting in a sudden increase of reactivity. The negative reactivity coefficients lead to the increase of power in the fuel elements. The scenario analysis was performed for low power. The results received were satisfactory.

The slow reactivity insertion accident during normal operation was very similar to the slow reactivity insertion accident on low power. Also here the results were satisfactory.

A break of control rods is another scenario analysed. The break of control rods leads to fast insertion of positive reactivity into the reactor. It is assumed that the maximum insertion of positive reactivity is equal to 1.5\$ with the top speed of insertion 4\$/s.

The main differences in the results between RELAP and the SN code are due to the different models of reactor kinetics. RELAP5 uses the point kinetic model and this model was applied to the RIA analysis. In case of the SN code a more pessimistic model was used.

Summarizing the analysed cases it can be stated that most of the results of the simulation for the research reactor MARIA obtained using the RELAP5 code, showed that there are no big differences between the results achieved by the validated SN and the RELAP5 codes. Only in one case (RIA with fast reactivity insertion with maximum power level) there is the opportunity to exceed the lowest allowed level of the ONBR parameter. Exceeding this parameter can cause the onset of boiling of the coolant in the gap between the fuel pipes. In the analysed case, the duration of time when ONBR is lower than 1.2 is very short (about 0.35s) and should not cause any damage to the fuel and clad material. In the fast RIA scenario, the power jump during the insertion of positive reactivity was stopped by the negative reactivity coefficients (fuel and coolant) before insertion of the safety and control rods into the core could be initiated.

In other simulated scenarios, no opportunity to exceed the ONBR parameter or temperature limit of clad – 452K occurred.

In the analysed LOFA scenario, the calculations showed that enough cooling capability is provided even when only one pump is working with a lower rotation speed than the normally required two pumps.

The content of this report does not cover all possible accident conditions that should be analysed for the research reactor. Further analysis will be necessary. A comparison of the SN and RELAP5 codes showed that RELAP5 can be used in the safety analysis for the research reactor MARIA.

ABBREVIATIONS

ECEP	external side of clad on the external side of pipe
ECIP	external side of clad on the internal side of pipe
HEU	highly enriched Uranium
ICEP	internal side of clad on the external side of pipe
ICIP	internal side of clad on the internal side of pipe
LEU	Low enriched Uranium
LOFA	Loss of Flow Accident
NCBJ	Narodowe Centrum Badań Jądrowych (National Centre for Nuclear Research)
ONBR	Onset of Nucleate Boiling Ratio
PAA	Państwowa Agencja Atomistyki (National Atomic Energy Agency of Poland)
PAR	automatic regulation rod
PK	control rods
PB	safety rods
REP	moving type fuel elements
RIA	Reactivity Initiated Accident
RR	research reactor
SN	name of computer code used for RR 'Maria' calculations

1 INTRODUCTION

Fulfilling the international agreement on GTRI (Global Threat Reduction Initiative) Poland agreed to change the fuel type in the MARIA research reactor in Świerk from Highly Enriched Uranium (HEU) fuel to Low Enriched Uranium fuel (LEU). The new fuel MC5-485 consists of 19,75% ²³⁵-U. At this stage several new MC elements have been inserted into the reactor core and are under a test procedure.

Prior to this test, thermal-hydraulic effects have been calculated by the operator using a specialized computer code called 'SN'. The SN code is capable of performing thermal-hydraulic calculations of the fuel elements behaviour and has been verified and validated for the research reactor MARIA only.

The Polish National Atomic Energy Agency (PAA) has decided to try to cross-check the results of the analysis using the RELAP5 code although it is aware that the results of the analysis at this stage might need further elaboration and additional calculations. However an important aim is to gain experience in performing analysis using RELAP5 and to judge whether it is applicable and to what extent to the analysis of the research reactor.

The National Centre for Nuclear Research who is the operator of the research reactor MARIA has provided the results of two types of accidents: a Reactivity Initiated Accident (RIA) and Loss of Flow Accident (LOFA). The results of the analyses are part of a supplementary document¹ to the Safety Analysis Report. The analysis of RIA was divided into four scenarios: two for reactor low power level operation (possible during start-up of the reactor or during work with low power level – 10 kW) and two for normal operation with maximum allowed power. Both cases were performed for slow and fast reactivity insertion. The SN code models the fuel element only. It does not include the possibility to model the whole reactor together with the safety systems. As a consequence of this limitation no analyses of the Loss Of Coolant Accident (LOCA) have been supplied as yet. Using RELAP should change this and enable the regulatory body to perform a LOCA analysis as well.

The Regulatory Body has cross checked the analyses made and presented by the operator in the supplementary document and has provided the comparison of results in this report. Due to other limitations of the SN code, the comparison is rather limited. Only a small number of parameters is included in the SN output. Thus, only those could be compared.

1 Aneks 2012/1 do Eksploatacyjnego Raportu Bezpieczeństwa Reaktora MARIA Konwersja rdzenia reaktora MARIA na paliwo MC, July 2012.

2 FACILITY DESCRIPTION

2.1 MARIA research reactor technical information

The Maria research reactor is a pool type research reactor with 20-25 closed fuel channels in the core, with a beryllium moderator and graphite reflector. The designed maximum thermal power is 30 MW. The reactor is placed about 30 km from Warsaw in Świerk-Otwock and is operated by the National Centre for Nuclear Research (NCBJ). More technical information including a description of the primary safety systems is provided in Appendix A.

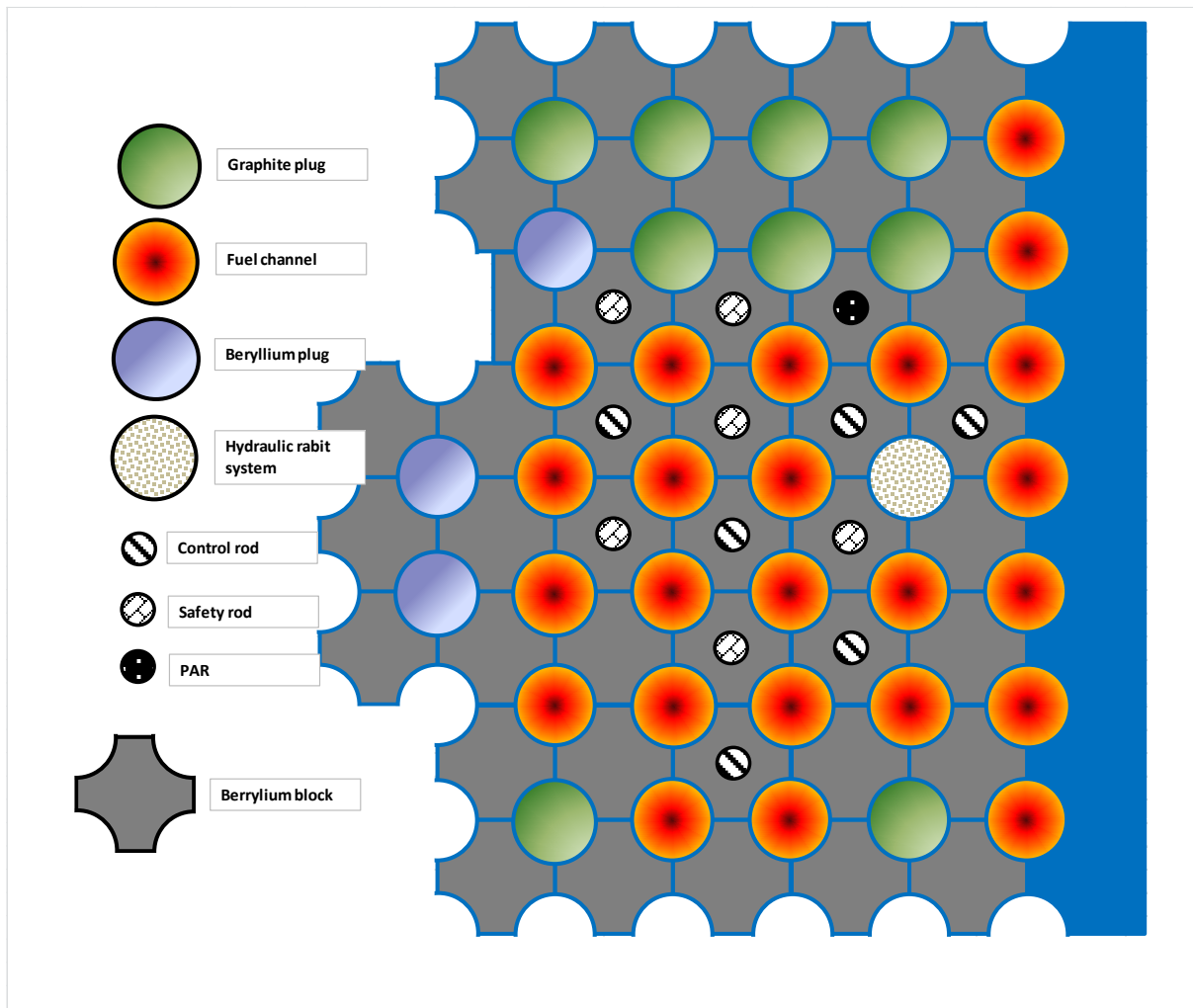


Figure 1. Simplified scheme of the Research Reactor 'MARIA' core configuration

2.2 Fuel channel with fuel element technical information:

This report assumes that only the new type of fuel – the French LEU fuel MC5-485 with 19.75% of ^{235}U is used. The fuel element is a pipe in pipe construction, consisting of 5 pipes with fuel (Fig.2 with numbers from 2 to 6) and filler. The fuel is a dispersion $\text{U}_3\text{Si}_2\text{-Al}$ with AG3NE alloy as a clad material and SAW alloy (aluminium alloy type) as an outer tube of the fuel channel. Water in the fuel element flows through 6 gaps (numbered from 1 to 6 on the picture) and through a gap in the centre of the fuel element. Fuel elements work with various thermal power levels depending on the position in the core. Usually, fuel elements work in the centre of the core with thermal power at the level of about 1.2-1.6 MW and in the peripheral position of the core with power about 0.3-1.2 MW. The maximum allowed thermal power – the safety limit for this fuel is 1.8 MW and it is forbidden for the reactor to exceed the limit in any conditions.

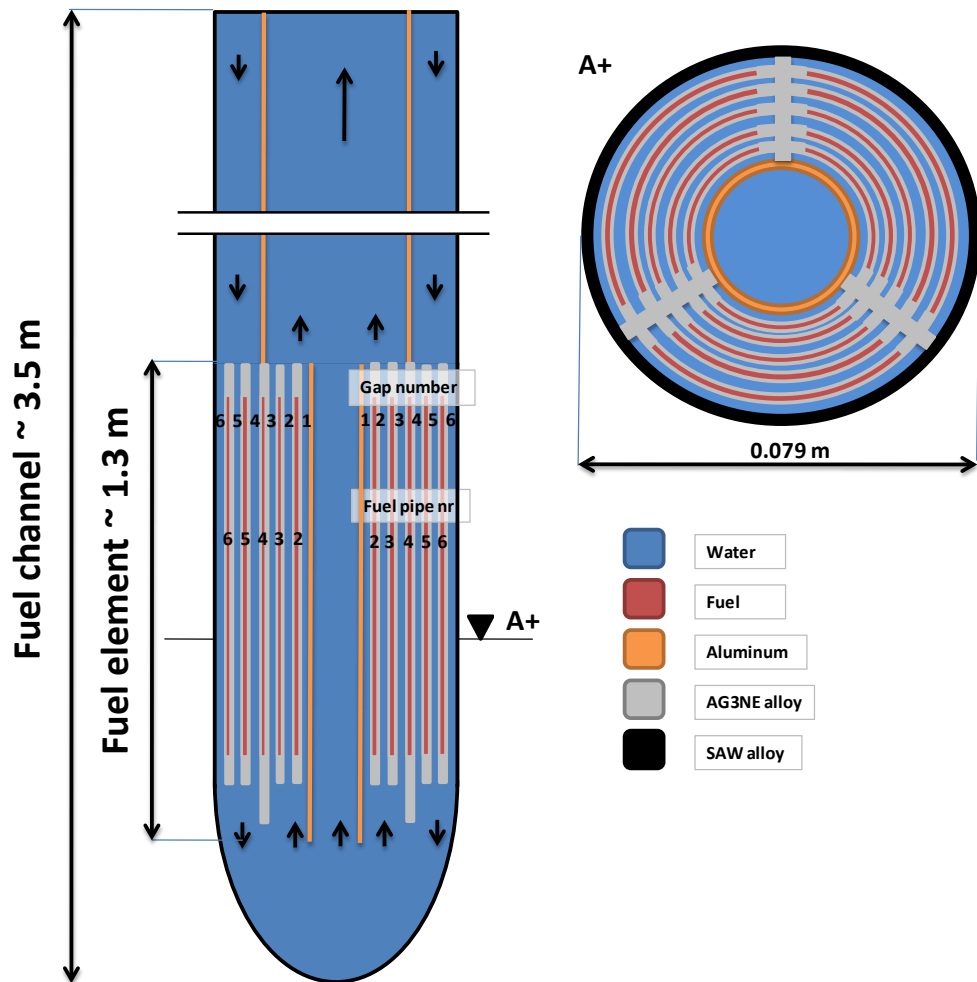


Figure 2. Simplified scheme of the fuel channel with an MC fuel element

3 CODE INPUT AND MODEL DESCRIPTION

3.1 Nodalization

In order to cross-check the analysis it was necessary to prepare a model of the fuel channel with a fuel element consisting of 5 fuel pipes and a bypass in centre. The nodalization is presented on Fig.3. Water flowing in the channel is directed first to the outer part of channel (component 10), then split into three gaps between fuel pipes (components 20, 25 and 30). Next, the water mixes and changes direction of flow (in component 35, 40 and 45) and goes up through the rest of the gaps and bypass (components 50, 55, 60 and 80). Next, the water flows to the exit of the channel through the inner part of the channel (component 70).

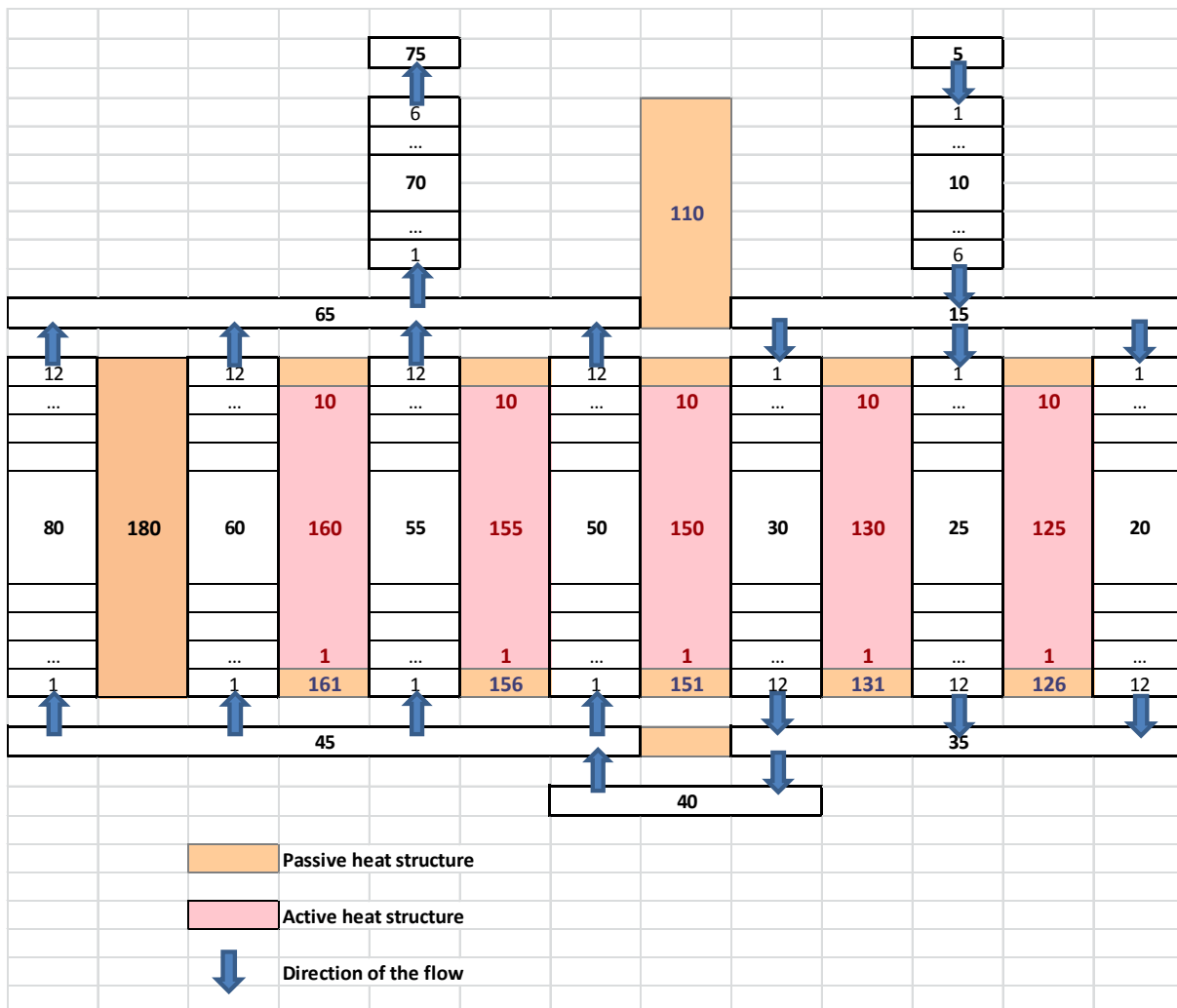


Figure 3. Nodalization scheme of the MC fuel element.

3.2 Heat structures

Two types of heat structures - active and passive were used for modelling heat exchange. Passive heat structures without heat generation are used for modelling heat transfer between the outer and inner part of the fuel channel (node no. 110 on Figure 3), non-filled fuel pipe parts (161, 156, 151, 131, 126) and filler (180). Active heat structures are used for modelling fuel pipes with heat generation (160, 155, 150, 130, 125 consisting of 10 cells). Each cell in the active heat structure was divided into 17 meshes as is visualised on Figure 4. In case of passive structures each cell was divided into less than 10 meshes.

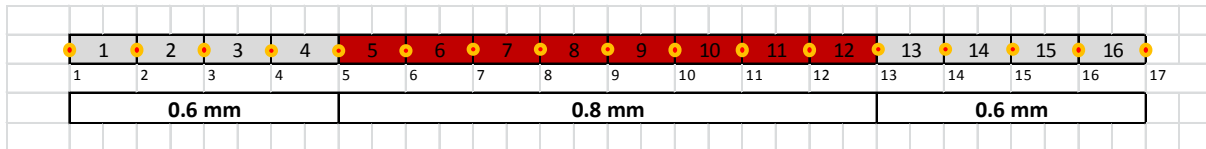


Figure 4. Positioning of mesh points in each fuel pipe – grey colour clad material, red colour - fuel

For the purpose of this document it was required to check the temperature in four points:
External side of Clad on the Internal side of Pipe (ECIP) – mesh nr 1,
Internal side of Clad on the Internal side of Pipe (ICIP) – mesh nr 5,
Internal side of Clad on the External side of Pipe (ICEP) – mesh nr 13,
External side of Clad on the External side of Pipe (ECEP) – mesh nr 17.
The placement of the four points is shown on Figure 5.

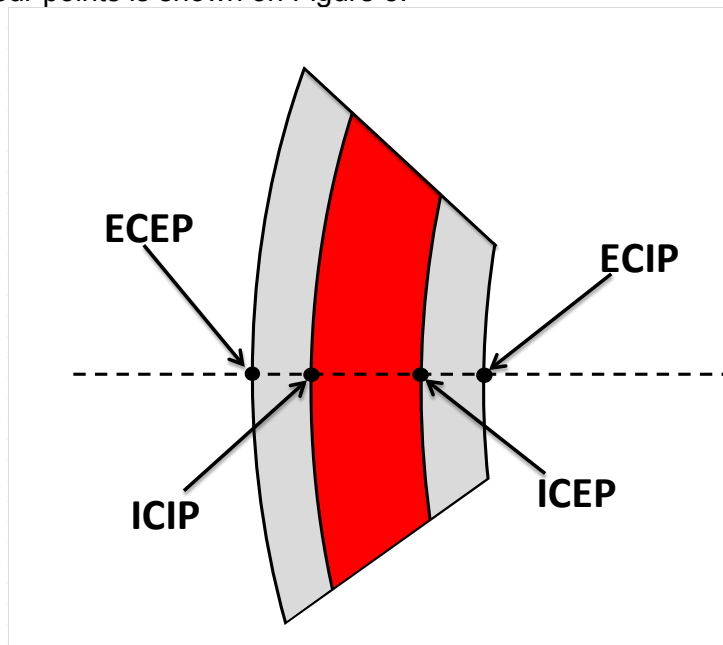


Figure 5. Placement of measurement points

The heat generation distribution model was based on two factors: (1) heat generation in each

pipe calculated by the computer code MCNP² and (2) axial heat generation based on the cosine model with a slight shift downwards in order to simulate partial insertion of control rods into the core during operation.

Table 1. Distribution of heat generation on fuel pipes and comparison of heat generation with content of uranium

Pipe	Heat generation [%]	Mass of U-235 [%]
2	11.0	11.15
3	14.1	15.58
4	18.1	20.00
5	23.8	24.43
6	33.0	28.84

3.3 Limitation of the model and errors

A model of the analysed objects, as well as data and calculations should always include an errors analysis that influence the final results. However the scenario analysed for the purpose of this document was made with conservative assumptions in the initial condition and did not include the influence of errors and sensitivity studies. The model used for this calculation was limited to a model of the fuel element only. Other elements of the reactor systems were not included. As a consequence it was necessary to:

- omit influence of reactivity coefficients of the coolant in reactor pool and beryllium blocks positioned around the analysed fuel channel; the omitted thermal reactivity coefficients are positive but during postulated accidents, the increase of the temperature of the beryllium blocks and water of pool is very low,
- omit heat transfer between the fuel channel and water of the reactor pool; the influence of this factor is very small due to the very small difference in temperatures between water in the outer part of the fuel channel and the water in the pool (i.e. heated water flows in the internal part of fuel channel).

² Calculated by NCBJ in document: *Aneks 2009/1 do Eksploatacyjnego Raportu Bezpieczeństwa Reaktora MARIA Badania paliwa MC*

4 RESULTS

4.1 Steady state evaluation

Initial calculations were performed for steady-state conditions. The newly created model of the reactor with the new fuel elements for RELAP was used and compared with the results of steady state calculations received from the SN code. The limitations of the SN code do not allow to perform detailed comparisons, however peak cladding temperatures and heat flux were compared.

The steady state was calculated for the reactor normal operation deviated from full power.

Steady-state conditions

The conditions that were used in the simulation were chosen to simulate work of the fuel channel during normal operation with safety parameters equal to warning signals. In order to have such conditions the mass flow was reduced to 90% of nominal value and thermal power was increased to 110% of the nominal value.

Initial conditions:

- Cooling channel inlet water temperature $T_{in}=318.15K$
- Mass flow $Q=7.43kg/s$ ($27m^3/h$ for density of water: $990kg/m^3$) (90% of nominal mass flow)
- Pressure at the fuel channel inlet $p=1.7MPa$
- Fuel channel pressure drop $\Delta p=0.59MPa$
- Fuel element thermal power 1.98MW (110% of nominal value)

Results

Temperature distribution on fuel pipes

The results of calculations are presented on the following figures – from Figure 6 to Figure 13.

The temperature distribution on the internal side of the fuel pipe as below:

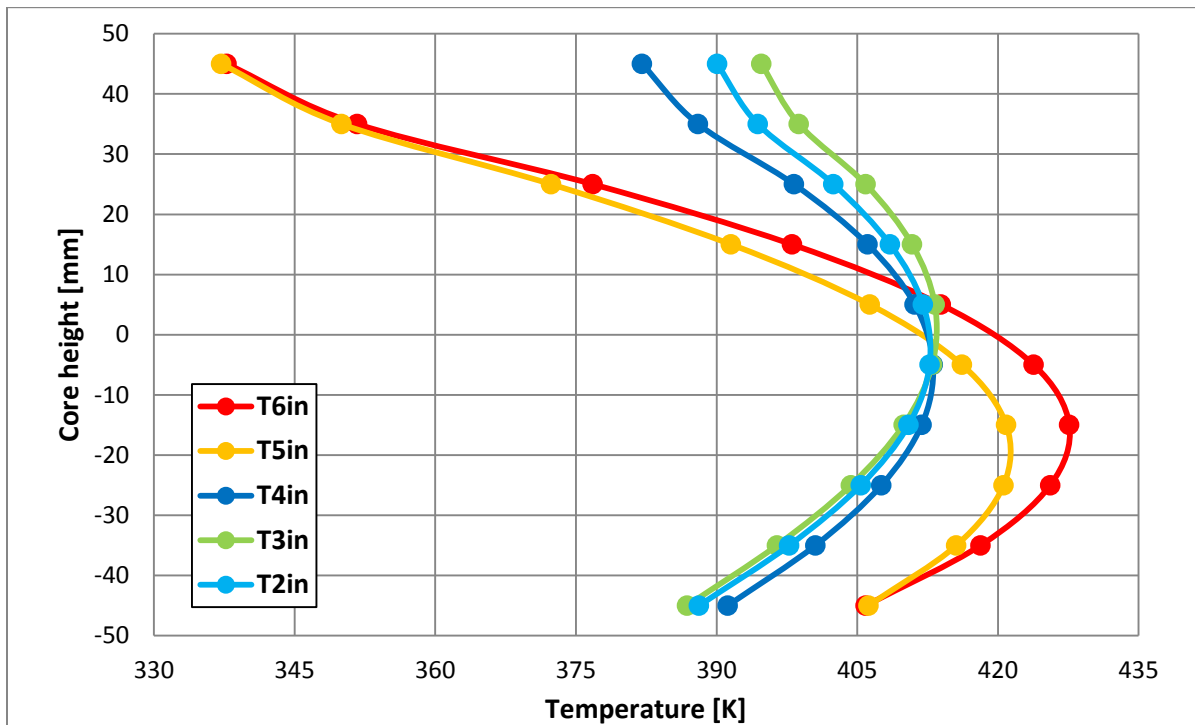


Figure 6. Temperature distribution on ICIP of each fuel pipe

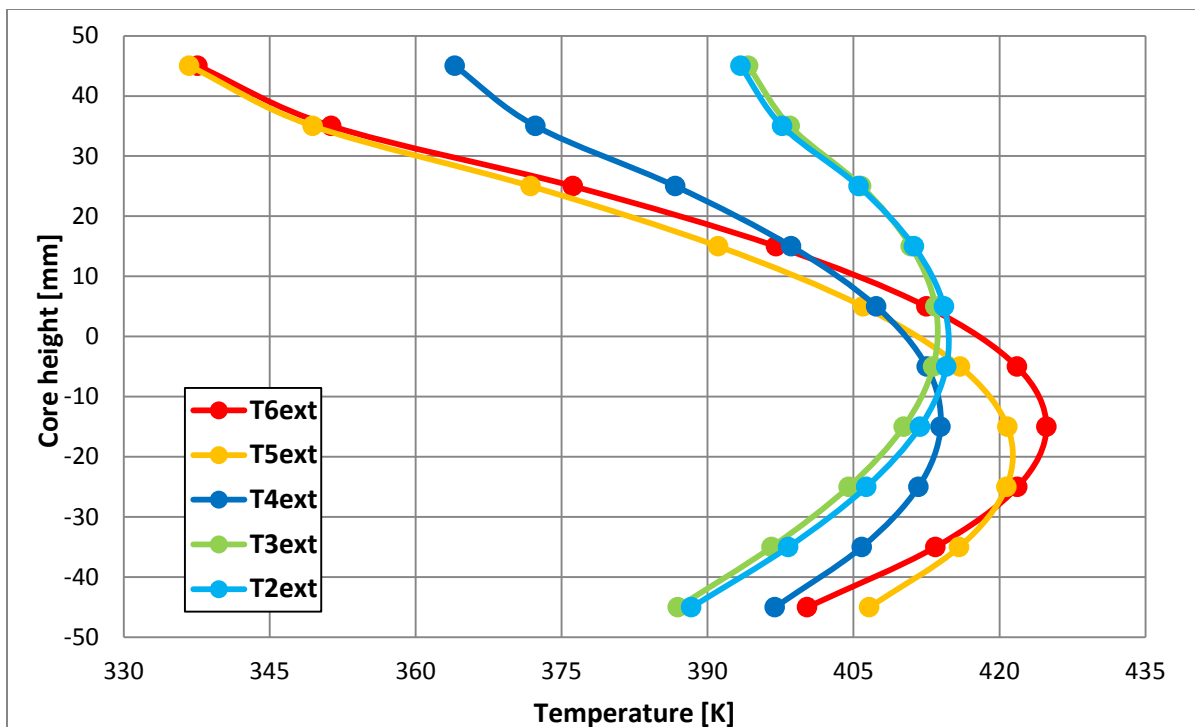


Figure 7. Temperature distribution on ECIP of each fuel pipe

On the outer side of fuel pipe as below:

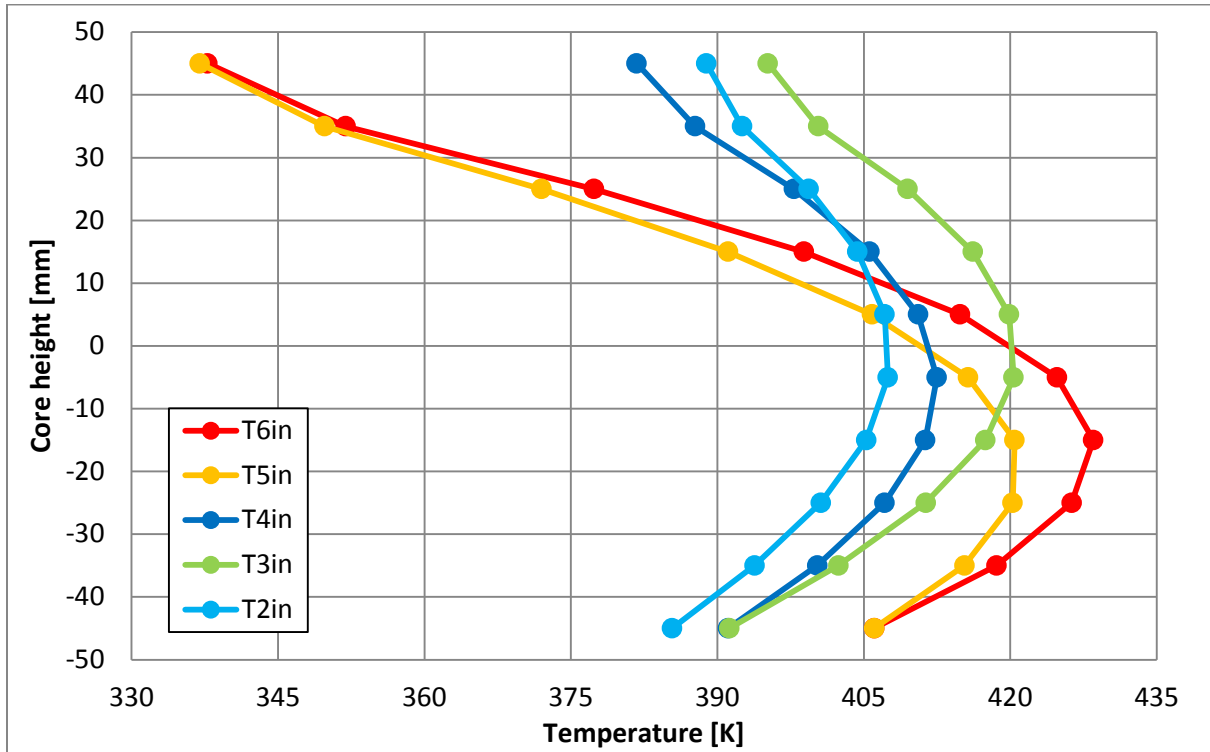


Figure 8. Temperature distribution on ICEP of each fuel pipe

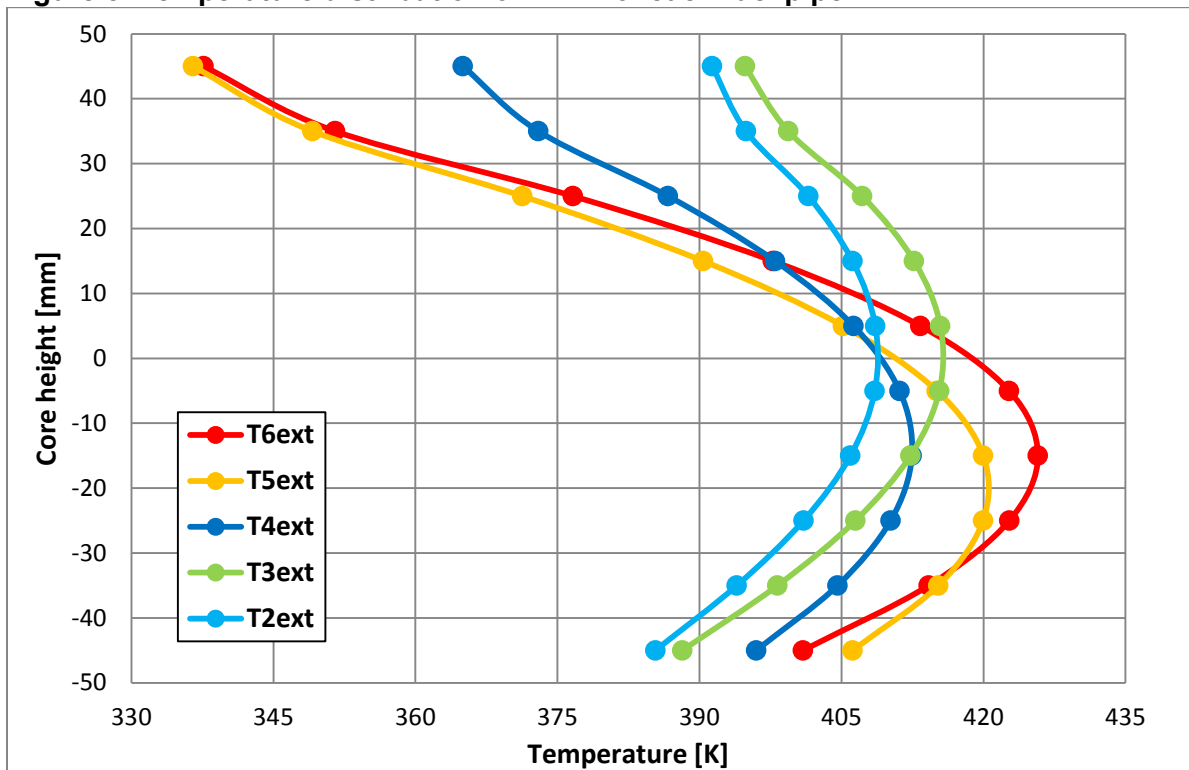


Figure 9. Temperature distribution on ECEP of each fuel pipe

Temperature distribution of water between pipes in gaps as below:

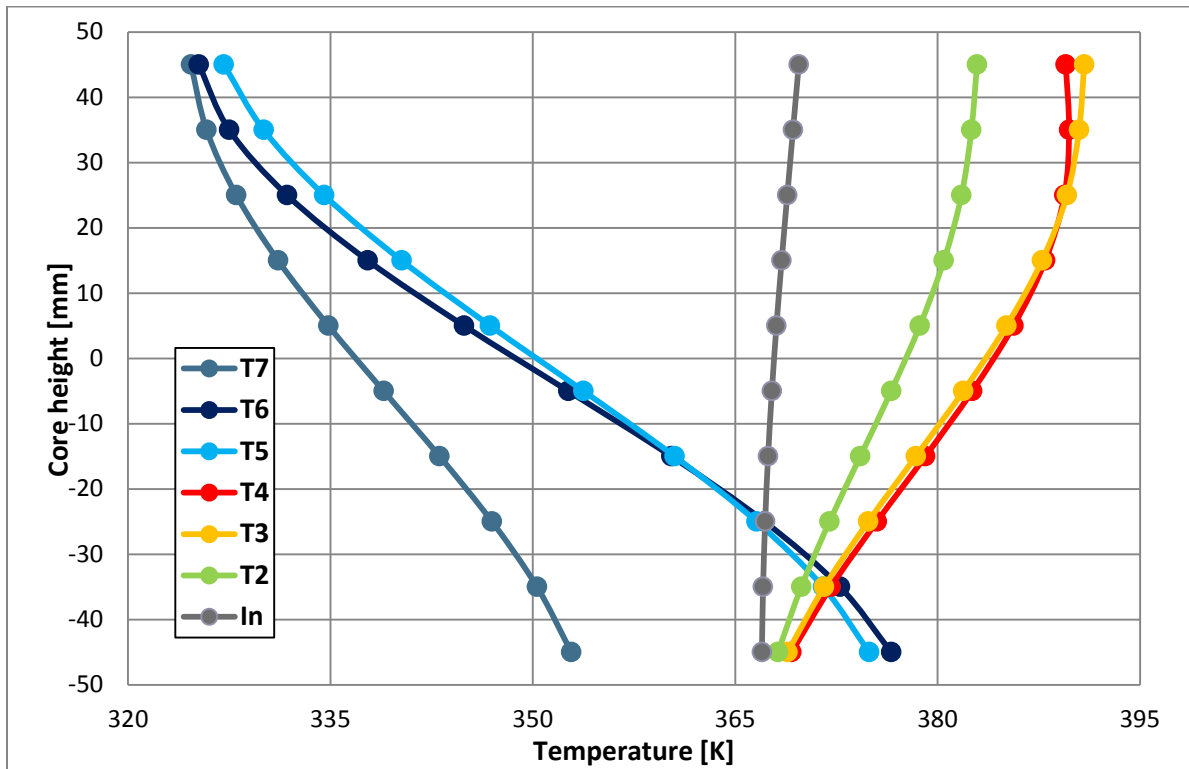


Figure 10. Water temperature distribution in gaps between fuel pipes. In – filler gap

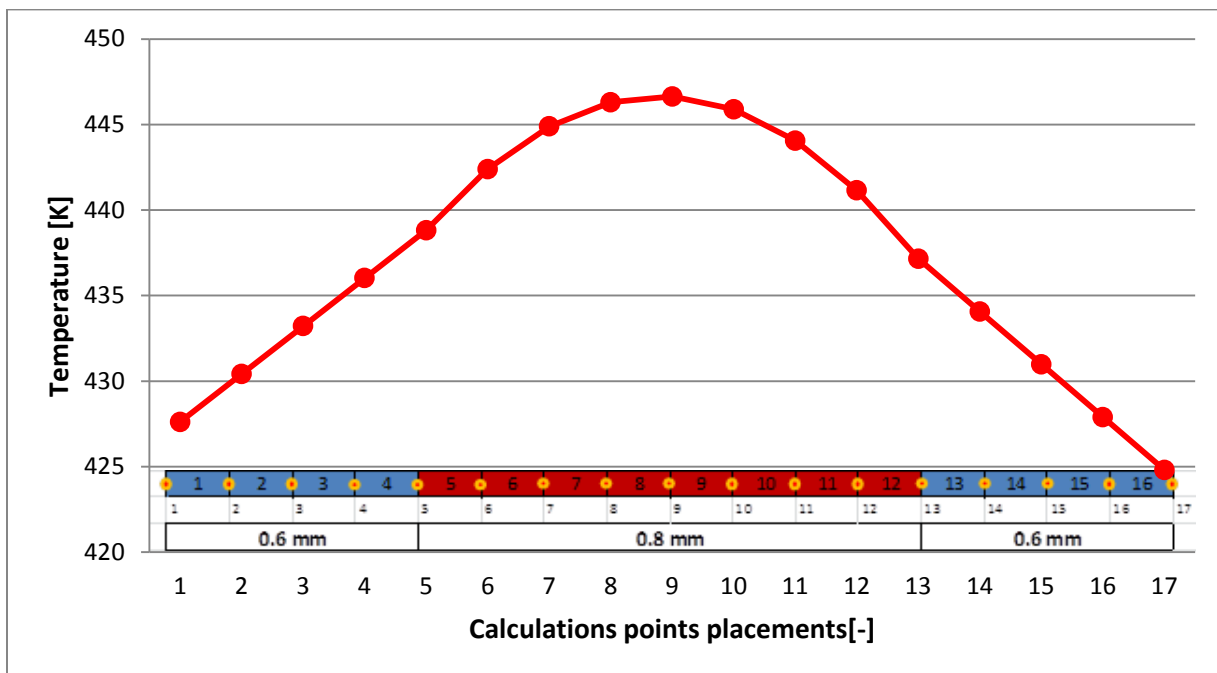


Figure 11. Maximum temperature axial distribution in fuel pipe no. 6. Yellow dots – calculation points in fuel pipe, red – fuel, blue – cladding

Heat flux distribution on outer side of fuel pipes

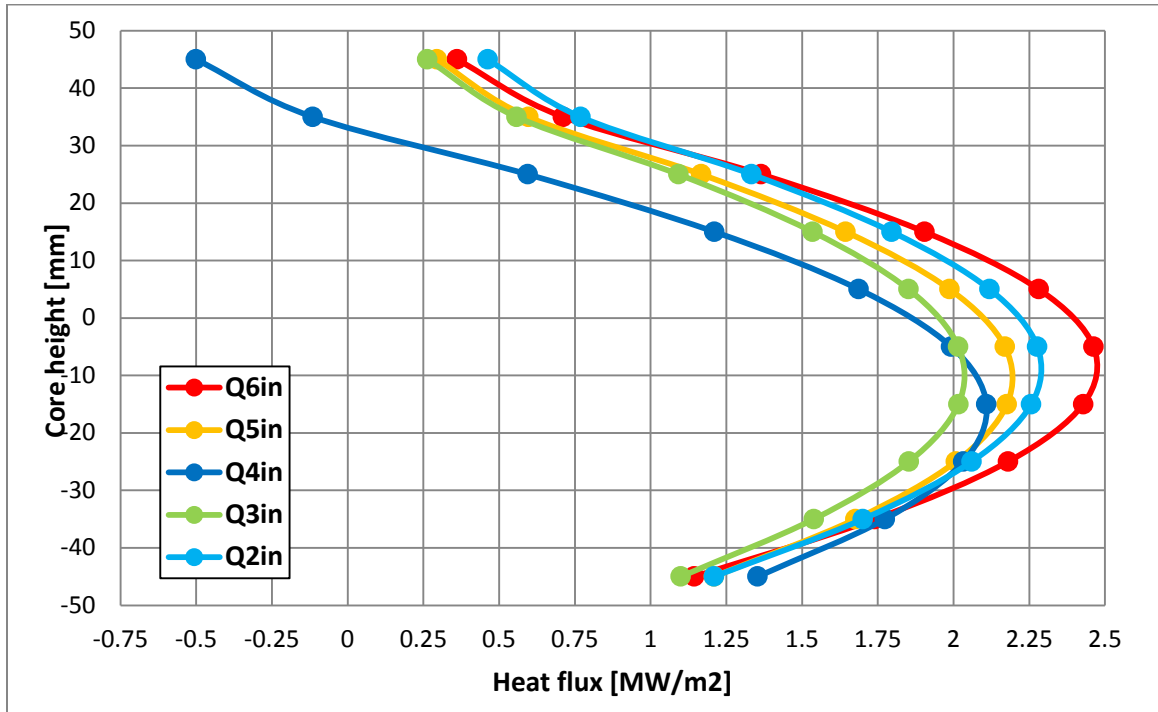


Figure 12. Heat flux distribution on inner side of fuel pipes.

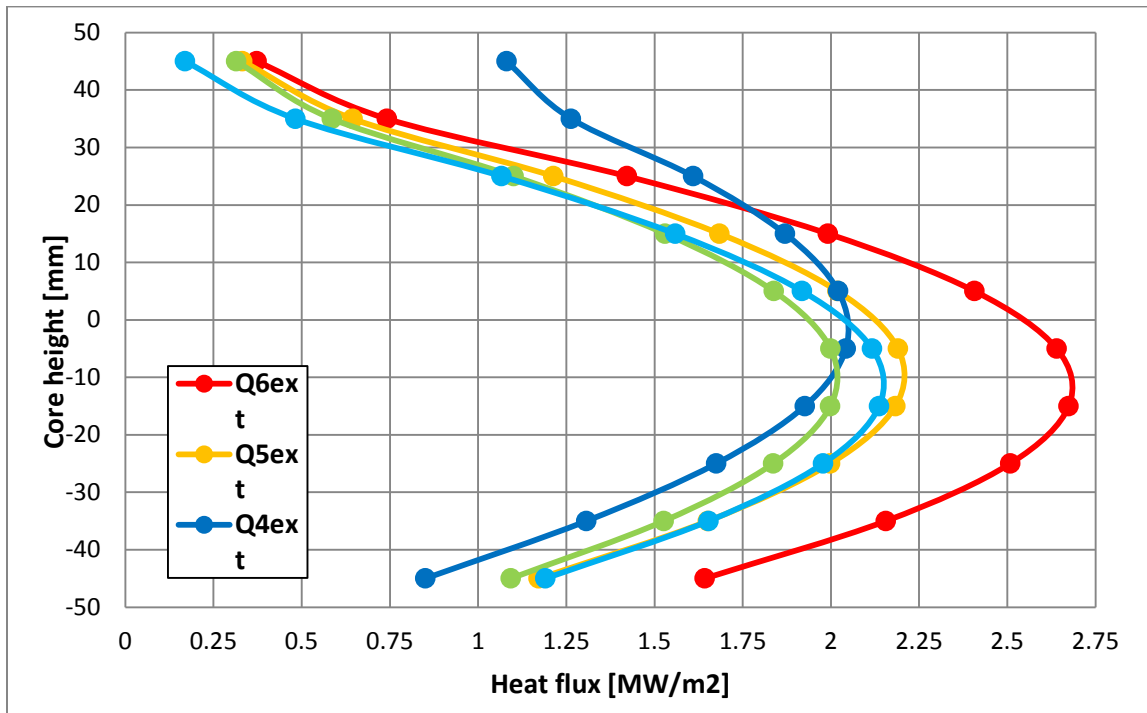


Figure 13. Heat flux distribution on outer side of fuel pipes

Comparison of results

A comparison of two calculations is presented in Table 2. The main results of the RELAP5 calculations with inlet temperature $T_{in}=318.15K$ presented in the chapter above are compared with the results received using the SN code. Additionally one more calculation using RELAP5 was performed for the same conditions except for the inlet temperature which was changed to $T_{in}=323.15K$

Table 2. Comparison of results for two scenarios

	RELAP5	RELAP5 ($T_{in}=323.1K$)	SN
Maximum peak clad temperature on ECIP of fuel pipe [K]	427.6	431.0	425.6
Maximum peak coolant temperature [K]	390.9	396.2	no data
Maximum heat flux [MW/m^2]	2.67	2.68	2.63
Maximum temperature in the fuel centre point [K]	446.6	450.0	no data

4.2 LOFA - Loss of flow in the fuel channel cooling system

Accident conditions

Loss of flow in the fuel channel cooling system is possible in case of the loss of power in the pump system. As a result a sudden decrease of pressure occurs in the cooling channel that leads to the initiation of the emergency signal and shutdown of the reactor. Furthermore, after the loss of flow a rapid increase of fuel clad temperature and cooling temperature in gaps between fuel pipes occurs. According to the scenario a few seconds after the loss of power in the pump system, the work of a backup pump should be initiated with the power supply from accumulator batteries and with lower speed – 1500 r/s. After the reactor shutdown and before the flow is stabilized another small temperature jump can be detected.

Initial and boundary conditions:

Initial conditions:

- Cooling channel Inlet water temperature $T_{in}=318.15K$
- Mass flow $Q=8.25kg/s$ ($30m^3/h$ for density of water: $990kg/m^3$)
- Pressure at the fuel channel inlet $p_{in}=1.7MPa$
- Fuel channel pressure drop $\Delta p=0.59MPa$
- Fuel element thermal power 1.8MW

Boundary conditions:

- Alarm signal – signal from decrease pressure to 1.4MPa
- Signal delay time $t_1=0.2s$
- Effective time of safety and control rods insertion $t_2=0.15s$
- Inserted negative reactivity (from rods PK and PB) $\rho=-5.5\%$ (-2% PK, -3.5% PB – with the

- assumption that the rod with the highest weight failed)
- Loos of flow modelled as in the Supplement³
- Temperature reactivity coefficients: $\alpha_f = -0.25\%/deg$, $\alpha_w = -2.02\%/deg$

Results

The sequence of events:

Table 3. Sequence of events for LOFA

Time [s]	
0.00	Pump trip, loos of flow
0.40	Alarm signal $p=1.4\text{Mpa}$
0.75	Beginning of the negative reactivity insertion from PK and PB
0.78	Peak Clad Temperature on ICIP of fuel pipe nr 6 - 440.38 K
0.79	Peak Clad Temperature on ECIP of fuel pipe nr 6 - 432.07 K
0.89	Peak Coolant Temperature in the gap between fuel pipe nr 3 and nr 4 – 394.07 K
6.32	Second Peak Clad Temperature on ECIP of fuel pipe nr 6 with 2 cooling pumps – 381.56 K
13.90	Second Peak Clad Temperature on ECIP of fuel pipe nr 6 with 1 cooling pump – 399 K

Table 4. Distribution of calculated top temperatures on fuel pipes

Pipe nr	2		3		4		5		6	
RELAP5 component	160		155		150		130		125	
Side of pipe	In.	Out.	In.	Out.	In.	Out.	In.	Out.	In.	Out.
Max. temperature on the outer layer of clad	413	415	413	413	416	418	426	426	432	430
Max. temperature on the inner layer of clad	421	422	420	420	423	424	433	433	440	439

³ Aneks 2012/1 do Eksploatacyjnego Raportu Bezpieczeństwa Reaktora MARIA Konwersja rdzenia reaktora MARIA na paliwo MC, July 2012.

Comparison of results

Clad temperature

The highest outer clad temperature calculated with the SN code was 433.4K, and temperature calculated with RELAP5 code was 432K (outer layer temperature – 440K). Both codes calculated the highest temperature in the same place – on the internal side of pipe no 6.

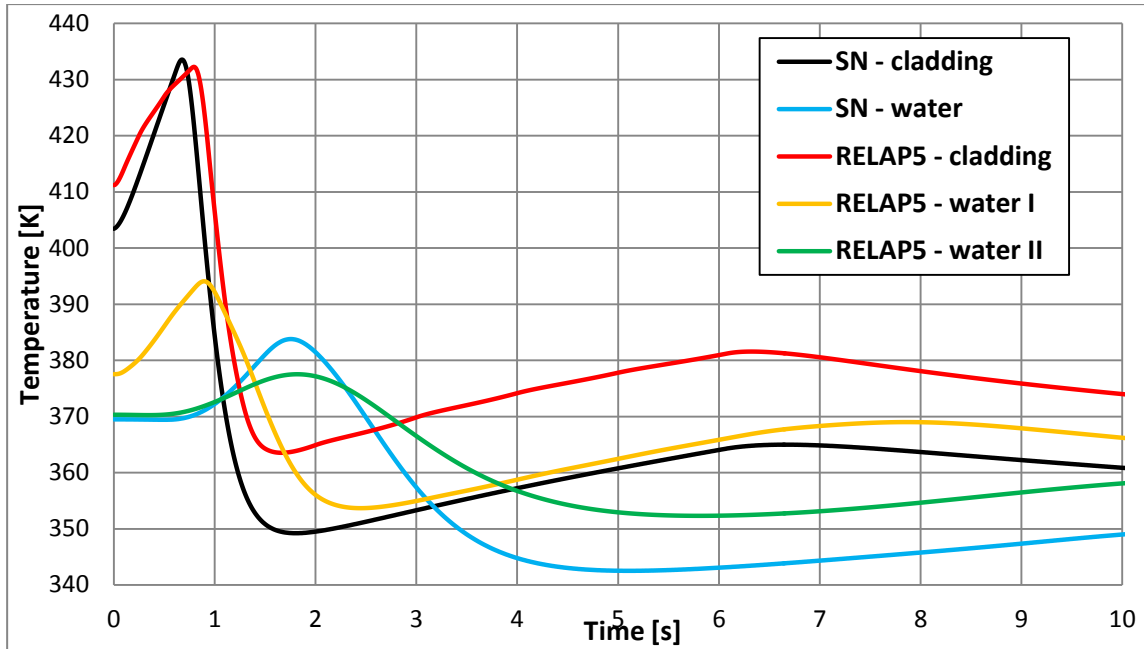


Figure 14. Cladding and water temperature changes. SN code: water and fuel element outlet temperature, RELAP5: water I – fuel element outlet temperature, water II - fuel channel outlet temperature

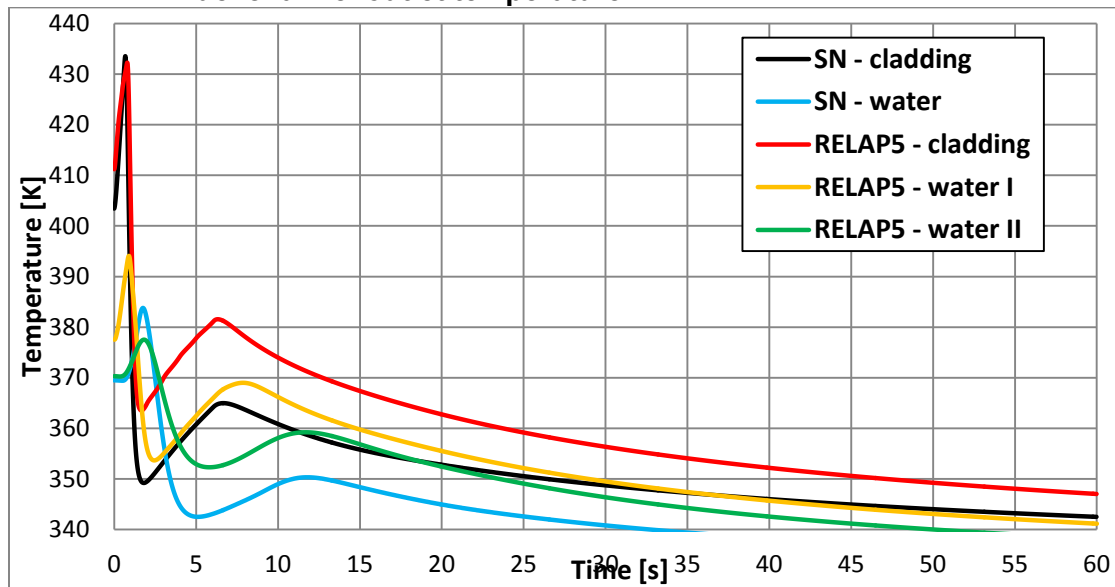


Figure 15. Cladding and water temperature changes. SN code: water and fuel element outlet temperature, RELAP5: water I – fuel element outlet temperature, water II - fuel channel outlet temperature. Wider scale range.

ONBR⁴ parameter

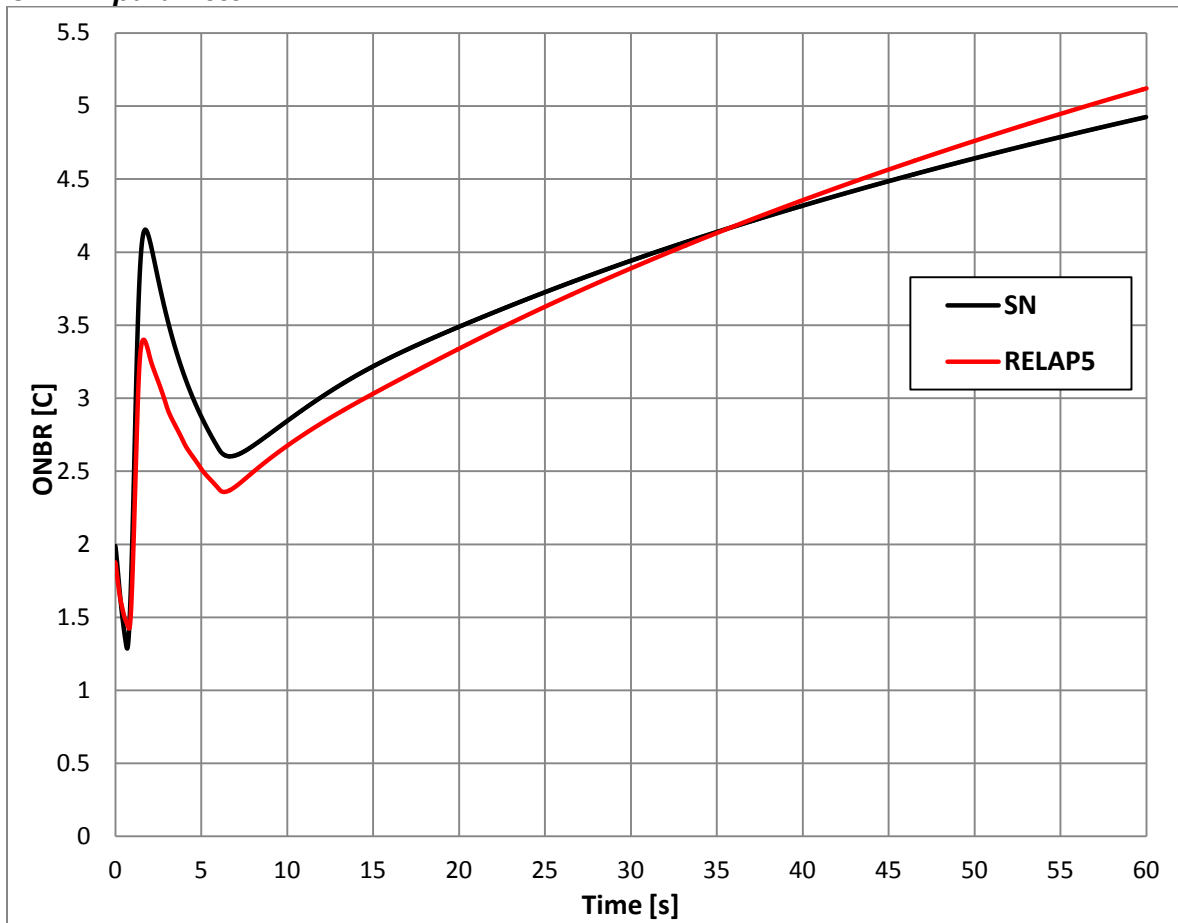


Figure 16. ONBR parameter changes

4 ONBR (Onset of Nuclear Boiling Ratio) should be greater than 1.2, where:

$$ONBR = (T_{ONB} - T_{in}) / (T_{wall} - T_{in})$$

$$T_{ONB} = T_{sat} + 0.182 * q^{0.35} / p^{0.23} \text{ (Forester-Greif correlations)}$$

T_{in} - inlet coolant temperature,

T_{wall} - the clad surface temperature,

T_{sat} - saturation coolant temperature,

q - heat flux [W/m^2],

p - pressure [bar].

Second clad temperature maximum (depending on the number of cooling pumps)

Table 5. Comparison of results for second temperature peak

Parameter	SN		RELAP5	
	1 pump	2 pumps	1 pump	2 pumps
Maximum outer temperature of clad [K]	387.25	364.98	399.0	381.56
Minimum ONBR	1.74	2.60	1.84	2.34

Differences in results

Differences in the results calculated by RELAP5 and the SN code arose due to many factors and not necessarily related only to nodalization. One of the factors - is a different flow model. In case of the SN code a more pessimistic method was used – coolant flow from fuel channel occurs at the same time in all gaps between fuel pipes. In case of RELAP5 a more realistic model was used. The water first flows down into the three gaps then gets mixed and next fills the rest of the gaps between the fuel pipes. The second example of differences is another model of decay heat. In case of RELAP5 decay heat was calculated by the code from kinetics and time of operation, whereas in the case of the SN code - decay heat was calculated on the basis of the old type of fuel measurements.

4.3 Slow reactivity insertion accident on low power level

Accident conditions

In case when the operator undertakes incorrect actions or a malfunction of the reactivity regulation system occurs, it is possible that as a result, positive reactivity is inserted into the core with the maximum reactivity speed $0.04\$/s$. This scenario was checked for low power level conditions.

Initial conditions:

- Cooling channel Inlet water temperature $T_{in}=313.15K$
- Mass flow $Q=8.268kg/s$ ($30m^3/h$ for density of water: $992.2kg/m^3$)
- Pressure at the fuel channel inlet $p_{in}=1.7MPa$
- Fuel channel pressure drop $\Delta p=0.59MPa$
- Fuel element thermal power $10kW$

Boundary conditions:

- Alarm signal – signal from increase of power to 480% - in this case to $48kW$
- Signal delay time $t_1=0.2s$
- Effective time of safety and control rods insertion $t_2=0.15s$
- Insertion positive reactivity from accident $t=0s$ $\rho=0.04\$/s$, $\rho_{max}=1.5\%$

- Inserted negative reactivity (from rods PK and PB) $\rho = -5.5\%$ (-2% PK, -3.5% PB)
- Temperature reactivity coefficients: $\alpha_f = -0.23\%/deg$, $\alpha_w = -1.93\%/deg$

Comparison of results

Table 6. Comparison of results for SRIA on low power level

Sequence of events	SN		RELAP5	
	Time [s]	Value	Time [s]	Value
Start of positive reactivity insertion	0.0	-	0.0	-
Alarm signal 480% of power	12.3	-	12.48	-
Start of negative reactivity insertion	no data	-	12.83	-
Maximum power	12.7	53kW	12.83	52.7kW
Maximum peak cladding temperature on ECIP of fuel pipe nr 6	no data	316.15K	12.85	316.14K
Maximum peak cladding temperature on ICIP of fuel pipe nr 6	no data	no data	12.85	316.44K
Minimum ONBR	no data	about 50	12.85	53.8
Maximum peak coolant temperature in gap nr 3 between fuel pipe nr 3 and 4	no data	no data	12.9	314.72K

This scenario has the lowest impact on the fuel elements. The temperature peaks of water and clad are very small - smaller than fluctuations of temperature during normal operation of the reactor.

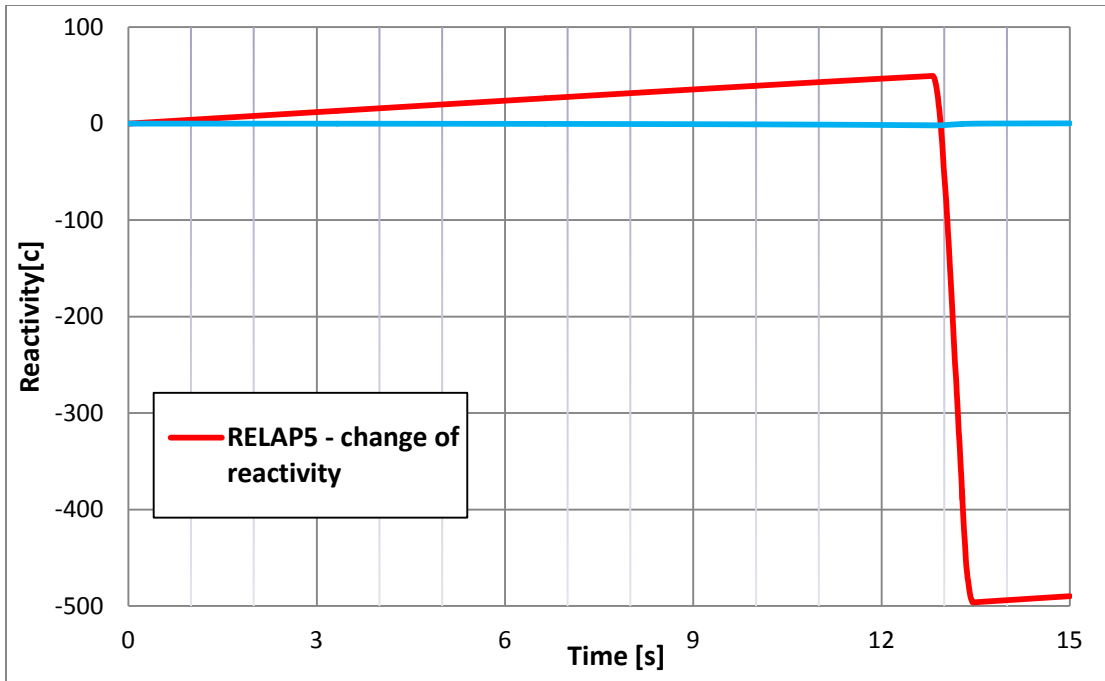


Figure 17. Reactivity changes. RELAP5: total reactivity change; water and fuel: reactivity change due to coolant and fuel temperature reactivity coefficients

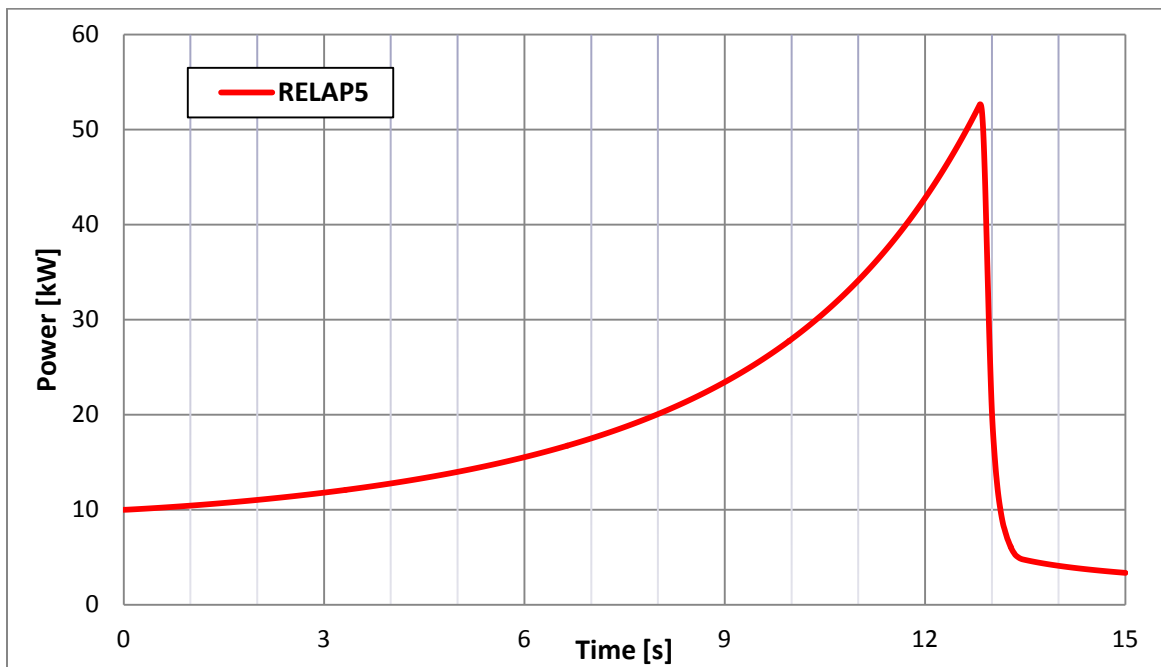


Figure 18. Power changes of fuel element for SRIA on low power level

4.4 Fast reactivity insertion accident on low power level

One of the important scenarios addressed in the supplementary document is the fast inflow of cold water into the core resulting in a sudden increase of reactivity. The negative reactivity coefficients lead to the increase of power in the fuel elements. The cold water is directed first between the first three pipes – pipes no. 4, 5, 6 on Figure 2 and after about 0.2s into the rest of the gaps.

Accident conditions

Initial conditions:

- Cooling channel Inlet water temperature $T_{in}=323.15K$, after 1s insertion of cold water $T_{2in}=283.15K$
- Mass flow $Q=8.268kg/s$ ($30m^3/h$ for density of water: $992.2kg/m^3$) $T_{2in}=283.15K$.
- Pressure at the fuel channel inlet $p_{in}=1.7MPa$
- Fuel channel pressure drop $\Delta p=0.59MPa$
- Fuel element thermal power 10kW

Boundary conditions:

- Alarm signal – increase of power to 480% - in this case to 48kW
- Signal delay time $t_1=0.2s$
- Effective time of safety and control rods insertion $t_2=0.15s$
- Insertion of positive reactivity from accident $t=0s$ $\rho=0.04\$/s$, $\rho_{max}=1.5\$/s$
- Insertion of negative reactivity (from rods PK and PB) $\rho=-5.5\$/s$ (-2\$ PK, -3.5\$ PB)
- Temperature reactivity coefficients: $a_f=-0.23\$/deg$, $a_w=-1.93\$/deg$

Comparison of results

Table 7. Comparison of results for FRIA on low power level

Sequence of events:	SN		RELAP5	
	Time [s]	Value	Time [s]	Value
Start of insertion of cold water to the fuel channel	1.0	-	1.0	-
Minimum ONBR	no data	about 5	1.34	4.95
Cold water In fuel pipes zone	1.59	-	1.67	-
Alarm 480% of power	2.44	-	2.47	-
Start of negative reactivity insertion	2.79	-	2.82	-
Maximum power	2.83	96.3kW	2.85	80.9kW

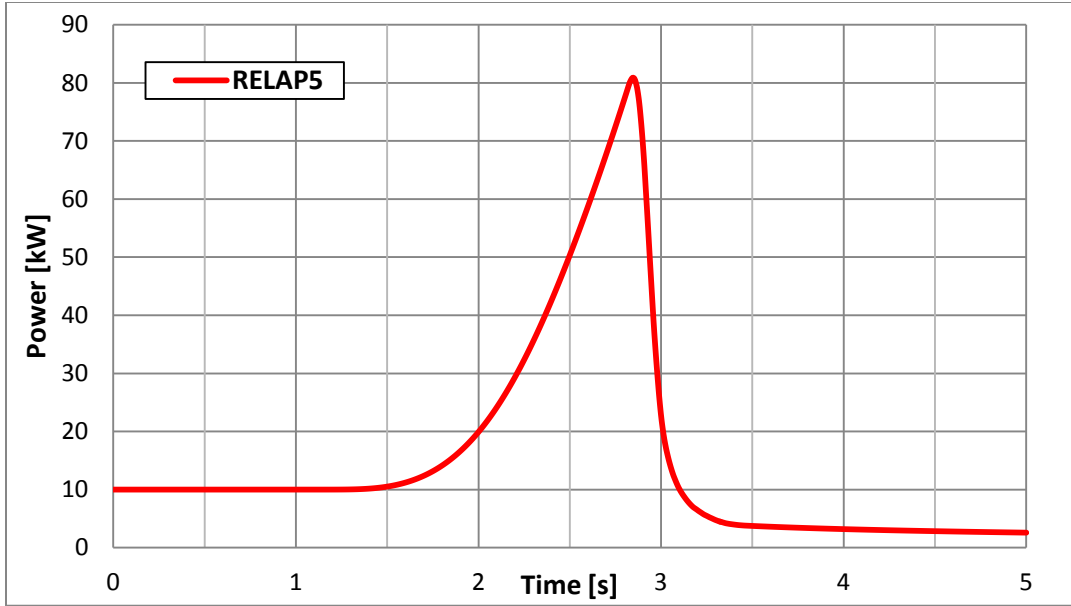


Figure 19. Power changes of fuel element for FRIA on low power level

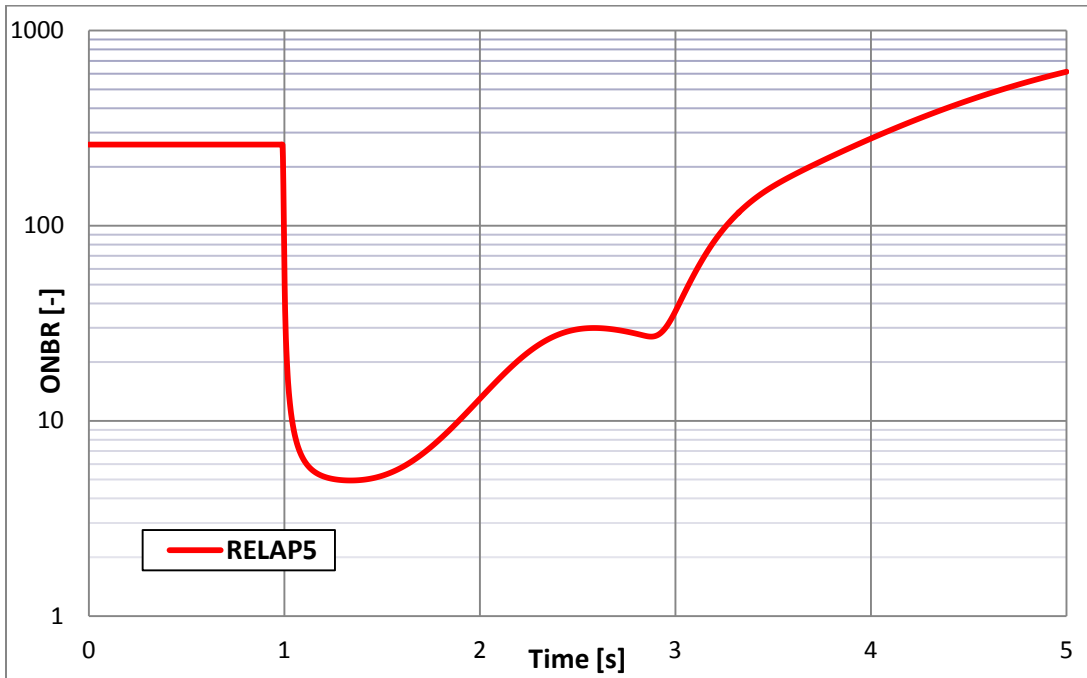


Figure 20. ONBR parameter changes

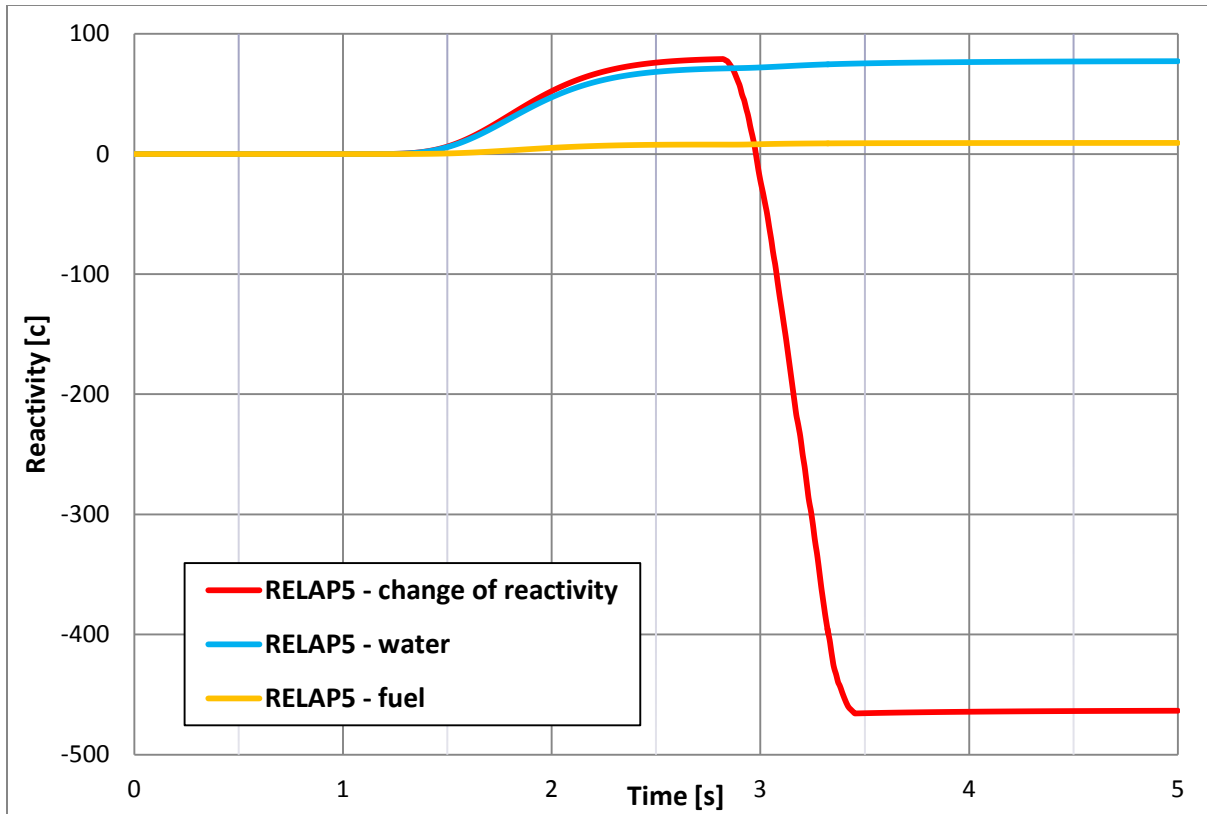


Figure 21. Reactivity changes - RELAP5 calculations: i) change of reactivity: total reactivity change, ii) water: change due to coolant temperature reactivity coefficients, iii) fuel: change due to fuel temperature reactivity coefficient

4.5 Slow reactivity insertion accident during normal operation of reactor

Accident conditions

The scenario analyzed in this transient is very similar to the slow reactivity insertion on low power. The main difference is that the reactor is in the normal operation mode, on full power, with the maximum allowed thermal power generation. In case when the operator undertakes incorrect actions or a malfunction of the reactivity regulation system occurs, it is possible that as a result, positive reactivity is inserted into the core with the maximum reactivity speed 0.04\$/s.

Initial conditions:

- Cooling channel Inlet water temperature $T_{in}=318.15K$,
- Mass flow $Q=8.252kg/s$ ($30m^3/h$ for density of water: $990.2kg/m^3$)
- Pressure at the fuel channel inlet $p_{in}=1.7MPa$
- Fuel channel pressure drop $\Delta p=0.59MPa$
- Fuel element thermal power 1.8MW

Boundary conditions:

- Alarm signal – signal from increase of power to 120% - in this case to 2.16MW
- Signal delayed $t_1=0.2s$
- Effective time of safety and control rods insertion $t_2=0.15s$
- Insertion of positive reactivity from accident $t=0s$ $\rho=0.04\$/s$, $\rho_{max}=1.5\%$
- Insertion of negative reactivity (from rods PK and PB) $\rho=-5.5\%$ (-2% PK, -3.5% PB)
- Temperature reactivity coefficients: $\alpha_f=-0.23\%/deg$, $\alpha_w=-1.93\%/deg$

Comparison of results

Table 8. Comparison of results for SRIA during normal operation

Sequence of events:	SN		RELAP5	
	Time [s]	Value	Time [s]	Value
Start of insertion of positive reactivity	0.0	0.04\$/s	0.0	0.04\$/s
Alarm signal – power 120%	5.37	-	6.44	-
Start of insertion of negative reactivity	no data	-	6.79	-
Maximum power	5.72	2.189MW	6.80	2.183MW
Maximum peak cladding temperature on ECIP of fuel pipe nr 6	5.73	424.86K	6.80	428.16K
Maximum peak cladding temperature on ICIP of fuel pipe nr 6	no data	-	6.80	440.5K
Minimum ONBR	5.73	about 1.6	6.80	1.60
Maximum peak coolant temperature on exit from fuel element	5.77	381.29K	6.86	386K

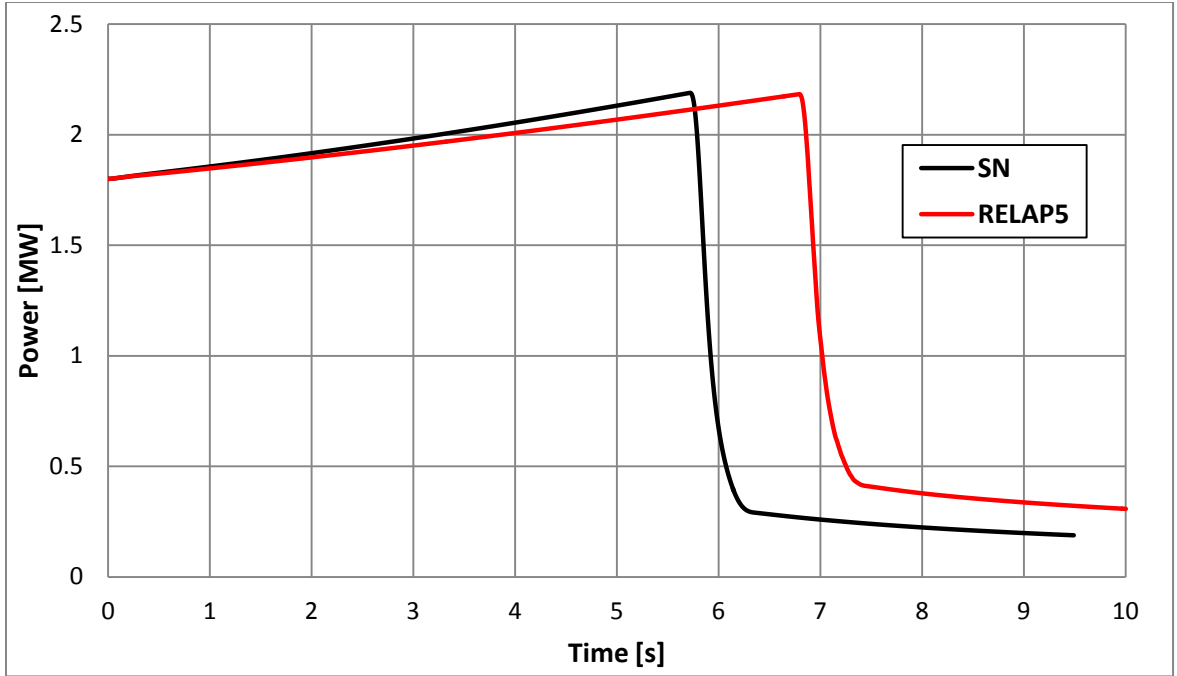


Figure 22. Power changes of fuel element for SRIA on nominal power level

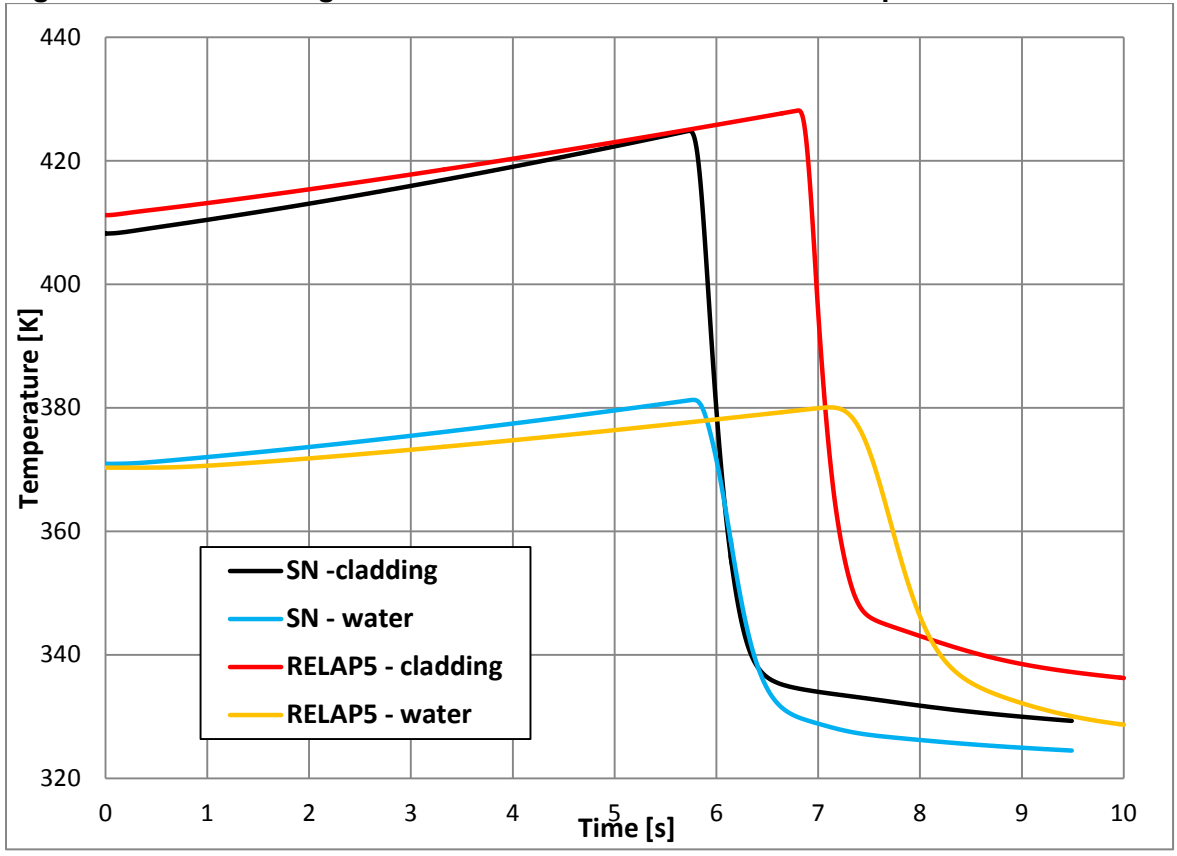


Figure 23. Cladding and water temperature changes. RELAP5 and SN codes: cladding – cladding temperature, water – fuel element outlet temperature

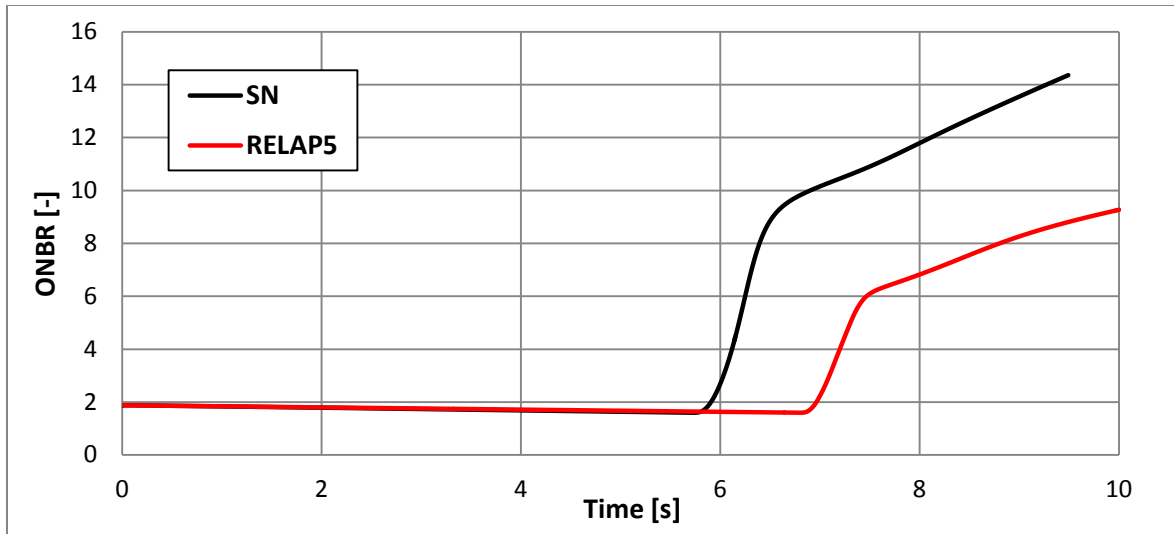


Figure 24. ONBR parameter changes

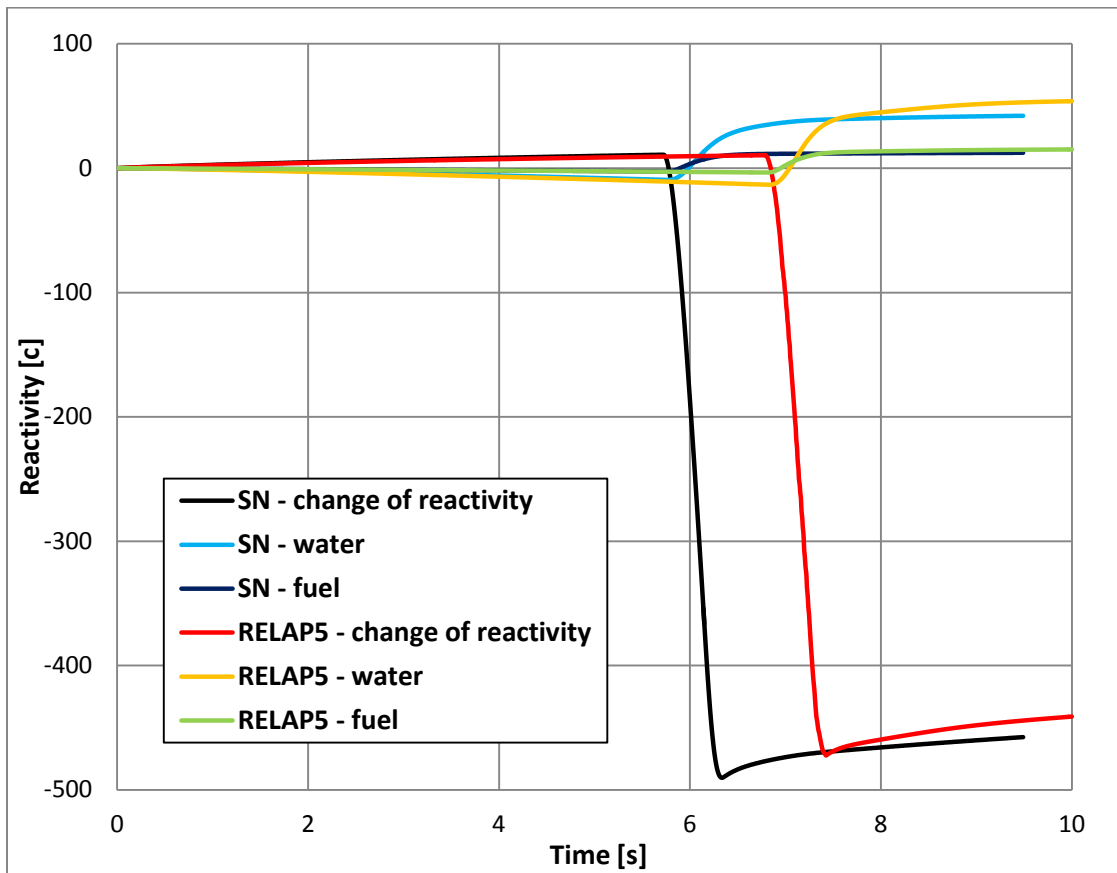


Figure 25. Reactivity changes. RELAP5 and SN codes: change of reactivity - total reactivity change, water - change due to coolant temperature reactivity coefficients, fuel - change due to fuel temperature reactivity coefficients

4.6 Fast reactivity insertion accident during reactor normal operation

Accident Conditions

A break of control rods is another scenario included in the supplementary document. The break of control rods leads to fast insertion of positive reactivity into the reactor. It is assumed that the maximum insertion of positive reactivity is equal to 1.5\$ with the top speed of insertion 4\$/s.

Initial conditions:

- Cooling channel inlet water temperature $T_{in}=318.15K$,
- Mass flow $Q=8.252kg/s$ ($30m^3/h$ for density of water: $990.2kg/m^3$)
- Pressure at the fuel channel inlet $p_{in}=1.7MPa$
- Fuel channel pressure drop $\Delta p=0.59MPa$
- Fuel element thermal power 1.8MW

Boundary conditions:

- Alarm signal – increase of power to 120% - in this case to 2.16MW
- Signal delay time $t_1=0.2s$
- Effective time of safety and control rods insertion $t_2=0.15s$
- Insertion of positive reactivity from accident $t=0s$ $\rho=0.04\$/s$, $\rho_{max}=1.5\%$
- Insertion of negative reactivity (from rods PK and PB) $\rho=-5.5\%$ (-2\$ PK, -3.5\$ PB)
- Temperature reactivity coefficients: $\alpha_f=-0.23\%/deg$, $\alpha_w=-1.93\%/deg$

Comparison of results

Table 9. Comparison results for FRIA during normal operation

Sequence of events:	SN		RELAP5	
	Time [s]	Value	Time [s]	Value
Start of	0.0	4\$/s	0.0	4\$/s
Alarm signal 120%	0.08	-	0.07	-
Maximum thermal power	0.40	8.6MW	0.38	5.62MW
Maximum peak cladding temperature on ECIP of fuel pipe nr 6	no data	598.88K	0.40	515.52K
Maximum peak cladding temperature on ICIP of fuel pipe no. 6	no data	-	0.40	547.46K
Minimum ONBR	0.45	0.64	0.41	0.928
Start of insertion of negative reactivity	0.44	-	0.42	-
Max. peak coolant temperature on exit from fuel element	0.58	460.65K	0.55	448.39K

The main differences in the results between RELAP and the SN code are due to the different models of reactor kinetics. RELAP5 uses the point kinetic model and this model was applied to the RIA analysis. In the nodalization model applied, total reactivity was divided into many sections depending on the position in the fuel pipes or in the gap between pipes. The fuel reactivity coefficient was divided in 50 point, 10 points in each cell of the fuel pipe because the values of the divided fuel reactivity coefficients depend on the distribution of heat generation on fuel pipes and axial distribution of heat generation (i.e. shifted cosine model). The coolant reactivity coefficient was divided into 60 points, 10 points in each gap. The values of the divided coolant reactivity coefficient depend on the distribution of the mass flow between gaps and the distribution of heat (shifted cosine model). In case of the SN code a more pessimistic model was used.

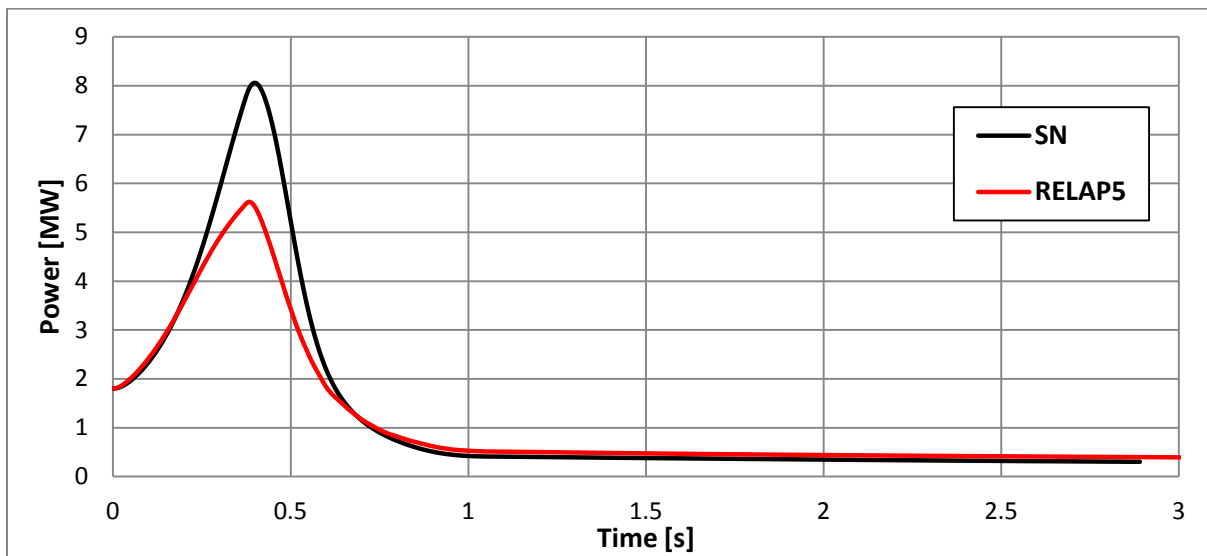


Figure 26. Power changes of fuel element for FRIA on nominal power level

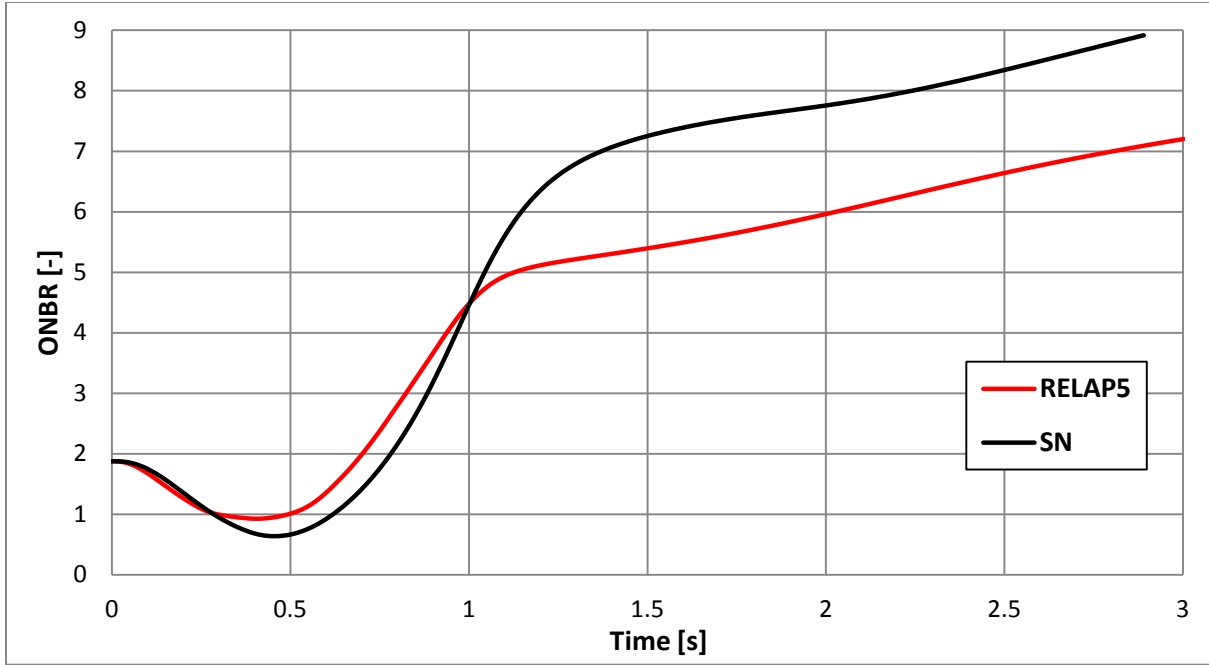


Figure 27. ONBR parameter changes

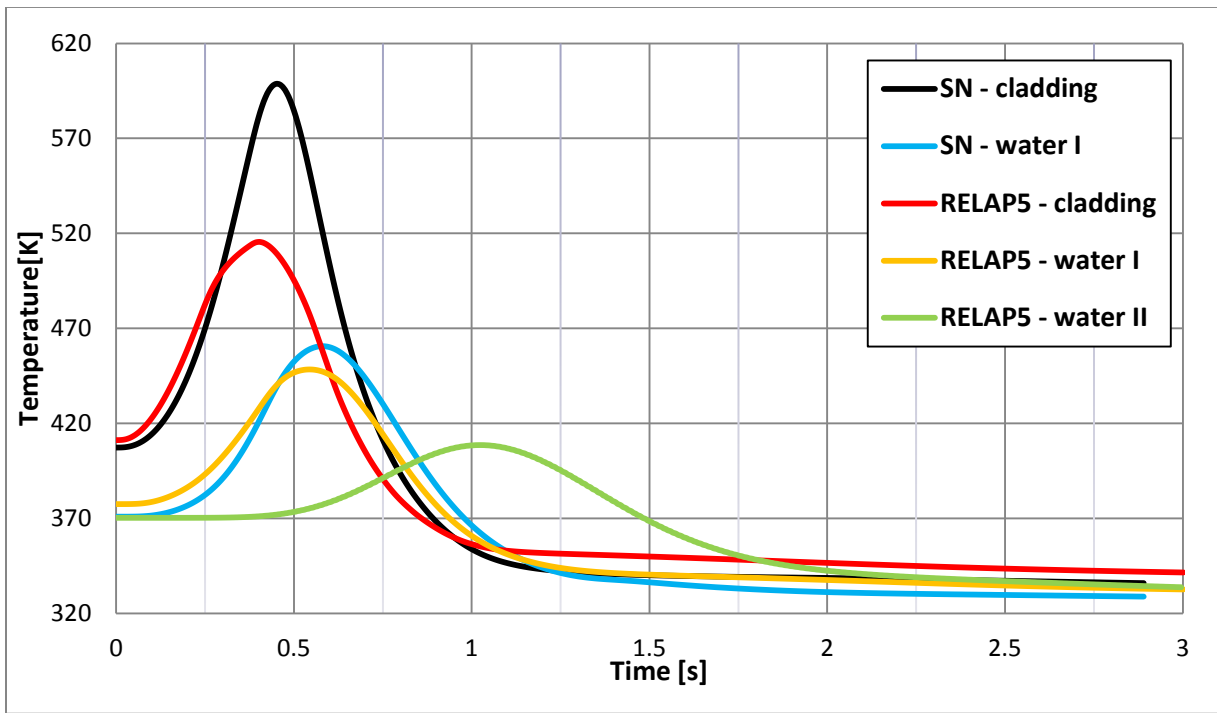


Figure 28. Cladding and water temperature changes. RELAP5 and SN codes: cladding – cladding temperature, water I – fuel element outlet temperature, water II - fuel channel outlet temperature

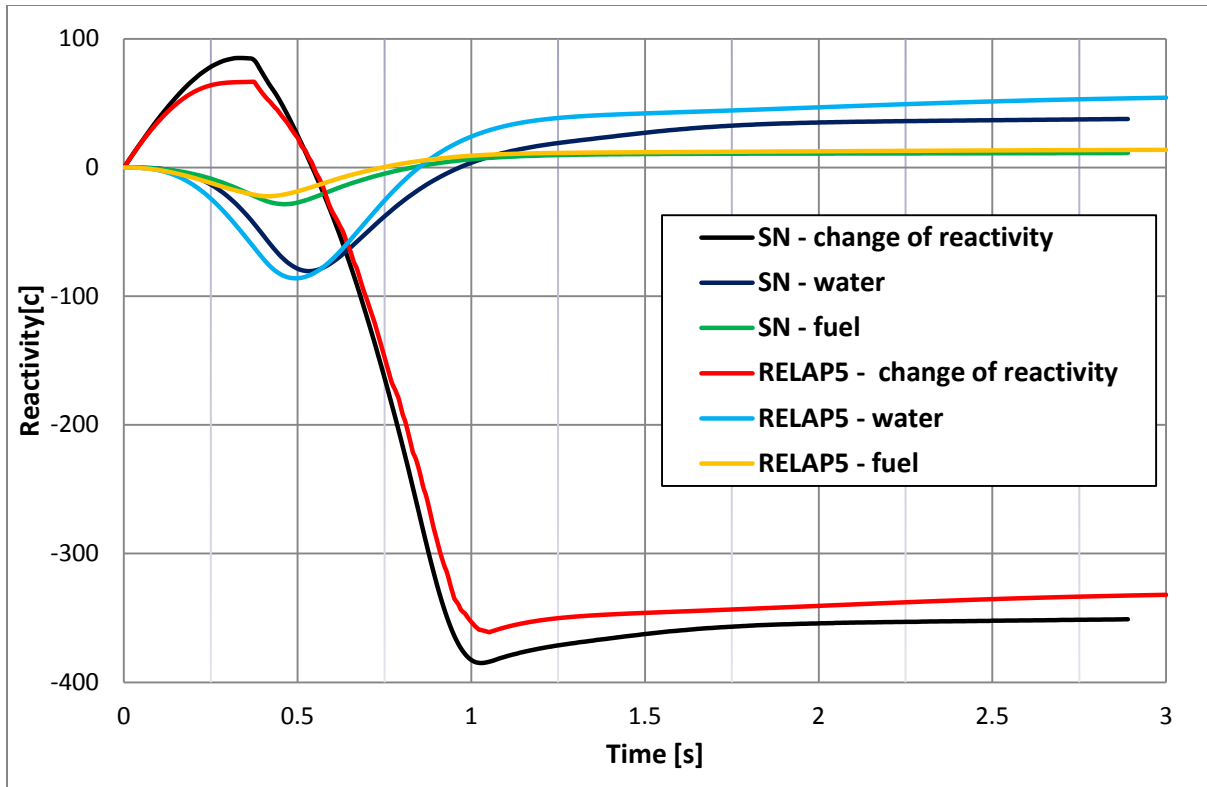


Figure 29. Reactivity changes. RELAP5 and SN codes: change of reactivity - total reactivity change, water - change due to coolant temperature reactivity coefficients, fuel - change due to fuel temperature reactivity coefficients

5 RUN STATISTICS

All analysis were performed on one computer:

Intel(R) Core(TM) i3-2125 CPU @ 3.30 GHz
RAM memory :4.00 GB
Windows 7 Professional – SP1, 64-bit version
IFC (Intel Fortran Compiler) for RELAP5

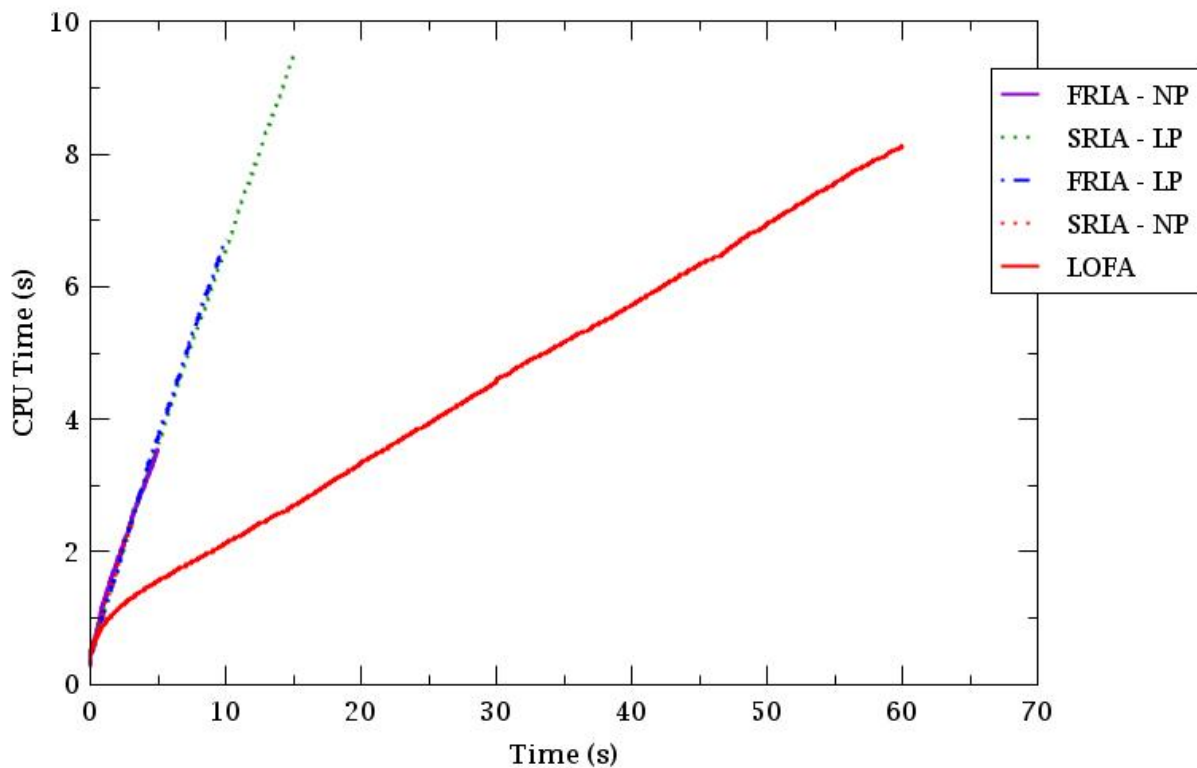


Figure 30. Calculation time for various cases

6 CONCLUSIONS

Most of the results of the simulation for the research reactor MARIA made with RELAP5 code showed that there is no big difference between the results achieved by the validated SN and the RELAP5 codes. Only in one case (RIA with fast reactivity insertion with maximum power level) there is the opportunity to exceed the lowest allowed level of the ONBR parameter. Exceeding this parameter can cause the onset of boiling of the coolant in the gap between the fuel pipes. In the analysed case, the duration of time when ONBR is lower than 1.2 is very short (about 0.35s) and should not cause any damage to the fuel and clad material. In the fast RIA scenario, the power jump during the insertion of positive reactivity was stopped by the negative reactivity coefficients (fuel and coolant) before insertion of the safety and control rods into the core could be initiated.

In other simulated scenarios, no opportunity to exceed the ONBR parameter or temperature limit of clad – 452K occurred.

In the analysed LOFA scenario, the calculations showed that enough cooling capability is provided even when only one pump is working with a lower rotation speed than the normally required two pumps.

The content of this report does not cover all possible accident conditions that should be analysed for the research reactor. Further analysis will be necessary. A comparison of the SN and RELAP5 codes showed that RELAP5 can be used in the safety analysis for the research reactor MARIA.

7 REFERENCES

1. "Aneks 2009/1 do Eksploatacyjnego Raportu Bezpieczeństwa Reaktora MARIA Badania paliwa MC", 2009 (in Polish).
2. "Aneks 2012/1 do Eksploatacyjnego Raportu Bezpieczeństwa Reaktora MARIA Konwersja rdzenia reaktora MARIA na paliwo MC", July 2012 (in Polish).
3. (SAR) "Eksploatacyjny Raport Bezpieczeństwa Reaktora MARIA", 2009 (in Polish).

APPENDIX A – TECHNICAL INFORMATION ON THE RESEARCH REACTOR MARIA

The research reactor 'Maria' was designed by the Institute for Nuclear Studies in Poland and is operated by the National Centre for Nuclear Research that was created on the basis of two older Institutes. The reactor started to work in 1974 and is under operation till now except for the period of 1986 to 1991 when it was undergoing modernization.

It is a pool type reactor with closed fuel channels and closed fuel channel primary cooling circuit, primary pool cooling circuit and secondary cooling circuit. The fuel channel cooling circuit includes also a pressurizer.

At present the reactor is used for the production of isotopes and for performing experiments. The total thermal power is 30 MW. More data that might be of interest is presented below.

Thermo-hydraulic parameters	During a typical cycle of work: Thermal power of a fuel channel: 15-19 MW(th) for 19-23 fuel channels, Inlet temperature to fuel channels: 303-323 K, Temperature increase in the core: 20-30 deg, Hot leg pressure (in outlet collector): about 0.9-1 MPa, Cold leg pressure (in inlet collector): about 1.7-1.8 MPa, Minimum flow in fuel channels 30 m ³ /h for channels with maximum thermal power 1.8 MW, Minimum flow is 15 m ³ /h for channels with 0.9 MW (in peripheral core position).
Pressurizer	Filled with water and helium gas under high pressure At pressure about 1.7 MPa maintains sufficient water inventory in the circuit.
Safety signals causing reactor scram	1) Decrease of mass flow in the fuel channel in the channel cooling circuit. Each fuel channel is equipped with temperature and mass flow measurements (it is important for calculating the thermal power of the element), a small value of the mass flow in the channel will generate a "low mass flow" signal i.e. a warning signal when the flow drops to 90% of nominal mass flow and an alarm when the flow drops to 80% of nominal mass flow. 2) Kinetics control system. In case of sudden power jump signal is generated through detectors and other systems. It's warning signal when is 110% of nominal reactor power, and alarm signal in case of 120% of nominal power. Additional safety signal for fast reactivity jump it is

alarm signal from increase of period of the reactor.

Reactivity coefficients	<p>Fuel reactivity coefficient (negative) $-0.23\phi/\text{deg}$ to $-0.25\phi/\text{deg}$</p> <p>Coolant reactivity coefficient in the fuel channel (negative) $-1.93\phi/\text{deg}$ to $-2.09\phi/\text{deg}$</p> <p>Coolant reactivity coefficient of the pool plus moderator reactivity coefficient (positive) $+1.9\phi/\text{deg}$</p> <p>Void reactivity coefficient (negative) $-9.37 \phi/\%$ of void to $-9.71\phi/\%$ of void</p> <p>Values of coefficients depend on the beginning or end of the fuel cycle and number of molybdenum channels in the core (none, one or two molybdenum channels).</p>
Control system	<p>The reactor power is controlled through changes of position of the control rods and automatic or manual changes of position of the UAR. The UAR is an automatic regulation system, that through the change of position of one control rod in the reactor core controls the power level and maintains, if it's necessary, the criticality of the reactor.</p>
Shutdown system	<p>The shutdown system is provided through safety rods (insertion reactivity from -7.5% to -11% to the core) and control rods (the weights depend on the position of the rods in the core, it can be pessimistically assumed that the injection is -2.5%). Safety rods and control rods work in accordance to the fail-safe rule. In case of loss of the power supply the safety rods will be automatically released from electromagnets into the reactor core.</p> <p>It's also possible to remove two fuel elements from the core. This is done by moving two fuel type elements (REP). This action is slower than the movement of safety rods. Sometimes it's impossible to remove the REP because of temperature stress until several hours after reactor shutdown. The reactivity of two REPs is about $4.2\pm 0.5\%$.</p> <p>The shutdown system does not depend on the boron injection system.</p>
Emergency core cooling system	<p>In case of low water level in the pressurizer, an additional pump (1u6) that is connected to the pressurizer is automatically switched on and pumps water from the tank system (water volume $20-30\text{m}^3$) into the pressurizer. The solution is good only in case of a small leakage from the channel cooling circuit.</p> <p>The gas discharge system from the pressurizer. In case of very low water level in the pressurizer a discharge of helium</p>

into the tank system through a system of valves will take place. This will result in a sudden depressurization of the channel cooling circuit.

The safety valves 1z100A/B. In case of depressurization the valves automatically open and connect the channel cooling circuit with pool of the reactor (due to the pressure difference between two circuits).

Fuelling	Fuelling is performed when necessary depending on the reactivity supply, however always before a new work cycle. Refuelling, minimum 48 hours after a previous cycle, includes also a possibility of adding fuel elements removed after earlier cycles.
Cooling system	<p>Fuel cooling channels are cooled by two from four pumps. After shut-down is done by two from the four mentioned pumps but with rotation speed changed from 3000r/s to 1500r/s. Hot water from the core passes through the heat exchangers system (four from six) transferring heat to the secondary circuit.</p> <p>The pool is individually cooled by three from four pumps and in shutdown mode - by one from two shutdown pumps.</p> <p>There is one secondary cooling circuit for the fuel cooling circuit and the pool cooling circuit. It pumps water to the outer cooling tower with ventilators. During normal operation two from three pumps and after shutdown one from three shutdown pumps are in operation.</p> <p>During loss of external power after a rapid shutdown, in order to remove decay heat, about 4 hours of cooling with post-shutdown pumps is necessary. The post-shutdown pumps are powered by accumulator batteries or diesel generators.</p>
Moderator	Beryllium blocks are used as a moderator. They are placed between fuel channels.
Reflector	Graphite blocks are used as a reflector. They placed around beryllium blocks and fuel channels.
Operation	The reactor works in cycles lasting from five to ten days with nominal power usually between 16 and 23 MW(th). In some cases the reactor is used for training of students and then it operates for several hours with the power level about 10 kW(th).
Applications	Production of radioactive materials for medicine – mainly

molybdenum production in special molybdenum channels.
Training of students.
Research activities.

Safety analysis

Safety Analysis Report [1] updated in 2009.
Update of the report is planned till 03.2015.

APPENDIX B – INPUT FILE.

**RESEARCH REACTOR 'MARIA'
STEADY STATE CALCULATIONS INPUT
DATE: 26.10.2012**

=MARIA
 *m: SNAP:Symbolic Nuclear Analysis Package, Version 2.2.0,
 September 04, 2012
 *m: PLUGIN:RELAP Version 4.3.0
 *m: CODE:RELAP5 Version 3.3
 *m: DATE:10/26/12

```

*****
***** Model Options
*****
100      new      transnt
*        iunits  ounits
102      si       si
* tend minstep maxstep copt pfreq majed rstrf
201 10.0 1.0e-8 0.5 3 5 100 1000
20500000 9999
***** Control Blocks
*****
20500010 "dP_15-65" sum 1.0 5.882538e5 0 0
*        a0      scale name      param
20500011 0.0      1.0      p      15010000
20500012 -1.0     -1.0     p      65010000
*        name type scale      ival iflag limit
20500020 "dT_10-70" sum 1.0 0.38535583 0 0
*        a0      scale name      param
20500021 0.0      -1.0     tempf  10010000
20500022 1.0      1.0      tempf  70060000
*        name type scale      ival iflag limit
20500030 "Ent_70" mult 1.0 1.743369e6 0 0
*        input  param      input  param
20500031 hvmix 70060000 mflowj 74000000
*        name type scale      ival iflag limit
20500040 "Power" sum 1.0 8973.1709 0 0
*        a0      scale name      param
20500041 0.0      -1.0     cntrivar 5
20500042 1.0      1.0      cntrivar 3
*        name type scale      ival iflag limit
20500050 "Ent_10" mult 1.0 1.734396e6 0 0
*        input  param      input  param
20500051 hvmix 10010000 mflowj 6000000
*        name type scale      ival iflag limit
20500100 "unnamed" sum 1.0 323.40231 0 0
*        a0      scale name      param
20500101 0.0      1.0      httemp 6000113
*        name type scale      ival iflag limit
20500110 "unnamed" sum 1.0 323.46774 0 0
*        a0      scale name      param
20500111 0.0      1.0      httemp 6000213
*        name type scale      ival iflag limit
20500120 "unnamed" sum 1.0 323.52133 0 0
*        a0      scale name      param
20500121 0.0      1.0      httemp 6000313
*        name type scale      ival iflag limit
20500130 "unnamed" sum 1.0 323.55933 0 0
*        a0      scale name      param
20500131 0.0      1.0      httemp 6000413
*        name type scale      ival iflag limit
20500140 "unnamed" sum 1.0 323.57919 0 0
*        a0      scale name      param
20500141 0.0      1.0      httemp 6000513
*        name type scale      ival iflag limit
20500150 "unnamed" sum 1.0 323.57993 0 0
*        a0      scale name      param
20500151 0.0      1.0      httemp 6000613
*        name type scale      ival iflag limit
20500160 "unnamed" sum 1.0 323.56198 0 0
*        a0      scale name      param
20500161 0.0      1.0      httemp 6000713
*        name type scale      ival iflag limit
20500170 "unnamed" sum 1.0 323.5274 0 0
*        a0      scale name      param
20500171 0.0      1.0      httemp 6000813
*        name type scale      ival iflag limit
20500180 "unnamed" sum 1.0 323.47955 0 0
*        a0      scale name      param
20500181 0.0      1.0      httemp 6000913
*        name type scale      ival iflag limit
20500190 "unnamed" sum 1.0 323.45679 0 0
*        a0      scale name      param

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20500191 0.0      1.0      httemp 6001013
*        name type scale      ival iflag limit
20500200 "unnamed" sum 1.0 323.40326 0 0
*        a0      scale name      param
20500201 0.0      1.0      httemp 6000105
*        name type scale      ival iflag limit
20500210 "unnamed" sum 1.0 323.46854 0 0
*        a0      scale name      param
20500211 0.0      1.0      httemp 6000205
*        name type scale      ival iflag limit
20500220 "unnamed" sum 1.0 323.5217 0 0
*        a0      scale name      param
20500221 0.0      1.0      httemp 6000305
*        name type scale      ival iflag limit
20500230 "unnamed" sum 1.0 323.55899 0 0
*        a0      scale name      param
20500231 0.0      1.0      httemp 6000405
*        name type scale      ival iflag limit
20500240 "unnamed" sum 1.0 323.57797 0 0
*        a0      scale name      param
20500241 0.0      1.0      httemp 6000505
*        name type scale      ival iflag limit
20500250 "unnamed" sum 1.0 323.57767 0 0
*        a0      scale name      param
20500251 0.0      1.0      httemp 6000605
*        name type scale      ival iflag limit
20500260 "unnamed" sum 1.0 323.55865 0 0
*        a0      scale name      param
20500261 0.0      1.0      httemp 6000705
*        name type scale      ival iflag limit
20500270 "unnamed" sum 1.0 323.52307 0 0
*        a0      scale name      param
20500271 0.0      1.0      httemp 6000805
*        name type scale      ival iflag limit
20500280 "unnamed" sum 1.0 323.47437 0 0
*        a0      scale name      param
20500281 0.0      1.0      httemp 6000905
*        name type scale      ival iflag limit
20500290 "unnamed" sum 1.0 323.45117 0 0
*        a0      scale name      param
20500291 0.0      1.0      httemp 6001005
*        name type scale      ival iflag limit
20500300 "unnamed" sum 1.0 323.42294 0 0
*        a0      scale name      param
20500301 0.0      1.0      httemp 5500113
*        name type scale      ival iflag limit
20500310 "unnamed" sum 1.0 323.49878 0 0
*        a0      scale name      param
20500311 0.0      1.0      httemp 5500213
*        name type scale      ival iflag limit
20500320 "unnamed" sum 1.0 323.56104 0 0
*        a0      scale name      param
20500321 0.0      1.0      httemp 5500313
*        name type scale      ival iflag limit
20500330 "unnamed" sum 1.0 323.60513 0 0
*        a0      scale name      param
20500331 0.0      1.0      httemp 5500413
*        name type scale      ival iflag limit
20500340 "unnamed" sum 1.0 323.62796 0 0
*        a0      scale name      param
20500341 0.0      1.0      httemp 5500513
*        name type scale      ival iflag limit
20500350 "unnamed" sum 1.0 323.62811 0 0
*        a0      scale name      param
20500351 0.0      1.0      httemp 5500613
*        name type scale      ival iflag limit
20500360 "unnamed" sum 1.0 323.60602 0 0
*        a0      scale name      param
20500361 0.0      1.0      httemp 5500713
*        name type scale      ival iflag limit
20500370 "unnamed" sum 1.0 323.5639 0 0
*        a0      scale name      param
20500371 0.0      1.0      httemp 5500813
*        name type scale      ival iflag limit
20500380 "unnamed" sum 1.0 323.50562 0 0
*        a0      scale name      param
20500381 0.0      1.0      httemp 5500913
*        name type scale      ival iflag limit

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20500390 "unnamed" sum 1.0 323.47556 0 0
* a0 scale name param
20500391 0.0 1.0 htemp 5501013
* name type scale ival iflag limit
20500400 "unnamed" sum 1.0 323.43329 0 0
* a0 scale name param
20500401 0.0 1.0 htemp 5500105
* name type scale ival iflag limit
20500410 "unnamed" sum 1.0 323.51294 0 0
* a0 scale name param
20500411 0.0 1.0 htemp 5500205
* name type scale ival iflag limit
20500420 "unnamed" sum 1.0 323.57779 0 0
* a0 scale name param
20500421 0.0 1.0 htemp 5500305
* name type scale ival iflag limit
20500430 "unnamed" sum 1.0 323.62311 0 0
* a0 scale name param
20500431 0.0 1.0 htemp 5500405
* name type scale ival iflag limit
20500440 "unnamed" sum 1.0 323.64563 0 0
* a0 scale name param
20500441 0.0 1.0 htemp 5500505
* name type scale ival iflag limit
20500450 "unnamed" sum 1.0 323.64407 0 0
* a0 scale name param
20500451 0.0 1.0 htemp 5500605
* name type scale ival iflag limit
20500460 "unnamed" sum 1.0 323.61902 0 0
* a0 scale name param
20500461 0.0 1.0 htemp 5500705
* name type scale ival iflag limit
20500470 "unnamed" sum 1.0 323.57294 0 0
* a0 scale name param
20500471 0.0 1.0 htemp 5500805
* name type scale ival iflag limit
20500480 "unnamed" sum 1.0 323.51001 0 0
* a0 scale name param
20500481 0.0 1.0 htemp 5500905
* name type scale ival iflag limit
20500490 "unnamed" sum 1.0 323.47787 0 0
* a0 scale name param
20500491 0.0 1.0 htemp 5501005
* name type scale ival iflag limit
20500500 "unnamed" sum 1.0 323.45538 0 0
* a0 scale name param
20500501 0.0 1.0 htemp 5000113
* name type scale ival iflag limit
20500510 "unnamed" sum 1.0 323.52072 0 0
* a0 scale name param
20500511 0.0 1.0 htemp 5000213
* name type scale ival iflag limit
20500520 "unnamed" sum 1.0 323.56552 0 0
* a0 scale name param
20500521 0.0 1.0 htemp 5000313
* name type scale ival iflag limit
20500530 "unnamed" sum 1.0 323.58615 0 0
* a0 scale name param
20500531 0.0 1.0 htemp 5000413
* name type scale ival iflag limit
20500540 "unnamed" sum 1.0 323.58093 0 0
* a0 scale name param
20500541 0.0 1.0 htemp 5000513
* name type scale ival iflag limit
20500550 "unnamed" sum 1.0 323.55032 0 0
* a0 scale name param
20500551 0.0 1.0 htemp 5000613
* name type scale ival iflag limit
20500560 "unnamed" sum 1.0 323.49677 0 0
* a0 scale name param
20500561 0.0 1.0 htemp 5000713
* name type scale ival iflag limit
20500570 "unnamed" sum 1.0 323.42453 0 0
* a0 scale name param
20500571 0.0 1.0 htemp 5000813
* name type scale ival iflag limit
20500580 "unnamed" sum 1.0 323.33942 0 0
* a0 scale name param

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20500581 0.0 1.0 htemp 5000913
* name type scale ival iflag limit
20500590 "unnamed" sum 1.0 323.29184 0 0
* a0 scale name param
20500591 0.0 1.0 htemp 5001013
* name type scale ival iflag limit
20500600 "unnamed" sum 1.0 323.4418 0 0
* a0 scale name param
20500601 0.0 1.0 htemp 5000105
* name type scale ival iflag limit
20500610 "unnamed" sum 1.0 323.50943 0 0
* a0 scale name param
20500611 0.0 1.0 htemp 5000205
* name type scale ival iflag limit
20500620 "unnamed" sum 1.0 323.55914 0 0
* a0 scale name param
20500621 0.0 1.0 htemp 5000305
* name type scale ival iflag limit
20500630 "unnamed" sum 1.0 323.58707 0 0
* a0 scale name param
20500631 0.0 1.0 htemp 5000405
* name type scale ival iflag limit
20500640 "unnamed" sum 1.0 323.59106 0 0
* a0 scale name param
20500641 0.0 1.0 htemp 5000505
* name type scale ival iflag limit
20500650 "unnamed" sum 1.0 323.57092 0 0
* a0 scale name param
20500651 0.0 1.0 htemp 5000605
* name type scale ival iflag limit
20500660 "unnamed" sum 1.0 323.52841 0 0
* a0 scale name param
20500661 0.0 1.0 htemp 5000705
* name type scale ival iflag limit
20500670 "unnamed" sum 1.0 323.46704 0 0
* a0 scale name param
20500671 0.0 1.0 htemp 5000805
* name type scale ival iflag limit
20500680 "unnamed" sum 1.0 323.39188 0 0
* a0 scale name param
20500681 0.0 1.0 htemp 5000905
* name type scale ival iflag limit
20500690 "unnamed" sum 1.0 323.3504 0 0
* a0 scale name param
20500691 0.0 1.0 htemp 5001005
* name type scale ival iflag limit
20500700 "unnamed" sum 1.0 323.52029 0 0
* a0 scale name param
20500701 0.0 1.0 htemp 3000113
* name type scale ival iflag limit
20500710 "unnamed" sum 1.0 323.58707 0 0
* a0 scale name param
20500711 0.0 1.0 htemp 3000213
* name type scale ival iflag limit
20500720 "unnamed" sum 1.0 323.62198 0 0
* a0 scale name param
20500721 0.0 1.0 htemp 3000313
* name type scale ival iflag limit
20500730 "unnamed" sum 1.0 323.62195 0 0
* a0 scale name param
20500731 0.0 1.0 htemp 3000413
* name type scale ival iflag limit
20500740 "unnamed" sum 1.0 323.58676 0 0
* a0 scale name param
20500741 0.0 1.0 htemp 3000513
* name type scale ival iflag limit
20500750 "unnamed" sum 1.0 323.51904 0 0
* a0 scale name param
20500751 0.0 1.0 htemp 3000613
* name type scale ival iflag limit
20500760 "unnamed" sum 1.0 323.42395 0 0
* a0 scale name param
20500761 0.0 1.0 htemp 3000713
* name type scale ival iflag limit
20500770 "unnamed" sum 1.0 323.30902 0 0
* a0 scale name param
20500771 0.0 1.0 htemp 3000813
* name type scale ival iflag limit

```

20500780	"unnamed"	sum	1.0	323.18326	0	0
*	a0	scale		name	param	
20500781	0.0	1.0	httemp	3000913		
*	name	type	scale	ival	iflag	limit
20500790	"unnamed"	sum	1.0	323.11334	0	0
*	a0	scale		name	param	
20500791	0.0	1.0	httemp	3001013		
*	name	type	scale	ival	iflag	limit
20500800	"unnamed"	sum	1.0	323.5889	0	0
*	a0	scale		name	param	
20500801	0.0	1.0	httemp	3000205		
*	name	type	scale	ival	iflag	limit
20500810	"unnamed"	sum	1.0	323.52145	0	0
*	a0	scale		name	param	
20500811	0.0	1.0	httemp	3000105		
*	name	type	scale	ival	iflag	limit
20500820	"unnamed"	sum	1.0	323.62451	0	0
*	a0	scale		name	param	
20500821	0.0	1.0	httemp	3000305		
*	name	type	scale	ival	iflag	limit
20500830	"unnamed"	sum	1.0	323.62512	0	0
*	a0	scale		name	param	
20500831	0.0	1.0	httemp	3000405		
*	name	type	scale	ival	iflag	limit
20500840	"unnamed"	sum	1.0	323.59042	0	0
*	a0	scale		name	param	
20500841	0.0	1.0	httemp	3000505		
*	name	type	scale	ival	iflag	limit
20500850	"unnamed"	sum	1.0	323.52289	0	0
*	a0	scale		name	param	
20500851	0.0	1.0	httemp	3000605		
*	name	type	scale	ival	iflag	limit
20500860	"unnamed"	sum	1.0	323.42776	0	0
*	a0	scale		name	param	
20500861	0.0	1.0	httemp	3000705		
*	name	type	scale	ival	iflag	limit
20500870	"unnamed"	sum	1.0	323.31241	0	0
*	a0	scale		name	param	
20500871	0.0	1.0	httemp	3000805		
*	name	type	scale	ival	iflag	limit
20500880	"unnamed"	sum	1.0	323.18585	0	0
*	a0	scale		name	param	
20500881	0.0	1.0	httemp	3000905		
*	name	type	scale	ival	iflag	limit
20500890	"unnamed"	sum	1.0	323.11505	0	0
*	a0	scale		name	param	
20500891	0.0	1.0	httemp	3001005		
*	name	type	scale	ival	iflag	limit
20500900	"unnamed"	sum	1.0	323.50284	0	0
*	a0	scale		name	param	
20500901	0.0	1.0	httemp	2500113		
*	name	type	scale	ival	iflag	limit
20500910	"unnamed"	sum	1.0	323.58917	0	0
*	a0	scale		name	param	
20500911	0.0	1.0	httemp	2500213		
*	name	type	scale	ival	iflag	limit
20500920	"unnamed"	sum	1.0	323.64075	0	0
*	a0	scale		name	param	
20500921	0.0	1.0	httemp	2500313		
*	name	type	scale	ival	iflag	limit
20500930	"unnamed"	sum	1.0	323.65314	0	0
*	a0	scale		name	param	
20500931	0.0	1.0	httemp	2500413		
*	name	type	scale	ival	iflag	limit
20500940	"unnamed"	sum	1.0	323.62518	0	0
*	a0	scale		name	param	
20500941	0.0	1.0	httemp	2500513		
*	name	type	scale	ival	iflag	limit
20500950	"unnamed"	sum	1.0	323.55893	0	0
*	a0	scale		name	param	
20500951	0.0	1.0	httemp	2500613		
*	name	type	scale	ival	iflag	limit
20500960	"unnamed"	sum	1.0	323.45953	0	0
*	a0	scale		name	param	
20500961	0.0	1.0	httemp	2500713		
*	name	type	scale	ival	iflag	limit
20500970	"unnamed"	sum	1.0	323.33487	0	0
*	a0	scale		name	param	
20500971	0.0	1.0	httemp	2500813		
*	name	type	scale	ival	iflag	limit
20500980	"unnamed"	sum	1.0	323.19482	0	0
*	a0	scale		name	param	
20500981	0.0	1.0	httemp	2500913		
*	name	type	scale	ival	iflag	limit
20500990	"unnamed"	sum	1.0	323.11862	0	0
*	a0	scale		name	param	
20500991	0.0	1.0	httemp	2501013		
*	name	type	scale	ival	iflag	limit
20501000	"unnamed"	sum	1.0	323.51813	0	0
*	a0	scale		name	param	
20501001	0.0	1.0	httemp	2500105		
*	name	type	scale	ival	iflag	limit
20501010	"unnamed"	sum	1.0	323.60406	0	0
*	a0	scale		name	param	
20501011	0.0	1.0	httemp	2500205		
*	name	type	scale	ival	iflag	limit
20501020	"unnamed"	sum	1.0	323.65451	0	0
*	a0	scale		name	param	
20501021	0.0	1.0	httemp	2500305		
*	name	type	scale	ival	iflag	limit
20501030	"unnamed"	sum	1.0	323.66528	0	0
*	a0	scale		name	param	
20501031	0.0	1.0	httemp	2500405		
*	name	type	scale	ival	iflag	limit
20501040	"unnamed"	sum	1.0	323.63525	0	0
*	a0	scale		name	param	
20501041	0.0	1.0	httemp	2500505		
*	name	type	scale	ival	iflag	limit
20501050	"unnamed"	sum	1.0	323.56671	0	0
*	a0	scale		name	param	
20501051	0.0	1.0	httemp	2500605		
*	name	type	scale	ival	iflag	limit
20501060	"unnamed"	sum	1.0	323.465	0	0
*	a0	scale		name	param	
20501061	0.0	1.0	httemp	2500705		
*	name	type	scale	ival	iflag	limit
20501070	"unnamed"	sum	1.0	323.3382	0	0
*	a0	scale		name	param	
20501071	0.0	1.0	httemp	2500805		
*	name	type	scale	ival	iflag	limit
20501080	"unnamed"	sum	1.0	323.19641	0	0
*	a0	scale		name	param	
20501081	0.0	1.0	httemp	2500905		
*	name	type	scale	ival	iflag	limit
20501090	"unnamed"	sum	1.0	323.11926	0	0
*	a0	scale		name	param	
20501091	0.0	1.0	httemp	2501005		
*	name	type	scale	ival	iflag	limit
20501100	"unnamed"	sum	1.0	323.6972	0	0
*	a0	scale		name	param	
20501101	0.0	1.0	httemp	2500409		
*	name	type	scale	ival	iflag	limit
20501110	"unnamed"	powerr	1.0	0.52376056	0	0
*	input	param		power		
20501111	cntrlvar		114	-0.23		
*	name	type	scale	ival	iflag	limit
20501120	"unnamed"	powerr	1.0	25.589294	0	0
*	input	param		power		
20501121	htrnr		2500400	0.35		
*	name	type	scale	ival	iflag	limit
20501130	"T_ONBR"	sum	1.0	478.85593	0	0
*	a0	scale		name	param	
20501131	0.0	1.0	sattemp	25040000		
20501132	0.182	cntrlvar		115		
*	name	type	scale	ival	iflag	limit
20501140	"unnamed"	sum	1.0	16.640322	0	0
*	a0	scale		name	param	
20501141	0.0	1.0e-5	p	25040000		
*	name	type	scale	ival	iflag	limit
20501150	"unnamed"	mult	1.0	13.402663	0	0
*	input	param		input	param	
20501151	cntrlvar		111	cntrlvar		112
*	name	type	scale	ival	iflag	limit
20501160	"unnamed"	sum	1.0	0.60251117	0	0
*	a0	scale		name	param	
20501161	0.0	1.0	httemp	2500401		

```

20501162      -1.0 tempf 10010000
*      name type scale ival iflag limit
20501170 "unnamed" sum 1.0 155.84138 0 0
*      a0 scale name param
20501171      0.0 1.0 cntrlvar 113
20501172      -1.0 tempf 10010000
*      name type scale ival iflag limit
20501180 "unnamed" powerr 1.0 1.6597203 0 0
*      input param power
20501181 cntrlvar 116 -1.0
*      name type scale ival iflag limit
20501190 "ONBR" mult 1.0 258.65311 0 0
*      input param input param
20501191 cntrlvar 117 cntrlvar 118
20600000 expanded
***** Variable Trips
*****n: Pressure_signal
*      var param r var param acon l timeo
20600010 p 10010000 le null 0 9.0 l -1.0
*n: Scram_delay
*      var param r var param acon l timeo
20600020 time 0 gt timeof 1001 0.35 l -1.0
*n: A120 Power_signal
*      var param r var param acon l timeo
20600030 rktpow 0 ge null 0 2.16e6 l -1.0
*n: LOOS OF COOLANT FLOW
*      var param r var param acon l timeo
20600040 time 0 ge null 0 160.0 l -1.0
*n: RIA_FAST
*      var param r var param acon l timeo
20600050 time 0 ge null 0 160.0 l -1.0
*n: RIA_SLOW
*      var param r var param acon l timeo
20600060 time 0 ge null 0 160.0 l -1.0
***** Logical Trips
*****n: SCRAM
*      trip1 oper trip2 l timeo
20610010 3 or 1 l -1.0
***** General Tables
*****n: ENVI
*      type trip
20200100 temp 0
*      Time Temperature
20200101 0.0 300.0
*n: PK + PAR
*      type trip factor1 factor2
20200200 reac-t 2 1.0 -2.0
*      Time Reactivity
20200201 0.0 0.0
20200202 0.01 5.0e-3
20200203 0.02 0.01
20200204 0.03 0.022
20200205 0.04 0.035
20200206 0.05 0.05
20200207 0.06 0.07
20200208 0.07 0.09
20200209 0.08 0.11
20200210 0.09 0.145
20200211 0.1 0.165
20200212 0.11 0.2
20200213 0.12 0.23
20200214 0.13 0.275
20200215 0.14 0.31
20200216 0.15 0.35
20200217 0.16 0.4
20200218 0.17 0.45
20200219 0.18 0.49
20200220 0.19 0.525
20200221 0.2 0.565
20200222 0.21 0.6
20200223 0.22 0.64
20200224 0.23 0.675
20200225 0.24 0.72
20200226 0.25 0.75
20200227 0.26 0.79
20200228 0.27 0.825
20200229 0.28 0.85
20200230 0.29 0.88

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20200231      0.3 0.9
20200232      0.35 0.975
20200233      0.36 0.983
20200234      0.37 0.99
20200235      0.38 0.999
20200236      0.39 1.0
*n: PB
*      type trip factor1 factor2
20200300 reac-t 2 1.0 -3.5
*      Time Reactivity
20200301 0.0 0.0
20200302 0.01 0.0
20200303 0.02 0.0
20200304 0.03 0.0
20200305 0.04 0.0
20200306 0.05 0.0
20200307 0.06 1.0e-3
20200308 0.07 2.0e-3
20200309 0.08 3.0e-3
20200310 0.09 4.0e-3
20200311 0.1 5.0e-3
20200312 0.11 6.0e-3
20200313 0.12 7.0e-3
20200314 0.13 8.0e-3
20200315 0.14 9.0e-3
20200316 0.15 0.01
20200317 0.16 0.013
20200318 0.17 0.016
20200319 0.18 0.019
20200320 0.19 0.022
20200321 0.2 0.025
20200322 0.21 0.03
20200323 0.22 0.04
20200324 0.23 0.05
20200325 0.24 0.06
20200326 0.25 0.07
20200327 0.26 0.085
20200328 0.27 0.1
20200329 0.28 0.118
20200330 0.29 0.135
20200331 0.3 0.157
20200332 0.35 0.3
20200333 0.36 0.32
20200334 0.37 0.345
20200335 0.38 0.38
20200336 0.39 0.41
20200337 0.4 0.45
20200338 0.41 0.49
20200339 0.42 0.515
20200340 0.43 0.55
20200341 0.44 0.59
20200342 0.45 0.62
20200343 0.46 0.66
20200344 0.47 0.7
20200345 0.48 0.735
20200346 0.49 0.77
20200347 0.5 0.8
20200348 0.51 0.825
20200349 0.52 0.86
20200350 0.53 0.89
20200351 0.54 0.905
20200352 0.55 0.925
20200353 0.56 0.935
20200354 0.57 0.95
20200355 0.58 0.963
20200356 0.59 0.975
20200357 0.6 0.985
20200358 0.63 1.0
*n: Reactivity_Slow
*      type trip
20200400 reac-t 6
*      Time Reactivity
20200401 -1.0 0.0
20200402 0.0 0.0
20200403 1.0 0.04
20200404 2.0 0.08
20200405 3.0 0.12
20200406 4.0 0.16

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20200407	5.0	0.2
20200408	6.0	0.24
20200409	7.0	0.28
20200410	8.0	0.32
20200411	9.0	0.36
20200412	10.0	0.4
20200413	11.0	0.44
20200414	12.0	0.48
20200415	13.0	0.52
20200416	14.0	0.56
20200417	15.0	0.6
20200418	16.0	0.64
20200419	17.0	0.68
20200420	18.0	0.72
20200421	19.0	0.76
20200422	20.0	0.8
20200423	21.0	0.84
20200424	22.0	0.88
20200425	23.0	0.92
20200426	24.0	0.96
20200427	25.0	1.0
20200428	26.0	1.04
20200429	27.0	1.08
20200430	28.0	1.12
20200431	29.0	1.16
20200432	30.0	1.2
20200433	31.0	1.24
20200434	32.0	1.28
20200435	33.0	1.32
20200436	34.0	1.36
20200437	35.0	1.4
20200438	36.0	1.44
20200439	37.0	1.48
20200440	38.0	1.52
20200441	39.0	1.56
20200442	40.0	1.6
20200443	41.0	1.64
20200444	42.0	1.68
20200445	43.0	1.72
20200446	44.0	1.76
20200447	45.0	1.8
20200448	46.0	1.84
20200449	47.0	1.88
20200450	48.0	1.92
20200451	49.0	1.96
20200452	50.0	2.0

*n: Reactivity_Fast

* type trip		
20200500	react-t	5
* Time Reactivity		
20200501	-1.0	0.0
20200502	0.0	0.0
20200503	0.01	0.04
20200504	0.02	0.08
20200505	0.03	0.12
20200506	0.04	0.16
20200507	0.05	0.2
20200508	0.06	0.24
20200509	0.07	0.28
20200510	0.08	0.32
20200511	0.09	0.36
20200512	0.1	0.4
20200513	0.11	0.44
20200514	0.12	0.48
20200515	0.13	0.52
20200516	0.14	0.56
20200517	0.15	0.6
20200518	0.16	0.64
20200519	0.17	0.68
20200520	0.18	0.72
20200521	0.19	0.76
20200522	0.2	0.8
20200523	0.21	0.84
20200524	0.22	0.88
20200525	0.23	0.92
20200526	0.24	0.96
20200527	0.25	1.0
20200528	0.26	1.04

20200529	0.27	1.08
20200530	0.28	1.12
20200531	0.29	1.16
20200532	0.3	1.2
20200533	0.31	1.24
20200534	0.32	1.28
20200535	0.33	1.32
20200536	0.34	1.36
20200537	0.35	1.4
20200538	0.36	1.44
20200539	0.37	1.48
20200540	0.375	1.5

*n: Power_for_SS

* type trip		
20200600	power	0
* Time Power		
20200601	-1.0	1.8e6
20200602	0.0	1.8e6
20200603	1.0	1.8e6
20200604	1.0e6	1.8e6

*****n: Materials

Fuel

* type tflag vflag			
20100100	tbl/fctn	1	1
* thcond			
20100101	59.0		
* temp capacity			
20100151	273.0	0.35837293	
20100152	303.0	0.35837293	
20100153	313.0	0.37012693	
20100154	323.0	0.38188093	
20100155	333.0	0.39363493	
20100156	343.0	0.40538893	
20100157	353.0	0.41714293	
20100158	363.0	0.42889693	
20100159	373.0	0.44065093	
20100160	383.0	0.45240493	
20100161	393.0	0.46415893	
20100162	403.0	0.47591293	
20100163	413.0	0.48766693	
20100164	423.0	0.49942093	
20100165	433.0	0.51117493	
20100166	443.0	0.52292893	
20100167	453.0	0.53468293	
20100168	463.0	0.54643693	
20100169	473.0	0.55819093	
20100170	523.0	0.61696093	
20100171	573.0	0.67573093	
20100172	623.0	0.73450093	
20100173	673.0	0.79327093	
20100174	723.0	0.85204093	
20100175	773.0	0.91081093	
20100176	823.0	0.96958093	
20100177	873.0	1.0283509	
20100178	923.0	1.0871209	
20100179	973.0	1.1458909	
20100180	2000.0	1.1458909	

*n: AGN cladding

* type tflag vflag			
20100200	tbl/fctn	1	1
* thcond			
20100201	130.0		
* heat Capacity			
20100251	2.3496e6		

*n: Aluminium

* type tflag vflag			
20100300	tbl/fctn	1	1
* temp thcond			
20100301	273.0	237.0	
20100302	300.0	237.0	
20100303	350.0	240.0	
20100304	400.0	240.0	
20100305	500.0	236.0	
20100306	600.0	231.0	
20100307	800.0	218.0	
20100308	1200.0	218.0	
* temp capacity			
20100351	273.0	2.4219e6	

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20100352 298.0 2.4219e6
20100353 350.0 2.51262e6
20100354 400.0 2.57985e6
20100355 500.0 2.68596e6
20100356 600.0 2.7918e6
20100357 1000.0 2.7918e6
*n: SAW
* type tflag vflag
20100400 tbl/ctn 1 1
* temp thcond
20100401 273.0 170.0
20100402 900.0 170.0
* temp capacity
20100451 273.0 2.4192e6
20100452 900.0 2.4192e6
***** Hydraulic Components
***** name type
0050000 "unnamed" tmdpvol
* area length vol
0050101 20.0 20.0 0.0
* az-angle inc-angle dz
0050102 0.0 90.0 20.0
* x-rough x-hd flags
0050103 0.0 0.0 0
* cword
0050200 3
* srch press temp
0050201 0.0 1.4e6 323.15
0050202 0.99 1.4e6 323.15
0050203 1.0 1.4e6 323.15
* name type
0060000 "unnamed" tmdpjun
* from to area jefvcahs
0060101 5010002 10010001 2.294e-3 0
* control
0060200 1
* srch mfl mfv unused
0060201 0.0 7.41 0.0 0.0
* name type
0100000 "unnamed" pipe
* ncells
0100001 6
* x-area volid
0100101 2.294e-3 6
* x-length volid
0100301 0.3 1
0100302 0.5 4
0100303 0.4 5
0100304 0.2 6
* volume volid
0100401 0.0 6
* azim-angle volid
0100501 0.0 6
* vert-angle volid
0100601 -90.0 6
* x-wall xhd volid
0100801 1.0e-5 0.027 6
* x-flags volid
0101001 0 6
* ebt press water-ie steam-ie void none id
0101201 000 1.698744e6 2.085118e5 2.596097e6 0.0 0.0 1
0101202 000 1.700844e6 2.085396e5 2.596122e6 0.0 0.0 2
0101203 000 1.703468e6 2.085674e5 2.596154e6 0.0 0.0 3
0101204 000 1.706092e6 2.085951e5 2.596185e6 0.0 0.0 4
0101205 000 1.708454e6 2.086174e5 2.596214e6 0.0 0.0 5
0101206 000 1.710028e6 2.086285e5 2.596232e6 0.0 0.0 6
* jefvcahs jun num
0101101 00000000 5
* vl vv unused junid
0101301 3.6371021 3.6371021 0.0 1
0101302 3.63711 3.63711 0.0 2
0101303 3.6371169 3.6371169 0.0 3
0101304 3.6371241 3.6371241 0.0 4
0101305 3.6371293 3.6371293 0.0 5
* hd corr gas slope junid
0101401 0.027 0.0 1.0 1.0 5
* name type
0150000 "unnamed" branch

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* njuns
0150001 4
* area length vol
0150101 2.294e-3 0.1 0.0
* az-angle inc-angle dz
0150102 0.0 -90.0 -0.1
* x-rough x-hd flags
0150103 0.0 0.0 0
* ebt press water-ie steam-ie void
0150200 000 1.710953e6 2.086334e5 2.596243e6
0.0
* from to area
0151101 15010001 10060002 2.294e-3
* fwd. loss rev. loss efvcahs
0151102 0.0 0.0 0
* hyd diam ccfl wght ccfl gas ccfl slope
0151110 0.027 0.0 1.0 1.0
* vl vv unused
0151201 -3.6371312 -3.6371312 0.0
* from to area
0152101 15010002 20010001 5.24e-4
* fwd. loss rev. loss efvcahs
0152102 0.4 0.4 0
* vl vv unused
0152201 6.1487789 6.1487789 0.0
* from to area
0153101 15010002 25010001 4.54e-4
* fwd. loss rev. loss efvcahs
0153102 0.4 0.4 0
* vl vv unused
0153201 6.1307321 6.1307321 0.0
* from to area
0154101 15010002 30010001 3.83e-4
* fwd. loss rev. loss efvcahs
0154102 0.4 0.4 0
* vl vv unused
0154201 6.1051373 6.1051373 0.0
* name type
0200000 "unnamed" pipe
* ncells
0200001 12
* x-area volid
0200101 5.24e-4 12
* x-length volid
0200301 0.05 1
0200302 0.1 11
0200303 0.05 12
* volume volid
0200401 0.0 12
* azim-angle volid
0200501 0.0 12
* vert-angle volid
0200601 -90.0 12
* x-wall xhd volid
0200801 1.0e-5 4.827e-3 12
* x-flags volid
0201001 0 12
* ebt press temp none none none id
0201201 003 1.689443e6 323.045 0.0 0.0 0.0 1
* ebt press water-ie steam-ie void none id
0201202 000 1.682478e6 2.086602e5 2.595899e6 0.0 0.0 2
* ebt press water-ie steam-ie void none id
0201203 000 1.673191e6 2.086929e5 2.595784e6 0.0 0.0 3
* ebt press water-ie steam-ie void none id
0201204 000 1.663904e6 2.087463e5 2.595668e6 0.0 0.0 4
* ebt press water-ie steam-ie void none id
0201205 000 1.654618e6 2.088172e5 2.595551e6 0.0 0.0 5
* ebt press water-ie steam-ie void none id
0201206 000 1.645331e6 2.089011e5 2.595432e6 0.0 0.0 6
* ebt press water-ie steam-ie void none id
0201207 000 1.636045e6 2.089922e5 2.595312e6 0.0 0.0 7
* ebt press water-ie steam-ie void none id
0201208 000 1.626759e6 2.090844e5 2.595191e6 0.0 0.0 8
* ebt press water-ie steam-ie void none id
0201209 000 1.617473e6 2.091712e5 2.595068e6 0.0 0.0 9
* ebt press water-ie steam-ie void none id
0201210 000 1.608187e6 2.092468e5 2.594944e6 0.0 0.0 10
* ebt press water-ie steam-ie void none id

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0201211 000 1.598902e6 2.093061e5 2.594818e6 0.0 0.0 11
* ebt press water-ie steam-ie void none id
0201212 000 1.591937e6 2.093155e5 2.594723e6 0.0 0.0 12
* area jun
0200201 5.24e-4 11
* jefvcahs jun num
0201101 00000000 11
* vl vv unused junid
0201301 6.1488385 6.1488385 0.0 1
0201302 6.1488714 6.1488714 0.0 2
0201303 6.1489172 6.1489172 0.0 3
0201304 6.1489778 6.1489778 0.0 4
0201305 6.1490493 6.1490493 0.0 5
0201306 6.1491299 6.1491299 0.0 6
0201307 6.1492157 6.1492157 0.0 7
0201308 6.149302 6.149302 0.0 8
0201309 6.1493845 6.1493845 0.0 9
0201310 6.1494598 6.1494598 0.0 10
0201311 6.1495237 6.1495237 0.0 11
* hd corr gas slope junid
0201401 4.827e-3 0.0 1.0 1.0 11
* name type
0250000 "unnamed" pipe
* ncells
0250001 12
* x-area valid
0250101 4.54e-4 12
* x-length valid
0250301 0.05 1
0250302 0.1 11
0250303 0.05 12
* volume valid
0250401 0.0 12
* azim-angle valid
0250501 0.0 12
* vert-angle valid
0250601 -90.0 12
* x-wall xhd valid
0250801 1.0e-5 4.802e-3 12
* x-flags valid
0251001 0 12
* ebt press water-ie steam-ie void none id
0251201 000 1.689598e6 2.086388e5 2.595986e6 0.0 0.0 1
0251202 000 1.682626e6 2.086712e5 2.595901e6 0.0 0.0 2
0251203 000 1.673329e6 2.087246e5 2.595786e6 0.0 0.0 3
0251204 000 1.664032e6 2.088165e5 2.59567e6 0.0 0.0 4
0251205 000 1.654736e6 2.0894e5 2.595552e6 0.0 0.0 5
0251206 000 1.645439e6 2.090854e5 2.595434e6 0.0 0.0 6
0251207 000 1.636143e6 2.092415e5 2.595314e6 0.0 0.0 7
0251208 000 1.626848e6 2.093963e5 2.595192e6 0.0 0.0 8
0251209 000 1.617552e6 2.095376e5 2.595069e6 0.0 0.0 9
0251210 000 1.608257e6 2.096547e5 2.594945e6 0.0 0.0 10
0251211 000 1.598962e6 2.097386e5 2.594819e6 0.0 0.0 11
0251212 000 1.591991e6 2.09739e5 2.594724e6 0.0 0.0 12
* area jun
0250201 4.54e-4 11
* jefvcahs jun num
0251101 00000000 11
* vl vv unused junid
0251301 6.1307912 6.1307912 0.0 1
0251302 6.1308308 6.1308308 0.0 2
0251303 6.1308908 6.1308908 0.0 3
0251304 6.1309767 6.1309767 0.0 4
0251305 6.1310835 6.1310835 0.0 5
0251306 6.1312056 6.1312056 0.0 6
0251307 6.1313348 6.1313348 0.0 7
0251308 6.1314626 6.1314626 0.0 8
0251309 6.1315818 6.1315818 0.0 9
0251310 6.1316848 6.1316848 0.0 10
0251311 6.1317654 6.1317654 0.0 11
* hd corr gas slope junid
0251401 4.802e-3 0.0 1.0 1.0 11
* name type
0300000 "unnamed" pipe
* ncells
0300001 12
* x-area valid
0300101 3.83e-4 12

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* x-length valid
0300301 0.05 1
0300302 0.1 11
0300303 0.05 12
* volume valid
0300401 0.0 12
* azim-angle valid
0300501 0.0 12
* vert-angle valid
0300601 -90.0 12
* x-wall xhd valid
0300801 1.0e-5 4.767e-3 12
* x-flags valid
0301001 0 12
* ebt press water-ie steam-ie void none id
0301201 000 1.689816e6 2.086581e5 2.595989e6 0.0 0.0 1
0301202 000 1.682834e6 2.087158e5 2.595904e6 0.0 0.0 2
0301203 000 1.673524e6 2.087883e5 2.595789e6 0.0 0.0 3
0301204 000 1.664214e6 2.088898e5 2.595672e6 0.0 0.0 4
0301205 000 1.654904e6 2.090142e5 2.595555e6 0.0 0.0 5
0301206 000 1.645594e6 2.091535e5 2.595436e6 0.0 0.0 6
0301207 000 1.636285e6 2.092983e5 2.595316e6 0.0 0.0 7
0301208 000 1.626976e6 2.094388e5 2.595194e6 0.0 0.0 8
0301209 000 1.617667e6 2.095653e5 2.595071e6 0.0 0.0 9
0301210 000 1.608359e6 2.096694e5 2.594946e6 0.0 0.0 10
0301211 000 1.599051e6 2.097441e5 2.594826e6 0.0 0.0 11
0301212 000 1.59207e6 2.097471e5 2.594725e6 0.0 0.0 12
* area jun
0300201 3.83e-4 11
* jefvcahs jun num
0301101 00000000 11
* vl vv unused junid
0301301 6.1052089 6.1052089 0.0 1
0301302 6.1052651 6.1052651 0.0 2
0301303 6.1053376 6.1053376 0.0 3
0301304 6.1054296 6.1054296 0.0 4
0301305 6.1055369 6.1055369 0.0 5
0301306 6.1056542 6.1056542 0.0 6
0301307 6.1057749 6.1057749 0.0 7
0301308 6.1058931 6.1058931 0.0 8
0301309 6.1060019 6.1060019 0.0 9
0301310 6.1060958 6.1060958 0.0 10
0301311 6.1061702 6.1061702 0.0 11
* hd corr gas slope junid
0301401 4.767e-3 0.0 1.0 1.0 11
* name type
0350000 "unnamed" branch
* njuns
0350001 4
* area length vol
0350101 2.294e-3 0.05 0.0
* az-angle inc-angle dz
0350102 0.0 -90.0 -0.05
* x-rough x-hd flags
0350103 0.0 0.0 0
* ebt press water-ie steam-ie void
0350200 000 1.592632e6 2.095778e5 2.594733e6
0.0
* from to area
0351101 35010002 40010001 2.294e-3
* fwd. loss rev. loss efvcahs
0351102 1.5 1.5 0
* vl vv unused
0351201 3.6376903 3.6376903 0.0
* from to area
0352101 35010001 20120002 5.24e-4
* fwd. loss rev. loss efvcahs
0352102 0.5 0.5 0
* vl vv unused
0352201 -6.1495485 -6.1495485 0.0
* from to area
0353101 35010001 25120002 4.54e-4
* fwd. loss rev. loss efvcahs
0353102 0.5 0.5 0
* vl vv unused
0353201 -6.131784 -6.131784 0.0
* from to area
0354101 35010001 30120002 3.83e-4

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* fwd.loss rev.loss efvcahs
0354102 0.5 0.5 0
*
* vl vv unused
0354201 -6.1061902 -6.1061902 0.0
*
* name type
0400000 "unnamed" branch
*
* njuns
0400001 0
*
* area length vol
0400101 4.418e-3 0.05 0.0
*
* az-angle inc-angle dz
0400102 0.0 -90.0 -0.05
*
* x-rough x-hd flags
0400103 0.0 0.0 0
*
* ebt press water-ie steam-ie void
0400200 000 1.589762e6 2.095778e5 2.594694e6
0.0
*
* name type
0450000 "unnamed" branch
*
* njuns
0450001 5
*
* area length vol
0450101 1.81e-3 0.05 0.0
*
* az-angle inc-angle dz
0450102 0.0 90.0 0.05
*
* x-rough x-hd flags
0450103 0.0 0.0 0
*
* ebt press water-ie steam-ie void
0450200 000 1.562884e6 2.095779e5 2.594318e6
0.0
*
* from to area
0451101 45010001 40010001 1.81e-3
*
* fwd.loss rev.loss efvcahs
0451102 1.5 1.5 0
*
* vl vv unused
0451201 -4.6104264 -4.6104264 0.0
*
* from to area
0452101 45010002 50010001 3.12e-4
*
* fwd.loss rev.loss efvcahs
0452102 0.5 0.5 0
*
* vl vv unused
0452201 11.260211 11.260211 0.0
*
* from to area
0453101 45010002 55010001 2.42e-4
*
* fwd.loss rev.loss efvcahs
0453102 0.5 0.5 0
*
* vl vv unused
0453201 11.155989 11.155989 0.0
*
* from to area
0454101 45010002 60010001 1.71e-4
*
* fwd.loss rev.loss efvcahs
0454102 0.5 0.5 0
*
* vl vv unused
0454201 10.971682 10.971682 0.0
*
* from to area
0455101 45010002 80010001 1.1e-5
*
* fwd.loss rev.loss efvcahs
0455102 0.5 0.5 0
*
* vl vv unused
0455201 23.26129 23.26129 0.0
*
* name type
0500000 "unnamed" pipe
*
* ncells
0500001 12
*
* x-area valid
0500101 3.12e-4 12
*
* x-length valid
0500301 0.05 1
0500302 0.1 11
0500303 0.05 12
*
* volume valid
0500401 0.0 12
*
* azim-angle valid
0500501 0.0 12
*
* vert-angle valid
0500601 90.0 12
*
* x-wall xhd valid
0500801 1.0e-5 4.717e-3 12

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* x-flags valid
0501001 0 12
*
* ebt press water-ie steam-ie void none id
0501201 000 1.470377e6 2.095963e5 2.592927e6 0.0 0.0 1
0501202 000 1.444268e6 2.096746e5 2.592505e6 0.0 0.0 2
0501203 000 1.409458e6 2.097678e5 2.591922e6 0.0 0.0 3
0501204 000 1.374648e6 2.098706e5 2.591312e6 0.0 0.0 4
0501205 000 1.339838e6 2.099767e5 2.590677e6 0.0 0.0 5
0501206 000 1.305028e6 2.100796e5 2.590014e6 0.0 0.0 6
0501207 000 1.270217e6 2.101732e5 2.589321e6 0.0 0.0 7
0501208 000 1.235407e6 2.102518e5 2.588597e6 0.0 0.0 8
0501209 000 1.200597e6 2.10311e5 2.587841e6 0.0 0.0 9
0501210 000 1.165786e6 2.103481e5 2.58705e6 0.0 0.0 10
0501211 000 1.130976e6 2.103731e5 2.586223e6 0.0 0.0 11
0501212 000 1.104867e6 2.10377e5 2.585578e6 0.0 0.0 12
*
* area jun
0500201 3.12e-4 11
*
* jefvcahs jun num
0501101 00000000 11
*
* vl vv unused junid
0501301 11.260675 11.260675 0.0 1
0501302 11.260897 11.260897 0.0 2
0501303 11.261178 11.261178 0.0 3
0501304 11.261471 11.261471 0.0 4
0501305 11.261768 11.261768 0.0 5
0501306 11.262062 11.262062 0.0 6
0501307 11.262344 11.262344 0.0 7
0501308 11.262608 11.262608 0.0 8
0501309 11.262847 11.262847 0.0 9
0501310 11.26306 11.26306 0.0 10
0501311 11.263257 11.263257 0.0 11
*
* hd corr gas slope junid
0501401 4.717e-3 0.0 1.0 1.0 11
*
* name type
0550000 "unnamed" pipe
*
* ncells
0550001 12
*
* x-area valid
0550101 2.42e-4 12
*
* x-length valid
0550301 0.05 1
0550302 0.1 11
0550303 0.05 12
*
* volume valid
0550401 0.0 12
*
* azim-angle valid
0550501 0.0 12
*
* vert-angle valid
0550601 90.0 12
*
* x-wall xhd valid
0550801 1.0e-5 4.64e-3 12
*
* x-flags valid
0551001 0 12
*
* ebt press water-ie steam-ie void none id
0551201 000 1.472093e6 2.09595e5 2.592954e6 0.0 0.0 1
0551202 000 1.445911e6 2.096632e5 2.592532e6 0.0 0.0 2
0551203 000 1.411005e6 2.097448e5 2.591948e6 0.0 0.0 3
0551204 000 1.376099e6 2.09836e5 2.591338e6 0.0 0.0 4
0551205 000 1.341192e6 2.099321e5 2.590702e6 0.0 0.0 5
0551206 000 1.306286e6 2.10028e5 2.590038e6 0.0 0.0 6
0551207 000 1.271379e6 2.101188e5 2.589344e6 0.0 0.0 7
0551208 000 1.236472e6 2.101997e5 2.58862e6 0.0 0.0 8
0551209 000 1.201565e6 2.102668e5 2.587862e6 0.0 0.0 9
0551210 000 1.166658e6 2.103176e5 2.58707e6 0.0 0.0 10
0551211 000 1.131751e6 2.103593e5 2.586242e6 0.0 0.0 11
0551212 000 1.10557e6 2.103754e5 2.585596e6 0.0 0.0 12
*
* area jun
0550201 2.42e-4 11
*
* jefvcahs jun num
0551101 00000000 11
*
* vl vv unused junid
0551301 11.156439 11.156439 0.0 1
0551302 11.156647 11.156647 0.0 2
0551303 11.156912 11.156912 0.0 3
0551304 11.157188 11.157188 0.0 4
0551305 11.157471 11.157471 0.0 5
0551306 11.157754 11.157754 0.0 6
0551307 11.158031 11.158031 0.0 7

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0551308 11.158295 11.158295 0.0 8
0551309 11.158542 11.158542 0.0 9
0551310 11.15877 11.15877 0.0 10
0551311 11.158986 11.158986 0.0 11
* hd corr gas slope junid
0551401 4.64e-3 0.0 1.0 1.0 11
* name type
0600000 "unnamed" pipe
* ncells
0600001 12
* x-area valid
0600101 1.71e-4 12
* x-length valid
0600301 0.05 1
0600302 0.1 11
0600303 0.05 12
* volume valid
0600401 0.0 12
* azim-angle valid
0600501 0.0 12
* vert-angle valid
0600601 90.0 12
* x-wall xhd valid
0600801 1.0e-5 4.506e-3 12
* x-flags valid
0601001 0 12
* ebt press water-ie steam-ie void none id
0601201 000 1.475083e6 2.095953e5 2.593001e6 0.0 0.0 1
0601202 000 1.448776e6 2.096526e5 2.592579e6 0.0 0.0 2
0601203 000 1.413704e6 2.097188e5 2.591994e6 0.0 0.0 3
0601204 000 1.37863e6 2.097916e5 2.591384e6 0.0 0.0 4
0601205 000 1.343557e6 2.098679e5 2.590746e6 0.0 0.0 5
0601206 000 1.308484e6 2.099442e5 2.590081e6 0.0 0.0 6
0601207 000 1.27341e6 2.100174e5 2.589386e6 0.0 0.0 7
0601208 000 1.238336e6 2.100842e5 2.588659e6 0.0 0.0 8
0601209 000 1.203262e6 2.10142e5 2.5879e6 0.0 0.0 9
0601210 000 1.168188e6 2.10189e5 2.587106e6 0.0 0.0 10
0601211 000 1.133113e6 2.102301e5 2.586275e6 0.0 0.0 11
0601212 000 1.106807e6 2.102442e5 2.585627e6 0.0 0.0 12
* area jun
0600201 1.71e-4 11
* jefvcahs jun num
0601101 00000000 11
* vl vv unused junid
0601301 10.972111 10.972111 0.0 1
0601302 10.972301 10.972301 0.0 2
0601303 10.972545 10.972545 0.0 3
0601304 10.972795 10.972795 0.0 4
0601305 10.97305 10.97305 0.0 5
0601306 10.973306 10.973306 0.0 6
0601307 10.973557 10.973557 0.0 7
0601308 10.973801 10.973801 0.0 8
0601309 10.974033 10.974033 0.0 9
0601310 10.974254 10.974254 0.0 10
0601311 10.974466 10.974466 0.0 11
* hd corr gas slope junid
0601401 4.506e-3 0.0 1.0 1.0 11
* name type
0650000 "unnamed" branch
* njuns
0650001 5
* area length vol
0650101 1.81e-3 0.1 0.0
* az-angle inc-angle dz
0650102 0.0 90.0 0.1
* x-rough x-hd flags
0650103 0.0 0.0 0
* ebt press water-ie steam-ie void
0650200 000 1.122699e6 2.103265e5 2.586021e6
0.0
* from to area
0651101 65010002 70010001 1.81e-3
* fwd. loss rev. loss efvcahs
0651102 0.0 0.0 0
* vl vv unused
0651201 4.6117187 4.6117187 0.0
* from to area
0652101 65010001 50120002 3.12e-4

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* fwd. loss rev. loss efvcahs
0652102 0.4 0.4 0
* vl vv unused
0652201 -11.263387 -11.263387 0.0
* from to area
0653101 65010001 55120002 2.42e-4
* fwd. loss rev. loss efvcahs
0653102 0.4 0.4 0
* vl vv unused
0653201 -11.159129 -11.159129 0.0
* from to area
0654101 65010001 60120002 1.71e-4
* fwd. loss rev. loss efvcahs
0654102 0.4 0.4 0
* vl vv unused
0654201 -10.974606 -10.974606 0.0
* from to area
0655101 65010001 80120002 1.1e-5
* fwd. loss rev. loss efvcahs
0655102 0.4 0.4 0
* vl vv unused
0655201 -23.267387 -23.267387 0.0
* name type
0700000 "unnamed" pipe
* ncells
0700001 6
* x-area valid
0700101 1.81e-3 6
* x-length valid
0700301 0.2 1
0700302 0.4 2
0700303 0.5 5
0700304 0.3 6
* volume valid
0700401 0.0 6
* azim-angle valid
0700501 0.0 6
* vert-angle valid
0700601 90.0 6
* x-wall xhd valid
0700801 1.0e-5 0.0 6
* x-flags valid
0701001 0 6
* ebt press water-ie steam-ie void none id
0701201 000 1.120749e6 2.103169e5 2.585973e6 0.0 0.0 1
0701202 000 1.116802e6 2.102979e5 2.585876e6 0.0 0.0 2
0701203 000 1.110882e6 2.102742e5 2.585728e6 0.0 0.0 3
0701204 000 1.104304e6 2.102504e5 2.585564e6 0.0 0.0 4
0701205 000 1.097726e6 2.102265e5 2.585398e6 0.0 0.0 5
0701206 000 1.092463e6 2.102121e5 2.585264e6 0.0 0.0 6
* jefvcahs jun num
0701101 00000000 5
* vl vv unused junid
0701301 4.6117172 4.6117172 0.0 1
0701302 4.6117153 4.6117153 0.0 2
0701303 4.6117148 4.6117148 0.0 3
0701304 4.6117158 4.6117158 0.0 4
0701305 4.6117167 4.6117167 0.0 5
* name type
0740000 "unnamed" sngljun
* from to area
0740101 70060002 75010001 0.0
* fwd. loss rev. loss efvcahs
0740102 0.0 0.0 0
* discharge thermal
0740103 1.0 0.14
* flow vl vv unused
0740201 0 4.6117196 4.6117196 0.0
* name type
0750000 "unnamed" tmdpvol
* area length vol
0750101 20.0 20.0 0.0
* az-angle inc-angle dz
0750102 0.0 90.0 20.0
* x-rough x-hd flags
0750103 0.0 0.0 0
* cword
0750200 3

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*      srch  press  temp
0750201  0.0  1.101e6  300.0
*      name  type
0800000  "unnamed"  pipe
*      ncells
0800001  12
*      x-area  valid
0800101  1.1e-5  1
0800102  3.46e-4  11
0800103  1.1e-5  12
*      x-length  valid
0800301  0.05  1
0800302  0.1  11
0800303  0.05  12
*      volume  valid
0800401  0.0  12
*      azim-angle  valid
0800501  0.0  12
*      vert-angle  valid
0800601  90.0  12
*      x-wall  xhd  valid
0800801  1.0e-5  0.0  12
*      x-flags  valid
0801001  0  12
*      ebt  press  water-ie  steam-ie  void  none  id
0801201 000 1.12475e6 2.096705e5 2.586072e6 0.0 0.0 1
0801202 000 1.34429e6 2.096706e5 2.59076e6 0.0 0.0 2
0801203 000 1.343289e6 2.096722e5 2.590741e6 0.0 0.0 3
0801204 000 1.342287e6 2.096755e5 2.590723e6 0.0 0.0 4
0801205 000 1.341286e6 2.096807e5 2.590704e6 0.0 0.0 5
0801206 000 1.340284e6 2.096875e5 2.590686e6 0.0 0.0 6
0801207 000 1.339282e6 2.09696e5 2.590667e6 0.0 0.0 7
0801208 000 1.338281e6 2.09706e5 2.590648e6 0.0 0.0 8
0801209 000 1.337279e6 2.09717e5 2.590629e6 0.0 0.0 9
0801210 000 1.336277e6 2.097289e5 2.59061e6 0.0 0.0 10
0801211 000 1.335276e6 2.097414e5 2.590592e6 0.0 0.0 11
0801212 000 1.020448e6 2.098705e5 2.583331e6 0.0 0.0 12
*      area  jun
0800201  3.46e-4  11
*      jefvcahs  jun num
0801101  00000000  11
*      vl  vv  unused  junid
0801301  0.73966569  0.73966569  0.0  1
0801302  0.73959684  0.73959684  0.0  2
0801303  0.73959726  0.73959726  0.0  3
0801304  0.73959786  0.73959786  0.0  4
0801305  0.73959857  0.73959857  0.0  5
0801306  0.73959947  0.73959947  0.0  6
0801307  0.73960048  0.73960048  0.0  7
0801308  0.73960161  0.73960161  0.0  8
0801309  0.7396028  0.7396028  0.0  9
0801310  0.73960406  0.73960406  0.0  10
0801311  0.73960543  0.73960543  0.0  11
***** Heat Structures
*****
reflood
10010000  8  7  2  1  0.024  0
*      mesh  format
10010100  0  1
*      intervals  radius
10010101  6  0.026
*      material  interval
10010201  3  6
*      rpkf  interval
10010301  0.0  6
*      temp  interval
10010401  300.0  7
* Left Boundary Condition Data
*      bound  incr  type  code  factor  node
10010501  70060000  0  101  1  0.3  1
10010502  70050000  0  101  1  0.5  2
10010503  70040000  0  101  1  0.5  3
10010504  70030000  0  101  1  0.5  4
10010505  70020000  0  101  1  0.4  5
10010506  70010000  0  101  1  0.2  6
10010507  65010000  0  101  1  0.1  7
10010508  45010000  0  101  1  0.05  8
* Right Boundary Condition Data

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```

*      bound  incr  type  code  factor  node
10010601  10010000  0  101  1  0.3  1
10010602  10020000  0  101  1  0.5  2
10010603  10030000  0  101  1  0.5  3
10010604  10040000  0  101  1  0.5  4
10010605  10050000  0  101  1  0.4  5
10010606  10060000  0  101  1  0.2  6
10010607  15010000  0  101  1  0.1  7
10010608  35010000  0  101  1  0.05  8
*      source  mult  dmhl  dmhr  num
10010701  0  0.0  0.0  0.0  8
* Left Additional Boundary Condition Data
10010800  0
*      hthd  hlf  hlr  gslf  gslr  glcf  glcr  lbf  node
10010801  0.0  10.0  10.0  0.0  0.0  0.0  1.0  8
* Right Additional Boundary Condition Data
10010900  0
*      hthd  hlf  hlr  gslf  gslr  glcf  glcr  lbf  node
10010901  0.0  10.0  10.0  0.0  0.0  0.0  1.0  8
*n: 5
*      nh  np  geom  ssid  leftcoord  reflood
10025000  10  17  2  1  0.033  0
*      mesh  format
10025100  0  1
*      intervals  radius
10025101  4  0.0336
10025102  8  0.0344
10025103  4  0.035
*      material  interval
10025201  2  4
10025202  1  12
10025203  2  16
*      rpkf  interval
10025301  0.0  4
10025302  1.0  12
10025303  0.0  16
*      temp  interval
10025401  300.0  17
* Left Boundary Condition Data
*      bound  incr  type  code  factor  node
10025501  25110000  0  101  1  0.1  1
10025502  25100000  0  101  1  0.1  2
10025503  25090000  0  101  1  0.1  3
10025504  25080000  0  101  1  0.1  4
10025505  25070000  0  101  1  0.1  5
10025506  25060000  0  101  1  0.1  6
10025507  25050000  0  101  1  0.1  7
10025508  25040000  0  101  1  0.1  8
10025509  25030000  0  101  1  0.1  9
10025510  25020000  0  101  1  0.1  10
* Right Boundary Condition Data
*      bound  incr  type  code  factor  node
10025601  20110000  0  101  1  0.1  1
10025602  20100000  0  101  1  0.1  2
10025603  20090000  0  101  1  0.1  3
10025604  20080000  0  101  1  0.1  4
10025605  20070000  0  101  1  0.1  5
10025606  20060000  0  101  1  0.1  6
10025607  20050000  0  101  1  0.1  7
10025608  20040000  0  101  1  0.1  8
10025609  20030000  0  101  1  0.1  9
10025610  20020000  0  101  1  0.1  10
*      source  mult  dmhl  dmhr  num
10025701  1000  0.026176409  0.0  0.0  1
10025702  1000  0.036591412  0.0  0.0  2
10025703  1000  0.044041994  0.0  0.0  3
10025704  1000  0.047924554  0.0  0.0  5
10025705  1000  0.044041994  0.0  0.0  6
10025706  1000  0.036591412  0.0  0.0  7
10025707  1000  0.026176409  0.0  0.0  8
10025708  1000  0.013640753  0.0  0.0  9
10025709  1000  6.890509e-3  0.0  0.0  10
* Left Additional Boundary Condition Data
10025800  0
*      hthd  hlf  hlr  gslf  gslr  glcf  glcr  lbf  node
10025801  9.816e-3  10.0  10.0  0.0  0.0  0.0  1.0  10
* Right Additional Boundary Condition Data
10025900  0

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*      hthd hlf hlr gslf gslr glcf glcr lbf node
10025901 0.010697 10.0 10.0 0.0 0.0 0.0 0.0 1.0 10
*      nh np geom ssif leftcoord refflood
10026000 2 7 2 1 0.033 0
*      mesh format
10026100 0 1
*      intervals radius
10026101 6 0.035
*      material interval
10026201 2 6
*      rpkf interval
10026301 0.0 6
*      temp interval
10026401 300.0 7
* Left Boundary Condition Data
*      bound incr type code factor node
10026501 25010000 0 101 1 0.05 1
10026502 25120000 0 101 1 0.05 2
* Right Boundary Condition Data
*      bound incr type code factor node
10026601 20010000 0 101 1 0.05 1
10026602 20120000 0 101 1 0.05 2
*      source mult dmhl dmhr num
10026701 0 0.0 0.0 0.0 2
* Left Additional Boundary Condition Data
10026800 0
*      hthd hlf hlr gslf gslr glcf glcr lbf node
10026801 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
* Right Additional Boundary Condition Data
10026900 0
*      hthd hlf hlr gslf gslr glcf glcr lbf node
10026901 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
*n: 4
*      nh np geom ssif leftcoord refflood
10030000 10 17 2 1 0.0285 0
*      mesh format
10030100 0 1
*      intervals radius
10030101 4 0.0291
10030102 8 0.0299
10030103 4 0.0305
*      material interval
10030201 2 4
10030202 1 12
10030203 2 16
*      rpkf interval
10030301 0.0 4
10030302 1.0 12
10030303 0.0 16
*      temp interval
10030401 300.0 17
* Left Boundary Condition Data
*      bound incr type code factor node
10030501 30110000 0 101 1 0.1 1
10030502 30100000 0 101 1 0.1 2
10030503 30090000 0 101 1 0.1 3
10030504 30080000 0 101 1 0.1 4
10030505 30070000 0 101 1 0.1 5
10030506 30060000 0 101 1 0.1 6
10030507 30050000 0 101 1 0.1 7
10030508 30040000 0 101 1 0.1 8
10030509 30030000 0 101 1 0.1 9
10030510 30020000 0 101 1 0.1 10
* Right Boundary Condition Data
*      bound incr type code factor node
10030601 25110000 0 101 1 0.1 1
10030602 25100000 0 101 1 0.1 2
10030603 25090000 0 101 1 0.1 3
10030604 25080000 0 101 1 0.1 4
10030605 25070000 0 101 1 0.1 5
10030606 25060000 0 101 1 0.1 6
10030607 25050000 0 101 1 0.1 7
10030608 25040000 0 101 1 0.1 8
10030609 25030000 0 101 1 0.1 9
10030610 25020000 0 101 1 0.1 10
*      source mult dmhl dmhr num
10030701 1000 0.018878743 0.0 0.0 1
10030702 1000 0.02639017 0.0 0.0 2
10030703 1000 0.03176362 0.0 0.0 3
10030704 1000 0.034563769 0.0 0.0 5
10030705 1000 0.03176362 0.0 0.0 6
10030706 1000 0.02639017 0.0 0.0 7
10030707 1000 0.018878743 0.0 0.0 8
10030708 1000 9.837876e-3 0.0 0.0 9
10030709 1000 4.969519e-3 0.0 0.0 10
* Left Additional Boundary Condition Data
10030800 0
*      hthd hlf hlr gslf gslr glcf glcr lbf node
10030801 9.784e-3 10.0 10.0 0.0 0.0 0.0 0.0 1.0 10
* Right Additional Boundary Condition Data
10030900 0
*      hthd hlf hlr gslf gslr glcf glcr lbf node
10030901 0.01083 10.0 10.0 0.0 0.0 0.0 0.0 1.0 10
*      nh np geom ssif leftcoord refflood
10031000 2 7 2 1 0.0285 0
*      mesh format
10031100 0 1
*      intervals radius
10031101 6 0.0305
*      material interval
10031201 2 6
*      rpkf interval
10031301 0.0 6
*      temp interval
10031401 300.0 7
* Left Boundary Condition Data
*      bound incr type code factor node
10031501 30010000 0 101 1 0.05 1
10031502 30120000 0 101 1 0.05 2
* Right Boundary Condition Data
*      bound incr type code factor node
10031601 25010000 0 101 1 0.05 1
10031602 25120000 0 101 1 0.05 2
*      source mult dmhl dmhr num
10031701 0 0.0 0.0 0.0 2
* Left Additional Boundary Condition Data
10031800 0
*      hthd hlf hlr gslf gslr glcf glcr lbf node
10031801 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
* Right Additional Boundary Condition Data
10031900 0
*      hthd hlf hlr gslf gslr glcf glcr lbf node
10031901 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
*n: 3
*      nh np geom ssif leftcoord refflood
10050000 10 17 2 1 0.024 0
*      mesh format
10050100 0 1
*      intervals radius
10050101 4 0.0246
10050102 8 0.0254
10050103 4 0.026
*      material interval
10050201 2 4
10050202 1 12
10050203 2 16
*      rpkf interval
10050301 0.0 4
10050302 1.0 12
10050303 0.0 16
*      temp interval
10050401 300.0 17
* Left Boundary Condition Data
*      bound incr type code factor node
10050501 50020000 0 101 1 0.1 1
10050502 50030000 0 101 1 0.1 2
10050503 50040000 0 101 1 0.1 3
10050504 50050000 0 101 1 0.1 4
10050505 50060000 0 101 1 0.1 5
10050506 50070000 0 101 1 0.1 6
10050507 50080000 0 101 1 0.1 7
10050508 50090000 0 101 1 0.1 8
10050509 50100000 0 101 1 0.1 9
10050510 50110000 0 101 1 0.1 10
* Right Boundary Condition Data
*      bound incr type code factor node

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10050601 30110000 0 101 1 0.1 1
10050602 30100000 0 101 1 0.1 2
10050603 30090000 0 101 1 0.1 3
10050604 30080000 0 101 1 0.1 4
10050605 30070000 0 101 1 0.1 5
10050606 30060000 0 101 1 0.1 6
10050607 30050000 0 101 1 0.1 7
10050608 30040000 0 101 1 0.1 8
10050609 30030000 0 101 1 0.1 9
10050610 30020000 0 101 1 0.1 10
* source mult dmhl dmhr num
10050701 1000 0.014357363 0.0 0.0 1
10050702 1000 0.020069835 0.0 0.0 2
10050703 1000 0.024156366 0.0 0.0 3
10050704 1000 0.026285892 0.0 0.0 5
10050705 1000 0.024156366 0.0 0.0 6
10050706 1000 0.020069835 0.0 0.0 7
10050707 1000 0.014357363 0.0 0.0 8
10050708 1000 7.481746e-3 0.0 0.0 9
10050709 1000 3.77934e-3 0.0 0.0 10
* Left Additional Boundary Condition Data
10050800 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10050801 9.742e-3 10.0 10.0 0.0 0.0 0.0 1.0 10
* Right Additional Boundary Condition Data
10050900 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10050901 0.011028 10.0 10.0 0.0 0.0 0.0 0.0 1.0 10
* nh np geom ssif leftcoord reflowd
10051000 2 7 2 1 0.024 0
* mesh format
10051100 0 1
* intervals radius
10051101 6 0.026
* material interval
10051201 2 6
* rpkf interval
10051301 0.0 6
* temp interval
10051401 300.0 7
* Left Boundary Condition Data
* bound incr type code factor node
10051501 50010000 0 101 1 0.05 1
10051502 50120000 0 101 1 0.05 2
* Right Boundary Condition Data
* bound incr type code factor node
10051601 30120000 0 101 1 0.05 1
10051602 30010000 0 101 1 0.05 2
* source mult dmhl dmhr num
10051701 0 0.0 0.0 0.0 2
* Left Additional Boundary Condition Data
10051800 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10051801 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
* Right Additional Boundary Condition Data
10051900 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10051901 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
*n: 2
* nh np geom ssif leftcoord reflowd
10055000 10 17 2 1 0.0195 0
* mesh format
10055100 0 1
* intervals radius
10055101 4 0.0201
10055102 8 0.0209
10055103 4 0.0215
* material interval
10055201 2 4
10055202 1 12
10055203 2 16
* rpkf interval
10055301 0.0 4
10055302 1.0 12
10055303 0.0 16
* temp interval
10055401 300.0 17
* Left Boundary Condition Data
* bound incr type code factor node
10055501 55020000 0 101 1 0.1 1
10055502 55030000 0 101 1 0.1 2
10055503 55040000 0 101 1 0.1 3
10055504 55050000 0 101 1 0.1 4
10055505 55060000 0 101 1 0.1 5
10055506 55070000 0 101 1 0.1 6
10055507 55080000 0 101 1 0.1 7
10055508 55090000 0 101 1 0.1 8
10055509 55100000 0 101 1 0.1 9
10055510 55110000 0 101 1 0.1 10
* Right Boundary Condition Data
* bound incr type code factor node
10055601 50020000 0 101 1 0.1 1
10055602 50030000 0 101 1 0.1 2
10055603 50040000 0 101 1 0.1 3
10055604 50050000 0 101 1 0.1 4
10055605 50060000 0 101 1 0.1 5
10055606 50070000 0 101 1 0.1 6
10055607 50080000 0 101 1 0.1 7
10055608 50090000 0 101 1 0.1 8
10055609 50100000 0 101 1 0.1 9
10055610 50110000 0 101 1 0.1 10
* source mult dmhl dmhr num
10055701 1000 0.011184465 0.0 0.0 1
10055702 1000 0.015634512 0.0 0.0 2
10055703 1000 0.018817943 0.0 0.0 3
10055704 1000 0.020476855 0.0 0.0 5
10055705 1000 0.018817943 0.0 0.0 6
10055706 1000 0.015634512 0.0 0.0 7
10055707 1000 0.011184465 0.0 0.0 8
10055708 1000 5.828322e-3 0.0 0.0 9
10055709 1000 2.944127e-3 0.0 0.0 10
* Left Additional Boundary Condition Data
10055800 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10055801 0.09676 10.0 10.0 0.0 0.0 0.0 0.0 1.0 10
* Right Additional Boundary Condition Data
10055900 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10055901 0.011343 10.0 10.0 0.0 0.0 0.0 0.0 1.0 10
* nh np geom ssif leftcoord reflowd
10056000 2 7 2 1 0.0195 0
* mesh format
10056100 0 1
* intervals radius
10056101 6 0.0215
* material interval
10056201 2 6
* rpkf interval
10056301 0.0 6
* temp interval
10056401 300.0 7
* Left Boundary Condition Data
* bound incr type code factor node
10056501 55120000 0 101 1 0.05 1
10056502 55010000 0 101 1 0.05 2
* Right Boundary Condition Data
* bound incr type code factor node
10056601 50120000 0 101 1 0.05 1
10056602 50010000 0 101 1 0.05 2
* source mult dmhl dmhr num
10056701 0 0.0 0.0 0.0 2
* Left Additional Boundary Condition Data
10056800 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10056801 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
* Right Additional Boundary Condition Data
10056900 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10056901 0.0 10.0 10.0 0.0 0.0 0.0 0.0 1.0 2
*n: 1
* nh np geom ssif leftcoord reflowd
10060000 10 17 2 1 0.015 0
* mesh format
10060100 0 1
* intervals radius
10060101 4 0.0156

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```

10060102      8  0.0164
10060103      4  0.017
* material interval
10060201      2  4
10060202      1  12
10060203      2  16
* rpkf interval
10060301      0.0  4
10060302      1.0  12
10060303      0.0  16
* temp interval
10060401      300.0  17
* Left Boundary Condition Data
* bound incr type code factor node
10060501 60020000 0 101 1 0.1 1
10060502 60030000 0 101 1 0.1 2
10060503 60040000 0 101 1 0.1 3
10060504 60050000 0 101 1 0.1 4
10060505 60060000 0 101 1 0.1 5
10060506 60070000 0 101 1 0.1 6
10060507 60080000 0 101 1 0.1 7
10060508 60090000 0 101 1 0.1 8
10060509 60100000 0 101 1 0.1 9
10060510 60110000 0 101 1 0.1 10
* Right Boundary Condition Data
* bound incr type code factor node
10060601 55020000 0 101 1 0.1 1
10060602 55030000 0 101 1 0.1 2
10060603 55040000 0 101 1 0.1 3
10060604 55050000 0 101 1 0.1 4
10060605 55060000 0 101 1 0.1 5
10060606 55070000 0 101 1 0.1 6
10060607 55080000 0 101 1 0.1 7
10060608 55090000 0 101 1 0.1 8
10060609 55100000 0 101 1 0.1 9
10060610 55110000 0 101 1 0.1 10
* source mult dmhl dmhr num
10060701 1000 8.72547e-3 0.0 0.0 1
10060702 1000 0.012197137 0.0 0.0 2
10060703 1000 0.014680665 0.0 0.0 3
10060704 1000 0.015974851 0.0 0.0 5
10060705 1000 0.014680665 0.0 0.0 6
10060706 1000 0.012197137 0.0 0.0 7
10060707 1000 8.72547e-3 0.0 0.0 8
10060708 1000 4.546918e-3 0.0 0.0 9
10060709 1000 2.296836e-3 0.0 0.0 10
* Left Additional Boundary Condition Data
10060800 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10060801 9.563e-3 10.0 10.0 0.0 0.0 0.0 1.0 10
* Right Additional Boundary Condition Data
10060900 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10060901 0.011926 10.0 10.0 0.0 0.0 0.0 1.0 10
* nh np geom ssif leftcoord reflowd
10061000 2 7 2 1 0.015 0
* mesh format
10061100 0 1
* intervals radius
10061101 6 0.017
* material interval
10061201 2 6
* rpkf interval
10061301 0.0 6
* temp interval
10061401 300.0 7
* Left Boundary Condition Data
* bound incr type code factor node
10061501 60120000 0 101 1 0.05 1
10061502 60010000 0 101 1 0.05 2
* Right Boundary Condition Data
* bound incr type code factor node
10061601 55120000 0 101 1 0.05 1
10061602 55010000 0 101 1 0.05 2
* source mult dmhl dmhr num
10061701 0 0.0 0.0 0.0 2
* Left Additional Boundary Condition Data
10061800 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10061801 0.0 10.0 10.0 0.0 0.0 0.0 1.0 2
* Right Additional Boundary Condition Data
10061900 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10061901 0.0 10.0 10.0 0.0 0.0 0.0 1.0 2
*n: 0
* nh np geom ssif leftcoord reflowd
10080000 12 17 2 1 0.0105 0
* mesh format
10080100 0 1
* intervals radius
10080101 16 0.0125
* material interval
10080201 3 16
* rpkf interval
10080301 0.0 16
* temp interval
10080401 300.0 17
* Left Boundary Condition Data
* bound incr type code factor node
10080501 80020000 0 101 1 0.1 1
10080502 80030000 0 101 1 0.1 2
10080503 80040000 0 101 1 0.1 3
10080504 80050000 0 101 1 0.1 4
10080505 80060000 0 101 1 0.1 5
10080506 80070000 0 101 1 0.1 6
10080507 80080000 0 101 1 0.1 7
10080508 80090000 0 101 1 0.1 8
10080509 80100000 0 101 1 0.1 9
10080510 80110000 0 101 1 0.1 10
10080511 80010000 0 101 1 0.05 11
10080512 80120000 0 101 1 0.05 12
* Right Boundary Condition Data
* bound incr type code factor node
10080601 60020000 0 101 1 0.1 1
10080602 60030000 0 101 1 0.1 2
10080603 60040000 0 101 1 0.1 3
10080604 60050000 0 101 1 0.1 4
10080605 60060000 0 101 1 0.1 5
10080606 60070000 0 101 1 0.1 6
10080607 60080000 0 101 1 0.1 7
10080608 60090000 0 101 1 0.1 8
10080609 60100000 0 101 1 0.1 9
10080610 60110000 0 101 1 0.1 10
10080611 60010000 0 101 1 0.05 11
10080612 60120000 0 101 1 0.05 12
* source mult dmhl dmhr num
10080701 0 0.0 0.0 0.0 12
* Left Additional Boundary Condition Data
10080800 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10080801 9.563e-3 10.0 10.0 0.0 0.0 0.0 1.0 10
10080802 0.0 10.0 10.0 0.0 0.0 0.0 1.0 12
* Right Additional Boundary Condition Data
10080900 0
* hthd hlf hlr gslf gslr glcf glcr lbf node
10080901 0.011926 10.0 10.0 0.0 0.0 0.0 1.0 10
10080902 0.0 10.0 10.0 0.0 0.0 0.0 1.0 12
***** Point Kinetics
***** type feedback
30000000 point separabl
* decay power react dnf
30000001 gamma-ac 1.98e6 0.0 45.03311
* control
30000011 2 * General Table 2 (PK + PAR)
30000012 3 * General Table 3 (PB)
30000013 4 * General Table 4 (Reactivity_Slow)
30000014 5 * General Table 5 (Reactivity_Fast)

```

BIBLIOGRAPHIC DATA SHEET

(See instructions on the reverse)

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10. SUPPLEMENTARY NOTES

A. Calvo, NRC Project Manager

11. ABSTRACT (200 words or less)

The new fuel type in the Research Reactor 'Maria' is undergoing a test procedure. Thermal-hydraulic calculations using RELAP have been applied in order to cross-check the results obtained using a specialized thermal-hydraulic 'SN' code. Nodalization of the fuel element has been developed and calculations have been performed. LOFA and RIA cases have been analysed and compared showing good agreement between the two codes.

12. KEY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)

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GTRI (Global Threat Reduction Initiative)
National Centre for Nuclear Research
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Loss Of Coolant Accident (LOCA)
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March 2013