



# International Agreement Report

## Assessment of RELAP5/MOD3.3Beta Code for the LOFT Experiment L9-1/L3-3

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## ABSTRACT

The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3. The Experiment L9-1/L3-3 was a simulation of the total loss-of-feedwater accident and its recovery modes. Experiment L9-1 simulated a loss-of-feedwater accident with delayed reactor scram and no auxiliary feedwater injection. The loss-of-feedwater accident led to a loss-of-coolant accident through the PORV cycling operation.

Generally, the RELAP5/MOD3.3Beta calculation results were in good agreement with the L9-1 experimental data. The discrepancies between the calculation and the experiment were also identified in the temperature behaviors of the SG secondary side after dryout of the SG. However, these discrepancies were not considered to be significant, since the SG was in a de-coupled state from the PCS after the dryout of the SG secondary side.

Experiment L3-3 simulated two recovery modes from the loss-of-feedwater accident L9-1 without the aid of the emergency core coolant system. The first recovery mode consisted of turning off the primary coolant pumps and latching open the PORV to depressurize the primary system. The second mode consisted of refilling the SG to restore the secondary heat sink and removing decay heat through the feed-and-bleed operation using the secondary side of the SG.

The general trends observed in Experiment L3-3 were similar to those of the RELAP5/MOD3.3Beta code calculations. In addition, some differences between the code calculations and the L3-3 experimental data were observed. The code predicted excessive swelling of the PCS fluid during the first recovery mode, and predicted excessive cooling during the second recovery mode. The differences during the first recovery mode were due to the code's under-estimation of total discharged energy through the PORV. For the discrepancies during the second recovery mode, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, it is concluded that further investigation into the deviation sources are needed to enhance the code's predictability, since the specific reasons for the deviation were not clearly identified in this assessment.

Sensitivity studies show that several parameters have significant effect on the predicted thermal-hydraulic behaviors. These parameters include the pressurizer spray system loss coefficient, nodalization of the SG secondary side, SG U-tube heat transfer area, heat transfer coefficient from the LOFT main components to the environment, and the PORV discharge coefficient. The first three parameters are significant during the short-term transient phase, while the last two are significant during the long-term transient phase. Therefore, the five parameters listed above should be carefully modeled to obtain appropriate calculation results for transient types such as the total-loss-of feedwater accident and its recovery modes.



## FOREWORD

This report is prepared to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3. The RELAP5 computer code has been developed as a highly generic best-estimate code to be used for simulation of a wide variety of hydraulic and thermal transients in LWR systems. As one of the new code version, RELAP5/MOD3.3Beta was released in June 2001 with several new models and improvements to existing models.

The Loss-of-Fluid Test (LOFT) integral experimental facility was a scaled model of a commercial pressurized water reactor (PWR) to model the nuclear, and thermal-hydraulic phenomena expected to occur primarily during a loss-of-coolant accident (LOCA). The Experiment L9-1/L3-3 was performed in 1981 as a part of the LOFT Experimental Program to simulate total loss-of-feedwater accident and its recovery modes.

The code-predicted results were compared with experimental data to assess the code predictability. From the comparisons, it is concluded that the RELAP5/MOD3.3Beta computer code has sufficient capability in predicting the thermal hydraulic phenomena occurred in the LOFT Experiment L9-1/L3-3 because the code-predicted results were generally in agreement with the measured data. However, some discrepancies between the calculation and the experiment were also observed. In addition, major parameters having significant effect on the predicted thermal-hydraulic behaviors were identified through sensitivity studies.

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# CONTENTS

<b>Page</b>	
Abstract.....	iii
Foreword .....	v
Executive Summary .....	xi
1. Introduction .....	1-1
2. Facility and Test Description .....	2-1
2.1 Facility Description .....	2-1
2.2 Test Description.....	2-1
3. Code and Modeling.....	3-1
3.1 Code Description .....	3-1
3.2 Input Modeling .....	3-1
4. Results and Discussion.....	4-1
4.1 Base Calculation.....	4-1
4.2 Sensitivity Studies .....	4-11
4.3 Run Statistics .....	4-15
5. Conclusions .....	5-1
6. References .....	6-1

## Appendices

A	Steady State Input Deck for Base Case.....	A-1
B	Transient Input Deck for Base Case.....	B-1

## List of Figures

<b>Figure</b>	<b>Page</b>
1. Configuration of LOFT System for Experiment L9-1/L3-3 .....	2-1
2. RELAP5 Nodalization for LOFT L9-1/L3-3 .....	3-4
3. Comparison of Pressure for Short-term Response .....	4-2
4. Comparison of Temperature for Short-term Response .....	4-3
5. Comparison of Reactor Power for Short-term Response .....	4-3
6. Comparison of Mass Flow Rate through MSCV for Short-term Response .....	4-4
7. Comparison of SG Liquid Level for Short-term Response .....	4-4
8. Comparison of Pressure for Long-term Response .....	4-6
9. Comparison of Temperature for Long-term Response .....	4-7
10. Comparison of Pressurizer Collapsed Liquid Level .....	4-8
11. Mass Flow Rate through PORV for Long-term Response .....	4-9
12. Fluid Conditions of Hot Leg for Long-term Response .....	4-10
13. System Mass of PCS for Long-term Response .....	4-10
14. Sensitivity Studies for Short-term Parameters .....	4-12
15. Comparison of Heat Transfer Rate through SG U-tube .....	4-13
16. Sensitivity Studies for Long-term Parameters .....	4-14
17. Sensitivity Study for Mass Flow Rate through PORV .....	4-15
18. Required CPU Time of Base Calculation .....	4-16
19. Time Step Size of Base Calculation .....	4-16

## List of Tables

<u>Table</u>	<u>Page</u>
1. Initial Conditions for Experiment L9-1/L3-3 .....	3-5
2. Major Sequence of Events for Experiment L9-1/L3-3.....	4-5
3. Matrix for Sensitivity Studies.....	4-11



## EXECUTIVE SUMMARY

The RELAP5 computer code has been developed as a highly generic best-estimate code to be used for simulation of a wide variety of hydraulic and thermal transients in LWR systems. As one of the new code version of the RELAP5, RELAP5/MOD3.3Beta was released with several new models and improvements to existing models. The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3.

The Experiment L9-1/L3-3 was a simulation of the total loss-of-feedwater accident and its recovery modes. In Experiment L9-1, the pressure increase in the primary system due to the power-cooling mismatch was controlled by the cycling operation of the pressurizer spray valve and by the coolant discharge through the power-operated relief valve (PORV). In the subsequent Experiment L3-3, two independent recovery procedures for the removal of the core decay heat during the total loss-of-feedwater accident were investigated. The first recovery procedure was the PORV latching open to depressurize the primary coolant system. The second one was accomplished by refilling the steam generator to restore the secondary side heat sink and removing the decay heat through a feed-and-bleed operation using the steam generator secondary side.

For the assessment calculation, the base input decks were prepared by incorporating the major parameters which were identified through sensitivity studies to have significant effect on the code calculation results. The code-predicted results were compared with the experimental data to assess the code predictability. Major conclusions through this assessment are summarized as follows:

- From the comparisons presented with Figures and Tables, it was shown that the code-predicted results were generally in agreement with the measured data. Therefore, it is concluded that the RELAP5/MOD3.3Beta computer code has sufficient capability in predicting the thermal hydraulic phenomena occurred in the LOFT Experiment L9-1/L3-3.
- However, the discrepancies between the calculation and the experiment were also identified. In Experiment L9-1, the code over-estimated temperature behaviors of the SG secondary side after dryout of the SG. However, these discrepancies were not considered to be significant, since the SG was in a de-coupled state from the PCS after the dryout of the SG secondary side. In Experiment L3-3, the code predicted excessive swelling of the PCS fluid during the first recovery mode, and predicted excessive cooling during the second recovery mode. The differences during the first recovery mode were due to the code's under-estimation of total discharged energy through the

PORV. For the discrepancies during the second recovery mode, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, it is concluded that further investigation into the deviation sources are needed to enhance the code's predictability, since the specific reasons for the deviation were not clearly identified in this assessment.

- Through sensitivity studies, the major parameters were identified to have significant effect on the predicted thermal-hydraulic behaviors. These parameters include the pressurizer spray system loss coefficient, nodalization of the SG secondary side, SG U-tube heat transfer area, heat transfer coefficient from the LOFT main components to the environment, and the PORV discharge coefficient. The first three parameters are significant during the short-term transient phase, while the last two are significant during the long-term transient phase. Therefore, the five parameters listed above should be carefully modeled to obtain appropriate calculation results for transient types such as the total-loss-of feedwater accident and its recovery modes.

## 1. INTRODUCTION

The RELAP5 computer code has been developed as a highly generic best-estimate code to be used for simulation of a wide variety of hydraulic and thermal transients in LWR systems. As one of the new code version of the RELAP5, RELAP5/MOD3.3Beta was released in June 2001 with several new models and improvements to existing models [1]. The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3.

The Loss-of-Fluid Test (LOFT) integral experimental facility was a scaled model of a commercial pressurized water reactor (PWR). The purpose of this facility was to model the nuclear, and thermal-hydraulic phenomena expected to occur primarily during a loss-of-coolant accident (LOCA). In general, coolant volumes and flow areas in the LOFT were scaled using the ratio of the core power of 50 MWth in the LOFT to 3,000 MWth in a commercial PWR.

The Experiment L9-1/L3-3 was performed in 1981 as a part of the LOFT Experimental Program. It was a simulation of the total loss-of-feedwater accident and its recovery modes. The total loss-of-feedwater (TLOFW) accident is a beyond-design-basis-accident initiated by a loss-of-feedwater due to the failure of the main feedwater pump and subsequent no auxiliary feedwater injection. During the total loss-of-feedwater accident, heat removal capability in the secondary side of the steam generator (SG) is completely degraded and pressure and temperature of the primary coolant system (PCS) are increased to the reactor scram set point. Following the reactor scram, the core decay heat should be removed by proper controlling methods to prevent severe core damage. The role of core decay heat removal during the total loss-of-feedwater accident was considered important since it was identified as one of the major contributors to the severe core damage frequency in previous studies such as WASH-1400 [2].

The LOFT Experiment L9-1/L3-3 provided experimental data for several methods of removing the decay heat during the total loss-of-feedwater accident and its recovery phases. In Experiment L9-1, the pressure increase in the primary system due to the power-cooling mismatch was controlled by the cycling operation of the pressurizer spray valve and by the coolant discharge through the power-operated relief valve (PORV). In the subsequent Experiment L3-3, two independent recovery procedures for the removal of the core decay heat during the total loss-of-feedwater accident were investigated. The first recovery procedure was the PORV latching open to depressurize the primary coolant system. The second one was accomplished by refilling the steam generator to restore the secondary side heat sink and removing the decay heat through a feed-and-bleed operation using the steam generator secondary side. During the second procedure, the primary system pressure decreased rapidly after the reestablishment of the steam generator heat removal capability, and the heat generated in the reactor core was transferred to the steam generator by two-phase natural circulation [3]. In short, the LOFT L9-1/L3-3 was an experiment to evaluate the effectiveness of the PORV and the feed-and-bleed operation using the secondary side for removal of decay heat. This experiment has also been used as a means to evaluate the ability of a thermal-hydraulic computer code in predicting major phenomena.

For the assessment calculation, the base input decks were prepared based on available RELAP5 assessment [4] for this experiment. The major parameters, which were identified through sensitivity studies to have the most significant effect on the predicted thermal hydraulic behaviors, were incorporated into the base calculation to improve the code predictability. The

code calculation results were then compared with the measured data to assess the code capability of predicting major phenomena.



## 2. FACILITY AND TEST DESCRIPTION

### 2.1 Facility Description

The LOFT integral experimental facility was a scale model of a commercial PWR. The purpose of this facility is to model the nuclear, and thermal-hydraulic phenomena expected to occur primarily during a LOCA. In general, coolant volumes and flow areas in the LOFT were scaled with a ratio of the 50 MWth LOFT core to a commercial 3,000 MWth PWR core. Also, components used in the LOFT are similar to those of a commercial PWR [3]. The experimental facility included five major subsystems which had been instrumented such that system variables could be measured and recorded throughout the experiment. The subsystems include (a) the reactor vessel, (b) the intact loop, (c) the broken loop, (d) the blowdown suppression system, and (e) the emergency core cooling system (ECCS) [5]. The major components of the LOFT facility are shown in Figure 1, and a detailed system description is presented in Reference [6].

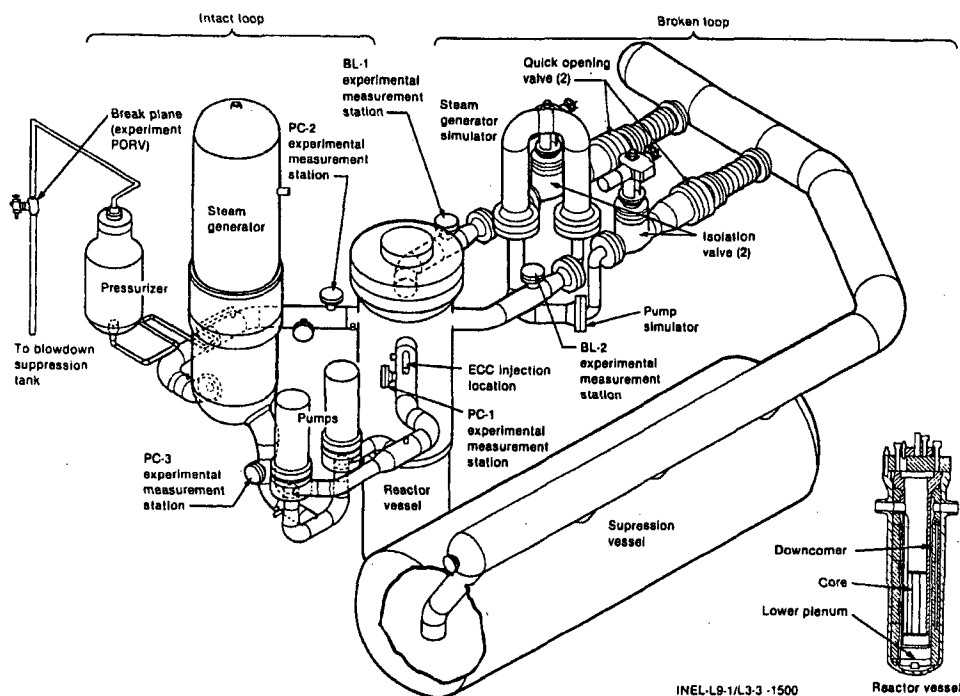


Figure 1. Configuration of LOFT System for Experiment L9-1/L3-3

### 2.2 Test Description

Since 1976, 43 non-nuclear and nuclear experiments have been performed in the LOFT facility

[3]. The Experiment L9-1/L3-3 [3,5,7] conducted on April 15, 1981, consisted of two sequential tests. Experiment L9-1 was performed as part of the LOFT Experiment Series L9 (anticipated transient with multiple failure), and Experiment L3-3 was performed as part of the LOFT Experiment Series L3 (small break LOCA).

Experiment L9-1 was the first anticipated transient with multiple failures performed in the LOFT, and simulated a loss-of-feedwater accident with delayed reactor scram and no auxiliary feedwater injection. The loss-of-feedwater accident led to a loss-of-coolant accident through the PORV. In Experiment L9-1, the transient was initiated by loss-of-feedwater due to the failure of the main feedwater pump. The reactor scrammed on the indication of high pressure (15.745 MPa) in the intact loop hot leg approximately 65 seconds after the main feedwater pump was tripped. The auxiliary feedwater injection into the steam generator was prevented, as was scram on the indication of low liquid level in the steam generator. The main steam control valve (MSCV) of the steam generator started to close automatically on the reactor scram and finished closing 12.2 seconds later (at 77.2 sec). The pressurizer spray valve cycled automatically at its close (15.05 MPa) and open (15.338 MPa) set points from 30 seconds until it was closed by the operators at the 1,246.0 seconds to allow the PCS pressure to increase to the PORV set point. The PORV started cycling operation at 1,467.9 seconds to control primary system pressure, until it was manually latched open at 3,270 seconds. The open and close set points of the PORV were 16.20 MPa and 16.06 MPa, respectively.

Experiment L3-3 simulated two recovery modes from the loss-of-feedwater accident L9-1 without the aid of emergency core coolant (ECC). The first recovery mode consisted of turning off the primary coolant pumps and latching open the PORV to depressurize the primary system. The second mode consisted of refilling the steam generator to restore the secondary heat sink and removing decay heat through the feed-and-bleed operation using the secondary side of the steam generator. Experiment L3-3 began when the PORV was secured in the open position. The primary coolant pumps were tripped 15 seconds later, with pump coastdown lasting about 20 seconds. Saturation occurred in the upper plenum about 60 seconds after the beginning of Experiment L3-3 at the 3,329.4 seconds. The primary pressure decreased to the saturation pressure of 12.3 MPa. This pressure was below the high pressure safety injection system (HPSI) set point of 13.2 MPa, which would have initiated ECCS injection had it not been purposely locked out. After closing the PORV at 4,849.7 seconds, steam generator refill began at 5,114.6 seconds. Natural circulation was established during steam generator refill which was completed at 5,746.4 seconds. Alternating secondary coolant system feed-and-bleed operations began at the 6,712.2 seconds. The experiment was complete at 9,517.4 seconds. The initial plant operating conditions and the major sequence of events for Experiment L9-1/L3-3 are presented in Table 1 and 2, respectively.

The objectives of the L9-1/L3-3 Experiment were specified as follows [5]:

#### 2.2.1.1 Experiment L9-1 Objectives

- To evaluate uncertainties in predicted primary and secondary thermal hydraulic response associated with steam generator dryout during delayed scram,
- To evaluate the adequacy of PORV to provide overpressure protection in a loss-of-feedwater accident.

### 2.2.1.2 *Experiment L3-3 objectives*

- To investigate uncertainties in system response during a PORV imposed small break with loss of secondary heat sink,
- To assess uncertainties in small break performance predictions identified in NUREG-0623 [8],
- To assess the effectiveness of steam generator refill on loss-of-feedwater accidents following reestablishment of auxiliary feedwater availability,
- To assess the relative magnitude of the change in reactor vessel mixture level as a result of primary coolant system shrink during steam generator refill,
- To contribute to the NRC relief and safety valve testing program by providing experimental data on PORV performance characteristics over a range of PORV inlet fluid conditions.



## 3. CODE AND MODELING

### 3.1 Code Description

The code version of RELAP5/MOD3.3Beta, into which several new models and improvements were incorporated, was used for this assessment calculation. Some models recommended in the previous RELAP5 versions such as a new steam table and the Henry-Fauske choked flow model were used as default models in this version. In addition, improved or modified models in the RELAP5/MOD3.3Beta include non-condensable gas treatment, wall friction term modification, time-dependent volume correction, CANDU model updates, etc. The descriptions of the RELAP5/MOD3.3Beta code are presented in detail in the code manuals [1].

### 3.2 Base Input Modeling

For the purpose of the RELAP5/MOD3.3Beta assessment, input decks for the base calculation were prepared based on the reference calculation [4] which was the recent RELAP5 assessment for the LOFT Experiment L9-1/L3-3. The modifications were made to the reference input decks to incorporate the major parameters which were identified through sensitivity studies to have significant effect on the code calculation results. These parameters include loss coefficient of the pressurizer spray system, nodalization of the secondary side of the steam generator, heat transfer area of the steam generator U-tube, heat transfer coefficient from the LOFT main components to the environment, and discharge coefficient of the PORV. The results of the sensitivity studies for the parameters listed above are presented in Section 4.2.

The modifications made to the reference input decks for base input modeling are summarized as follows:

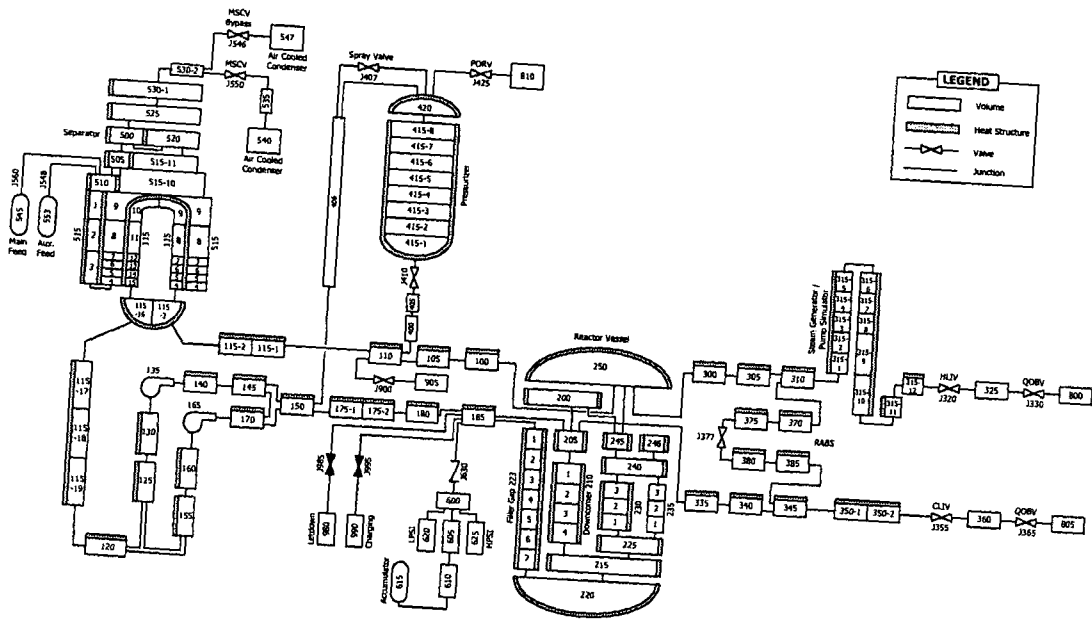
- The mass flow rate into the pressurizer through the pressurizer spray valve was increased by reducing the loss coefficient of the pressurizer spray system
- The bottom node of the steam generator secondary side and associated nodes of the U-tube of the reference calculation were subdivided into four, which implies that the number of nodes of the SG secondary side associated with the U-tube changed into six.
- The heat transfer area of all the nodes of the steam generator U-tube increased by 20% to improve the code-predicted heat transfer phenomena through the SG U-tube.
- The heat transfer coefficient to the environment from the LOFT main components (the reactor vessel, the steam generator, the pressurizer, and primary coolant system) was increased by 40% to have the PCS temperature match with the experimental data during the long-term phase of the transient.

- The discharge coefficient and the thermal non-equilibrium constant of the PORV were set to 0.8 and 0.03 respectively to make the code-calculated mass flow rate through the PORV be in agreement with test data.
- The counter current flow limitation (CCFL) model was applied to the junctions (components 115-3, 400-1, 410-0) for which the flooding phenomena was presumed to occur.
- The additional junction connected to the accumulator was removed, because it was not allowed in the code version of RELAP5/MOD3.3Beta. Since the emergency core cooling system (ECCS) was not injected during Experiment L9-1/L3-3, the junction removal from the accumulator does not affect the calculation results.
- The initial conditions in the reference input decks for some volumes were slightly modified to make the base input decks compatible with the RELAP5/MOD3.3Beta code.

As shown in Figure 2, the LOFT facility was composed of 134 volumes, 143 junctions, and 142 heat structures in the RELAP5 modeling for the base calculation. The intact loop was modeled with 31 hydrodynamic volumes. Environmental heat losses from all the piping metal structures exposed to atmosphere were simulated using the heat structure components. The broken loop was composed of a hot leg, a cold leg, a SG-pump simulator, a reflood assist bypass system (RABS), and quick opening blowdown valves (QOBVs). The volume and junction modeling options were set to the default options. The active core, the downcomer and the filler gap were composed of three volumes, six, and seven vertically stacked volumes, respectively. The rod bundle interphase friction model option was applied to the active core volumes. The fuel rods were modeled using 3 heat structures representing the central fuel assembly and 2 heat structures representing the peripheral fuel assemblies of the LOFT core. The pressurizer system was modeled with a surge line, a pressurizer vessel, a spray line from the cold leg, a spray valve and a PORV. Two volumes for the surge line, nine volumes for the pressurizer vessel and one volume for the spray line were used. The spray valve and the PORV were simulated with two trip valves. The associated trip logic was prepared according to the experimental specification. The SG was modeled using 12 volumes in the primary coolant system and 8 volumes in the SG riser. Heat was exchanged between the primary and secondary sides of the SG through the U-tube, which was modeled using 12 heat structures. The rod bundle interfacial friction option was used for the volumes in contact with the U-tubes heat structures. The emergency core cooling system in the LOFT was also modeled. However, it is not used in the transient calculation. The containment was modeled using a time-dependent volume with constant pressure.

A steady state run was performed to obtain initial conditions of the whole system prior to running the transient case. The initial conditions obtained from the steady state run are presented in Table 1 and compared to the measured data. The RELAP5 results for the steady state run agree well with the experimental initial conditions except for the hot leg temperature of the broken loop. The hot leg temperature of the broken loop deviated from the range of the experimental uncertainty. However, considering that the broken loop does not play an important role from the perspective of the heat removal and the temperature deviation was not significant, it was concluded that the out-of-range value for the broken hot leg temperature would not adversely affect the overall transient calculation.

The boundary conditions and the control trips used in the base calculation were identical to those used in the reference calculation. The information for the boundary conditions and the control trips can be found in the attached input decks. The steady state and the transient input decks for the base calculation are presented in Appendix A and B, respectively.



INTACT LOOP

BROKEN LOOP

Figure 2. RELAP5 Nodalization for LOFT L9-1/L3-3



Table 1. Initial Condition for Experiment L9-1/L3-3

Parameter	Measured	Calculated
<b>Primary Coolant System</b>		
Mass flow rate (kg/s)	479.1±2.6	479.4
Hot leg pressure (MPa)	14.9±0.10	14.91
Cold leg temperature (K)	558.9±1.3	557.7
Hot leg temperature (K)	578.2±1.8	577.0
<b>Reactor</b>		
Power level (MW)	49.6±0.9	49.6
<b>Steam Generator Secondary Side</b>		
Water level (m)	0.14±0.08	0.14
Water temperature (K)	545.0±0.8	546.1
Pressure (MPa)	5.67±0.08	5.70
Mass flow rate (kg/s)	27.0±1.0	26.1
<b>Broken Loop</b>		
Hot leg temperature (K)	563.3±2.6	556.9
Cold leg temperature (K)	557.6±2.6	557.6
<b>Pressurizer</b>		
Steam Volume (m <sup>3</sup> )	0.43±0.05	0.48
Liquid volume (m <sup>3</sup> )	0.50±0.05	0.48
Water temperature (K)	614.9±1.3	614.7
Pressure (MPa)	14.93±0.25	14.93
Liquid level (m)	0.92±0.1	0.92



## 4. RESULTS AND DISCUSSION

### 4.1 Base Calculation

The results of the base calculation with the RELAP5 modeling described in the previous section are compared with the experimental data in Figures 3 through 13. Figures 3 to 7 are comparisons for short-term responses up to 300 seconds, while Figures 8 to 13 are comparisons for the long-term transient up to 10,000 seconds. In addition, the chronology of the major events for the base calculation is compared with the measured data in Table 2 for the LOFT Experiment L9-1/L3-3.

#### 4.1.1 Short-term Responses

The major thermal-hydraulic phenomena which can be observed during the short-term phase of the transient include, dryout of the SG secondary side, PCS pressurization, PCS pressure control by the pressurizer spray valve, and decay heat removal following reactor trip, etc.

The pressure trend of the PCS together with that of the SG secondary side is compared with experimental data in Figure 3. As the heat removal capability in the SG secondary side degraded due to the trip of the main feedwater pump, the pressure of the PCS gradually increased. When the PCS pressure reached the set pressure of 15.338 MPa, it was controlled by the pressurizer spray valve activation. As the heat generation in the reactor core exceeded the heat removal capability by both the SG secondary side and the pressurizer spray valve actuation, the PCS pressure continued to increase up to the reactor scram set pressure of 15.745 MPa. Following the scram, the PCS pressure decreased because the power input to the PCS dropped sharply to the decay power level. After that, the pressurization of the PCS due to decay heat was controlled by pressurizer spray actuation and subsequent steam condensation. The pressure of the SG secondary side rose gradually following initiation of the transient due to heating from the primary side. As the secondary side of the SG was drying out, however, the reduced heat removal capability decreased the pressure in the SG. The SG pressure increased again as the main steam control valve (MSCV) started to close on the reactor scram signal. As shown in Figure 3, the code pressure results calculated for both the PCS and the SG secondary side were in agreement with the experimental data.

The temperature comparisons of the calculated and experimental results for the PCS and the SG secondary side are shown in Figure 4. It is shown in the figure that the temperature behavior is predicted well by the code, even though minor discrepancies are shown. However, these differences are not considered significant to affect the later calculation results.

Figure 5 shows a comparison of the calculated reactor power to the experimental data. It is apparent that the predicted behavior of the reactor power is very similar to the experimental data. This implies that the code-predicted heat addition to the PCS during the transient matched well with the experiment.

A comparison of the experimental and calculated mass flow rate through the MSCV is presented in Figure 6. As the pressure in the SG secondary side increased, the mass flow rate through the MSCV increased until the MSCV started to close on the reactor scram signal. From this comparison, it can be stated that the mass flow rate behavior through the MSCV can be

predicted very well by the code.

Figure 7 shows a comparison of the calculated and experimental results for the SG collapsed liquid level. The SG secondary collapsed water level is a good indication of SG secondary conditions changing. The water level of the SG secondary side dropped monotonically due to evaporation without feed. As the water level decreased, the heat transfer rate through the SG U-tube degraded and this forced the PCS pressure to increase up to the reactor scram set point. After dryout of the SG secondary side, the heat transfer to the SG secondary side through the U-tube was by vapor natural circulation with a small wall heat transfer coefficient. This implies that the secondary system was de-coupled from the primary side and therefore it could no longer control the PCS pressurization. The calculated dryout rate of the SG secondary side closely resembled the test data as shown in Figure 7.

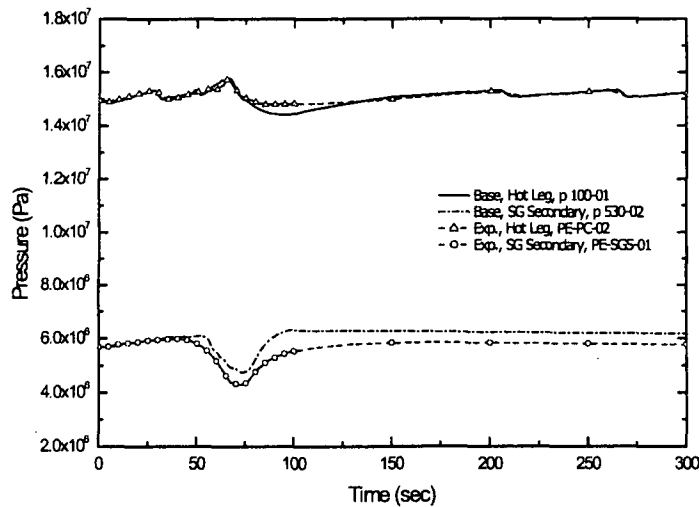


Figure 3. Comparison of Pressure for Short-term Response

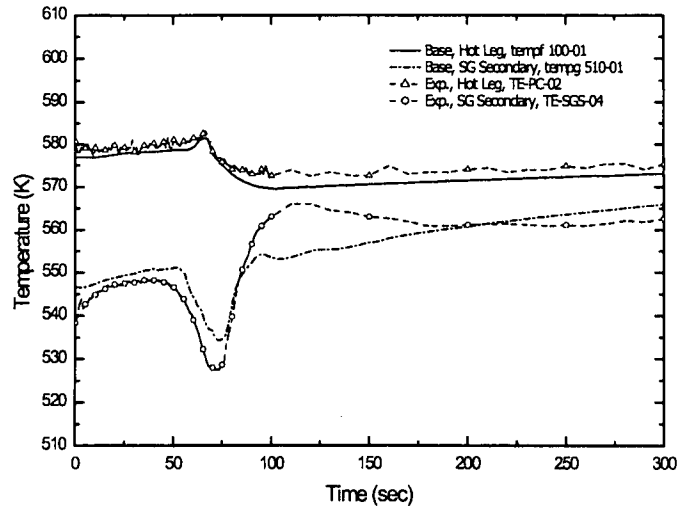


Figure 4. Comparison of Temperature for Short-term Response

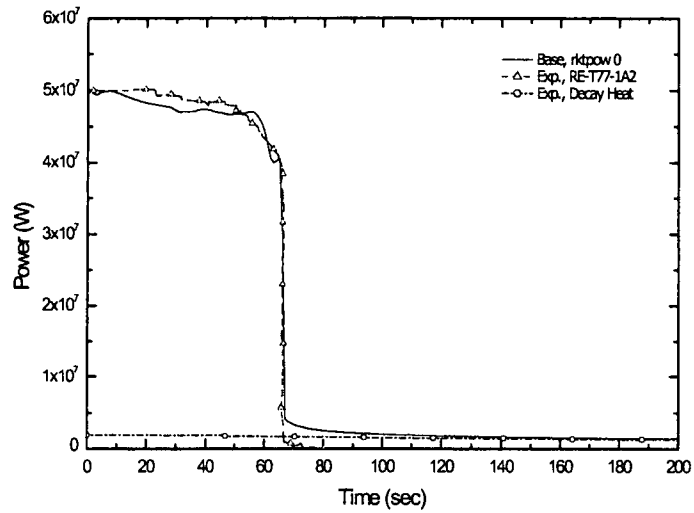


Figure 5. Comparison of Reactor Power for Short-term Response

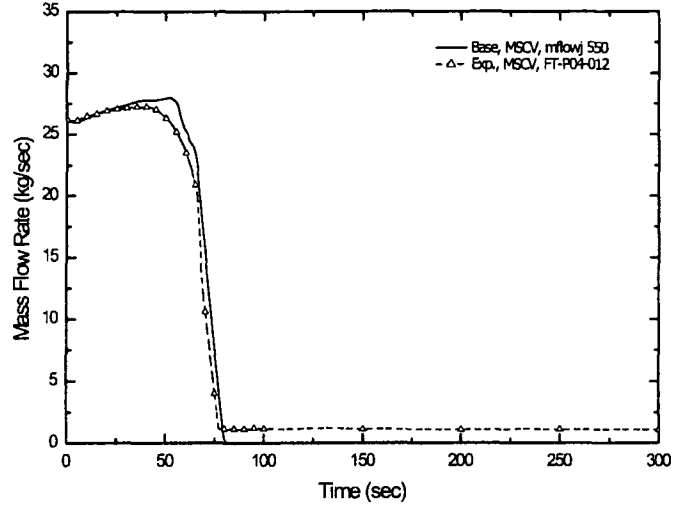


Figure 6. Comparison of Mass Flow Rate through MSCV for Short-term Response

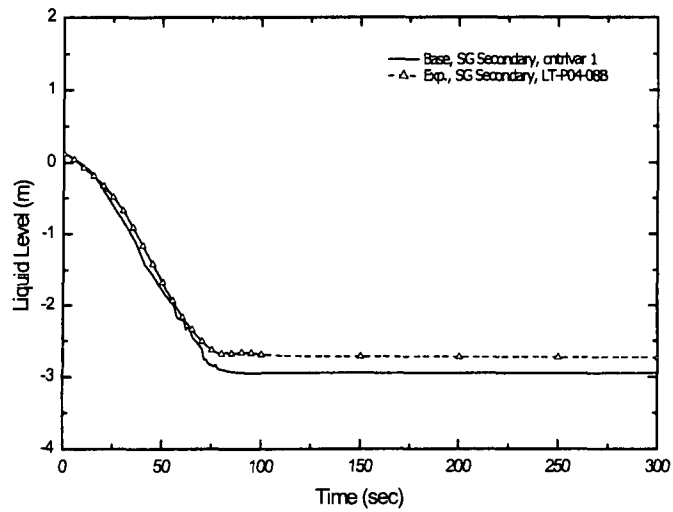


Figure 7. Comparison of SG Liquid Level for Short-term Response

Table 2. Major Sequence of Events for Experiment L9-1/L3-3

Event	Measured (sec)	Calculated (sec)
<b>L9-1</b>		
Main feedwater pump tripped off	0.0	0.0
Pressurizer spray activated	30.0±0.1	29.0
Reactor scram	65.4±0.2	65.0
Steam generator main steam control valve closed	77.2±0.2	80.0
Steam generator liquid level reached bottom of indicating range (0.25 m, above tube sheet)	190	71.0
Pressurizer spray valve cycling initiated	208.9±0.1	205.0
Pressurizer liquid level reached top of indicating range (1.83 m, above bottom)	1089.7±30	1365.0
Pressurizer spray valve cycling ended	1246.0±0.1	1785.0
PORV cycling initiated	1467.9±0.1	1785.0
<b>L3-3</b>		
PORV latched open	3269.9±0.1	3295.1
Primary coolant pumps tripped off	3284.8±0.2	3295.1
Primary coolant pump coastdown completed	3304.2±0.8	3330.1
Upper plenum fluid reached saturation pressure	3329.4±0.2	3405.3
PORV closed	4849.7±0.1	4880.4
Steam generator secondary refill initiated	5114.6±0.2	5145.4
Natural circulation initiated	5205±10	-
Steam generator secondary refill completed	5746.4±0.2	6255.5
Pressurizer liquid level reached bottom of indicating range (0.06 m, above bottom)	5915±5	5570.5
Steam generator secondary feed-and-bleed initiated	6712.2±0.2	7230.4
Experiment completed	9517.4±0.2	-

#### 4.1.2 Long-term Responses

Most of the thermal-hydraulic phenomena during the long-term phase occurred following sub-sequences such as PCS pressure control by PORV cycling and latched open, plant recovery by refilling the SG secondary side, and removing decay heat through a feed-and-bleed operation using the secondary side.

Figure 8 presents a comparison of calculated and experimental pressure value during the long-term transient phase for both the PCS and SG secondary side. The cycling operation of the pressurizer spray valve controlled the PCS pressure from the 30 seconds. In the experiment, the pressurizer spray was closed by an operator at 1,246.0 seconds. For the RELAP5 model, the pressurizer spray was modeled to be terminated on the indication of the PORV actuation. As decay heat added to the PCS exceeded the cooling capability of the pressurizer spray, the PORV cycling operation started to regulate the PCS pressure. The PORV cycling operation continued for about 1,800 seconds until the PORV was latched open. During the cycling operation by both the pressurizer spray valve and the PORV, the pressure of the SG secondary side was decreased monotonously. Figure 8 shows that the code-predicted pressure behavior during this period matched very well with test data.

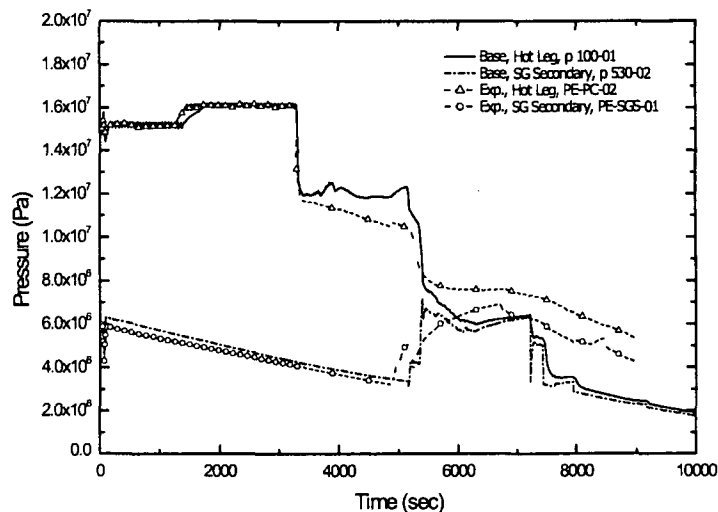


Figure 8. Comparison of Pressure for Long-term Response



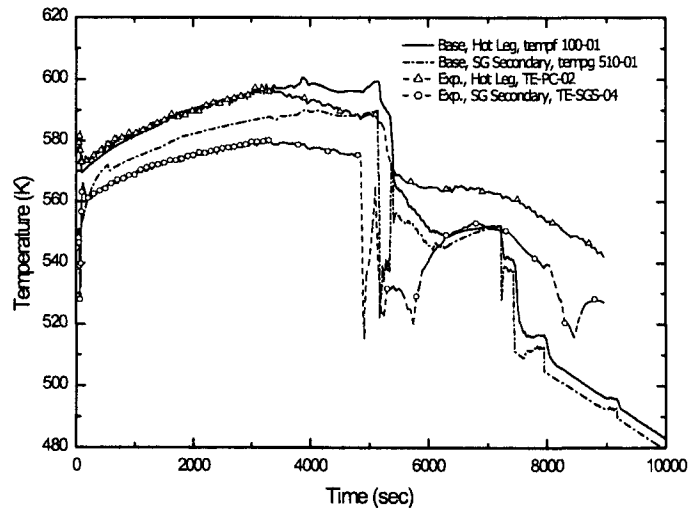


Figure 9. Comparison of Temperature for Long-term Response

The temperature for both the PCS and the SG secondary side during the cycling operation of the pressurizer spray valve and the PORV was increased gradually as presented in Figure 9. The calculated temperature of the PCS was in agreement with test data. The temperature of the SG secondary side, however, was over-estimated by the code. Since the SG was still in a de-coupled state from the PCS, the conservative prediction of the PCS behavior was not considered to be significant.

Figure 10 shows a comparison of pressurizer collapsed liquid level. It appears that the code-calculated liquid level is higher than the level in the experiment, especially during the PORV cycling operation. However, the difference is believed to be due to the fact that the differential pressure detector for water level calculation could not measure the water level over the upper detector location (1.83m, above bottom), while the code calculated the water level at the top of the pressurizer (2.0m, above bottom).

Experiment L3-3 was initiated by the PORV latched open. The LOFT plant recovery during this experiment was by two subsequent recovery procedures. The first recovery procedure was the PORV latched open to depressurize the primary coolant system. The second recovery procedure was by refilling the SG and removing decay heat through a feed-and-bleed operation using the SG secondary side.

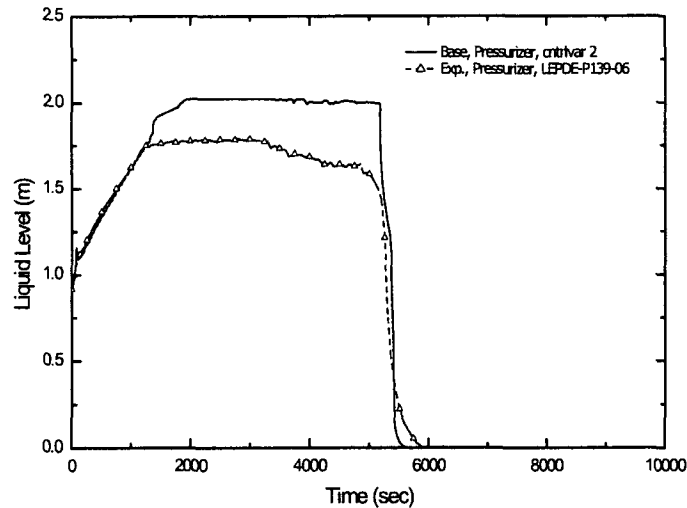


Figure 10. Comparison of Pressurizer Collapsed Liquid Level

The PORV was latched open at the 3,269.9 seconds, and maintained its state to 4849.7 seconds. The PCS pressure and temperature during the PORV latched open period was over-estimated by the code as seen in Figures 8 and 9, respectively. One of the reasons for this discrepancy was that the code-predicted excessive swelling of the PCS fluid during the time the PORV was latched open as noted in the reference calculation [4]. The excessive swelling of the code prediction can be confirmed from the behavior of the pressurizer water level in Figure 10.

The predicted water level during this period remained nearly constant, while the measured level decreased gradually as the fluid discharged through the PORV. This implies that the top of the pressurizer was filled with lower steam quality in the code calculation than in the experiment. Considering that water has much lower enthalpy than steam, the total discharged energy through the PORV would be under-estimated in the code, while the code-predicted mass flow rate through the PORV agreed well with the test data as shown in Figure 11. Therefore, it is concluded that over-estimation of the PCS pressure and temperature during the PORV latched open period is due to the code's under-estimation of total discharged energy through the PORV.

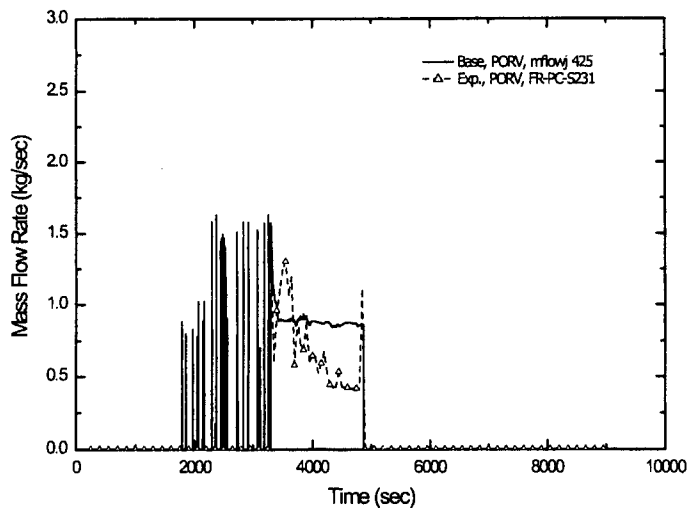


Figure 11. Mass Flow Rate through PORV for Long-term Response

Other important phenomena occurring during the period when the PORV was latched open were the changes in the fluid condition and the mass of the PCS. Figure 12 shows that the PCS fluid rapidly reached saturation conditions when the PORV was latched open, and, as a result, the steam started to be generated. In Figure 13, the change to the PCS system mass during this period is presented. It is apparent from Figure 13 that the code-calculated PCS mass behavior such as the total mass and the decreasing slope were very close to the measured data.

The second recovery procedure was initiated by refilling the SG secondary side through the auxiliary feedwater line, and the plant recovery was completed through feed-and-bleed operation. As the PCS was coupled again with the SG secondary side during the second recovery period, the PCS pressure and temperature decreased rapidly. It can be seen from Figures 8 and 9 that the code-predicted trends of the system pressure and temperature generally agree well with the experimental data, even though the excessive cooling by the code was also shown.

For the code-predicted excessive cooling during the second recovery procedure, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, the specific reasons for the deviation were not clearly identified in this assessment. Therefore, further investigations into the deviation sources are needed to enhance the code's predictability.

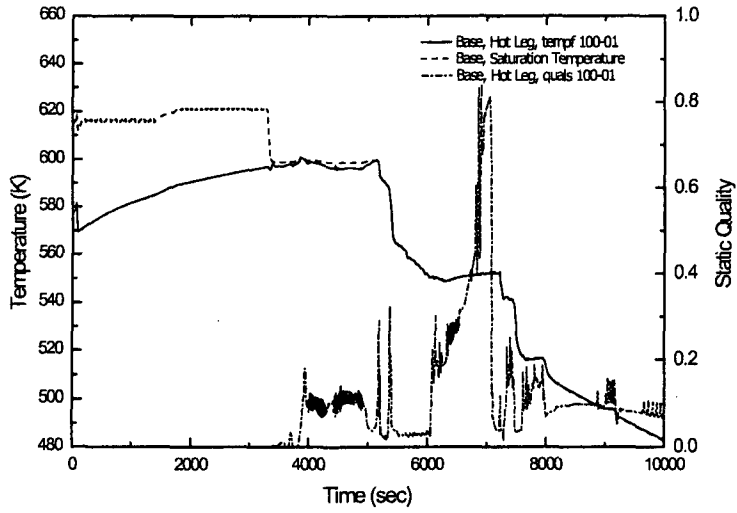


Figure 12. Fluid Conditions of Hot Leg for Long-term Response

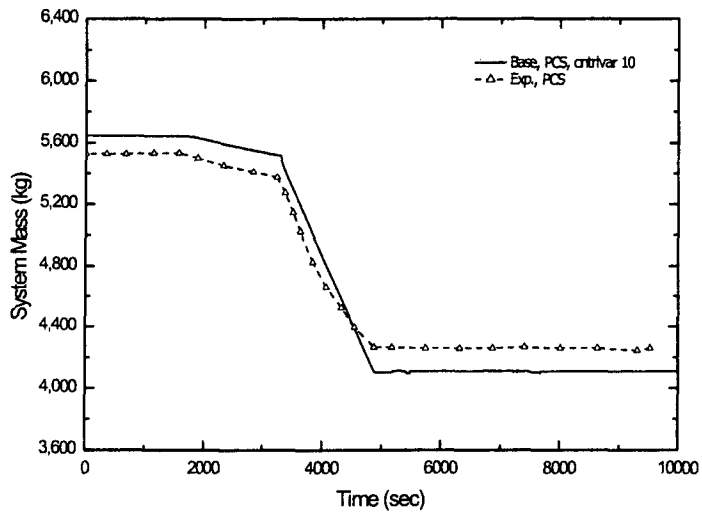


Figure 13. System Mass of PCS for Long-term Response

## 4.2 Sensitivity Studies

The sensitivity studies were performed to identify parameters having significant effect on the predicted thermal hydraulic behaviors. The cases and the parameters for the sensitivity studies are presented in Table 3. The first three parameters were selected as short-term parameters, while the last two were chosen as parameters which affect the long-term transient behavior. The code-predicted results for each case are compared with both the base calculation and the experimental data in Figures 14 through 17.

Table 3. Matrix for Sensitivity Studies

PARAMETERS		CASES	Base	Case 1	Case 2	Case 3	Case 4	Case 5
Short-term Parameters	Pressurizer Spray Valve Loss Coefficient		1.0	15.432 (Note 1)	Base	Base	Base	Base
	SG Nodalization		6	Base	3 (Note 1)	Base	Base	Base
	SG U-tube Heat Trans. Area (Cylinder Height)		12149.9 m <sup>2</sup>	Base	Base	10124.9 m <sup>2</sup> (Note 1)	Base	Base
Long-term Parameters	Heat Transfer Coefficient to Environment		(Note 2)	Base	Base	Base	(Note 1)	Base
	PORV Discharge Coefficient		0.8	Base	Base	Base	Base	1.0 (Note 1)

Notes:

1. These values are identical to those in NUREG/IA-0114 [4]. The environmental loss heat transfer coefficients for components are as follows:  
 Reactor Vessel and Pipe: 13.450 W/m<sup>2</sup>K  
 Steam Generator: 3.385 W/m<sup>2</sup>K  
 Pressurizer: 3.019 W/m<sup>2</sup>K
2. Compared to those in the NUREG/IA-0114, the environmental loss heat transfer coefficients for these cases are increased by 40% as follows:  
 Reactor Vessel and Pipe: 18.830 W/m<sup>2</sup>K  
 Steam Generator: 4.739 W/m<sup>2</sup>K  
 Pressurizer: 4.227 W/m<sup>2</sup>K

### 4.2.1 Pressurizer Spray System Loss Coefficient (Case 1)

The pressurizer spray in the LOFT facility was used to regulate the PCS pressure by condensing steam at the top of the pressurizer. The loss coefficient of the pressurizer spray system which determines the amount of the spray flow was known to have a remarkable effect on the RCS pressure behavior [9]. In this sensitivity study, the effect of the mass flow rate

through the spray valve was investigated. The mass flow rate was reduced from 1.7 kg/sec to 1.0 kg/sec by increasing the loss coefficient of the spray valve from 1.0 to 15.432 [4]. From the comparison in Figure 14, it is seen that the pressure before reactor scram increased more rapidly than for the base calculation, as the reduced mass flow rate was not sufficient to suppress the pressure increase. The pressure increase after the reactor scram, however, was slower than that for the base calculation because the heat added to the PCS was smaller than in the base calculation due to the earlier reactor trip.

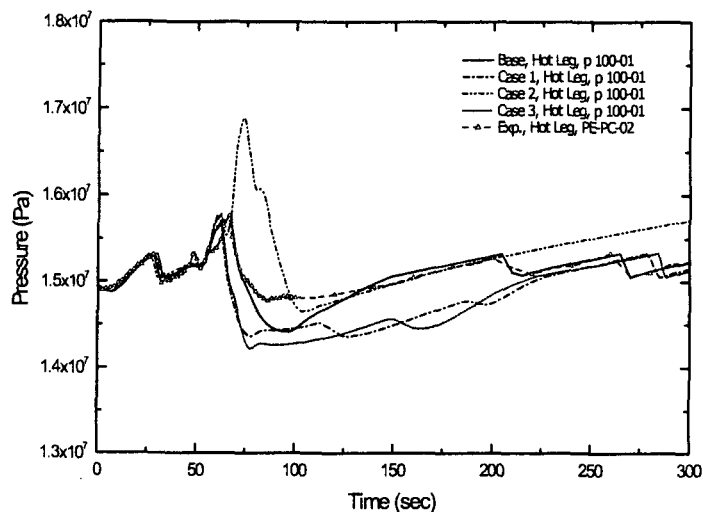


Figure 14. Sensitivity Studies for Short-term Parameters

#### 4.2.2 Steam Generator Nodalization (Case 2)

The heat transfer phenomena through the SG U-tube plays a very important role in this type of transient, because the heat generated in the reactor is mainly removed by the SG secondary side until it is de-coupled after a complete depletion. The SG nodalization is one of the most important parameters which affect the heat transfer phenomena through the SG [9, 10]. The effect of coarse nodalization of the SG was examined for this case. The nodes of the SG U-tube and the SG secondary side associated with the U-tube were reduced from 6 to 3 nodes, which implied that the subdivided four nodes in the base calculation were merged into one node as in the reference calculation [4]. As shown in Figure 14, this modeling change caused completely different results from the base calculation. The PCS pressure surge was not controlled, even though the reactor trip was accomplished on indication of the PCS high pressure. The pressure was not suppressed until it had increased sharply to the PORV actuation set pressure. The reason for this can be deduced from a comparison of the heat transfer rate through the U-tube.

Figure 15 shows that the heat transfer rate during the period of the steep pressure increase after the reactor trip was lower for this case than for the base calculation, which led to the PCS over-pressurization. Therefore, the PCS over-pressurization can be attributed to the coarse nodalization of the SG U-tube and the associated SG secondary side.

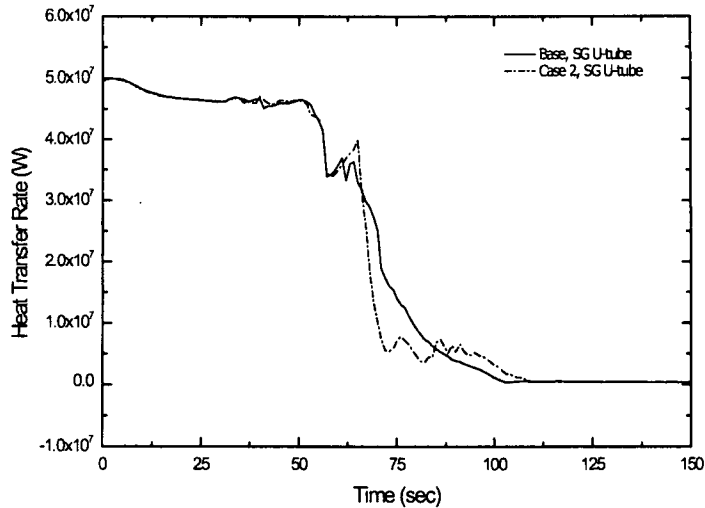


Figure 15. Comparison of Heat Transfer Rate through SG U-tube

#### 4.2.3 Steam Generator U-tube Heat Transfer Area (Case 3)

The heat transfer area of the SG U-tube was generally identified as a factor to have an impact on the initial conditions in the SG secondary side [4, 11]. This implies that the SG U-tube heat transfer area may also affect the SG heat transfer phenomena during the transient phase. Therefore, the SG U-tube heat transfer area also selected as a sensitivity parameter. In this sensitivity study, the heat transfer area of all the nodes of the SG U-tube was reduced to  $10,124.886 \text{ m}^2$  [4] from  $12,149.864 \text{ m}^2$  in the base calculation. From Figure 14, the PCS pressure behavior for Case 3 is very similar to that in the Case 1, i.e., reduction of the pressurizer spray valve loss coefficient. The reactor tripped earlier due to the reduced heat transfer to the SG secondary side, and the pressure increase after the reactor trip was slower than for the base calculation due to the reduced heat added to the PCS from the reactor core as in Case 1.

#### 4.2.4 Heat Transfer Coefficient to Environment (Case 4)

Generally, the heat losses to the environment from the plant main components after a reactor trip can affect the long-term trend of the transient since the amount of the heat loss to the environment is not negligible compared to the decay heat level. In the previous calculation using RELAP5/MOD1, the PCS fluid heatup rate during the PORV cycling operation was much faster than in the experiment, and the amount of the discharged coolant through the PORV was greater in the calculation than in the experiment [3,7]. This difference was considered due to higher environmental heat losses from the primary system than assumed [3]. In this sensitivity study, the effect of the environmental heat losses was investigated. The values from reference calculation [4] were used as heat transfer coefficients of the major components such as the

reactor vessel, the steam generator, the pressurizer, and primary coolant system, as shown in Table 3. This implies that the total heat loss to the environment from the plant main components was decreased by about 40% in this sensitivity study. As shown in Figure 16, the environmental heat loss mainly affected the PCS temperature behavior during the cycling operation period of both the pressurizer spray and the PORV. During this period, the temperature increased more rapidly than for the base calculation as the total heat loss to the environment was reduced. In addition, the steeper temperature increase resulted in the successive key events such as the PORV latched open, the SG refill, and the feed-and-bleed operation to occur earlier than for the base calculation.

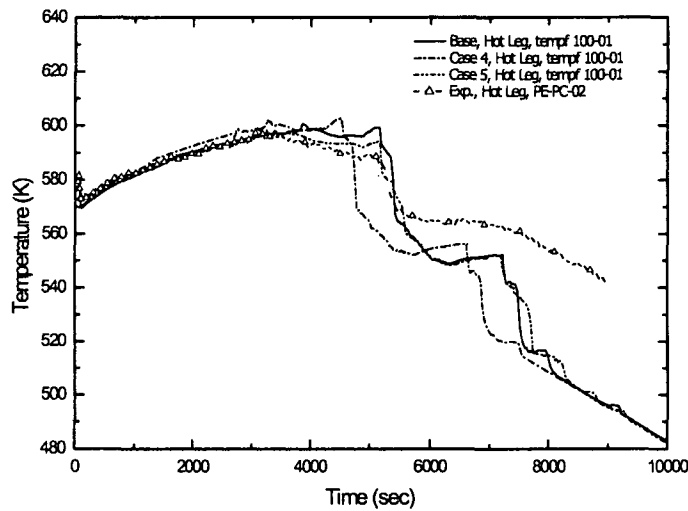


Figure 16. Sensitivity Studies for Long-term Parameters

#### 4.2.5 PORV Discharge Coefficient (Case 5)

The effect of the discharge coefficient and the thermal nonequilibrium constant of the PORV were checked by setting them at 1.0 and 0.14, respectively. The calculated mass flow rates using these settings are compared in Figure 17. Compared to the base calculation, the mass flow rate through the PORV for this sensitivity increased up to 50% during the PORV latched open period as shown in Figure 17. This increased mass flow resulted in a more rapid PCS cooling during the PORV latched open period. However, the PCS temperature behavior during the cycling operation of the PORV was not influenced by the increased mass flow rate through the PORV as shown in Figure 16.



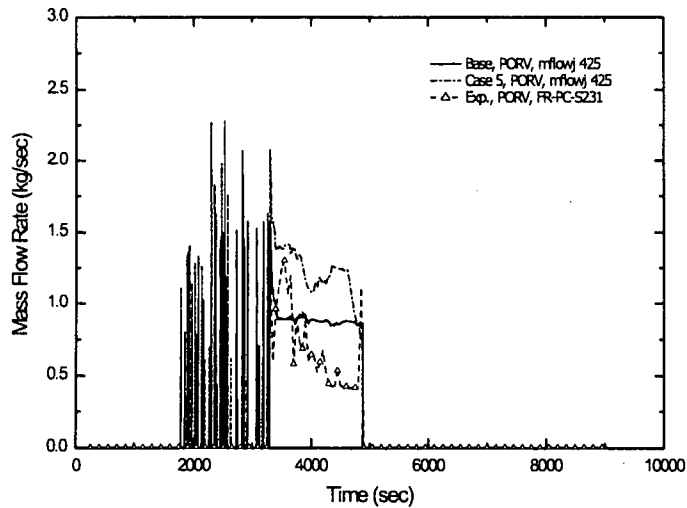


Figure 17. Sensitivity Study for Mass Flow Rate through PORV

### 4.3 Run Statistics

An IBM Personal Computer (Pentium III 933 MHz) was used for the present calculations with a DOS operating system. The required CPU time and the time step size with respect to the real transient times for the base calculation are presented in Figures 18 and 19, respectively. Figure 18 shows that the required CPU time up to the real transient time of 10,000 seconds is 2,427.76 seconds, including the input processing time of 3.46 seconds. Therefore, the grind time for the base calculation is calculated as follows:

CPU time,  $CPU = 2,427.76 - 3.46 = 2424.3 \text{ sec}$

Number of time steps,  $DT = 125,092$

Number of volumes,  $C = 134$

Grind time =  $CPU \times 1,000 / (C \times DT) = 0.14463 \text{ CPU msec/vol/step}$

In Figure 19, the advanced time step size is compared with the Courant time step size. The maximum time steps specified in the base input decks were 1.0 second up to 1,000 seconds, 0.1 second up to 2,000 seconds, 0.5 second up to 4,000 seconds, 0.1 second up to 8,000 seconds, and 0.5 second up to 10,000 seconds of the real transient time. It is shown in Figure 19 that the advanced time step sizes were below the Courant time step sizes throughout the transient.

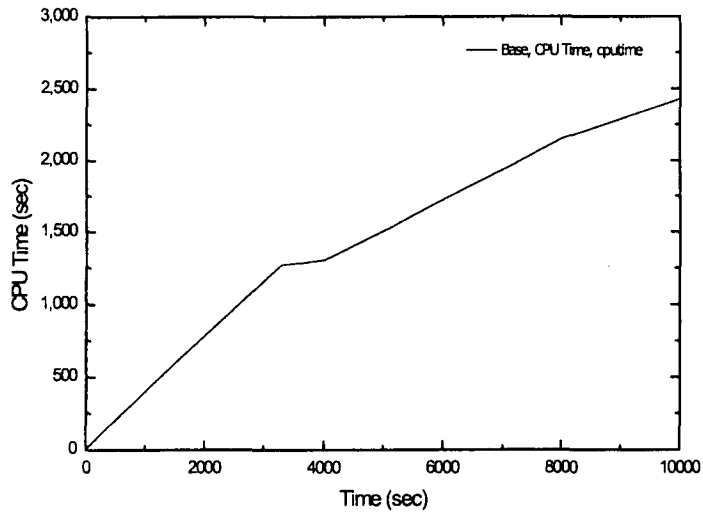


Figure 18. Required CPU Time of Base Calculation

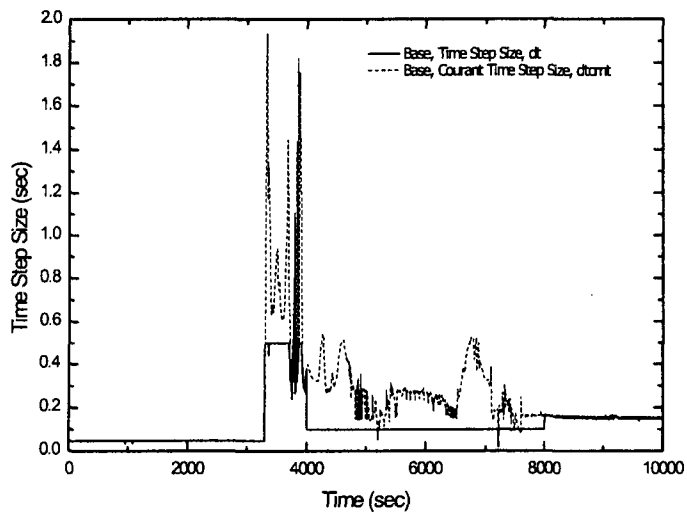


Figure 19. Time Step Size of Base Calculation

## 5. CONCLUSIONS

The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3. For this purpose, major parameters identified through sensitivity studies to have the most significant effect on the predicted thermal-hydraulic behaviors were incorporated into the base calculation to improve the code predictability. The code-predicted results were compared with the experimental data to assess the code predictability. Major conclusions through this assessment are summarized as follows:

From the comparisons presented with Figures and Tables, it was shown that the code-predicted results were generally in agreement with the measured data. Therefore, it is concluded that the RELAP5/MOD3.3Beta computer code has sufficient capability in predicting the thermal hydraulic phenomena occurred in the LOFT Experiment L9-1/L3-3.

However, the discrepancies between the calculation and the experiment were also identified. In Experiment L9-1, the code over-estimated temperature behaviors of the SG secondary side after dryout of the SG. However, these discrepancies were not considered to be significant, since the SG was in a de-coupled state from the PCS after the dryout of the SG secondary side. In Experiment L3-3, the code predicted excessive swelling of the PCS fluid during the first recovery mode, and predicted excessive cooling during the second recovery mode. The differences during the first recovery mode were due to the code's under-estimation of total discharged energy through the PORV. For the discrepancies during the second recovery mode, the code modeling deficiency of the SG secondary side was presumed to be one of the reasons. However, it is concluded that further investigation into the deviation sources are needed to enhance the code's predictability, since the specific reasons for the deviation were not clearly identified in this assessment.

Through sensitivity studies, the major parameters were identified to have significant effect on the predicted thermal-hydraulic behaviors. These parameters include the pressurizer spray system loss coefficient, nodalization of the SG secondary side, SG U-tube heat transfer area, heat transfer coefficient from the LOFT main components to the environment, and the PORV discharge coefficient. The first three parameters are significant during the short-term transient phase, while the last two are significant during the long-term transient phase. Therefore, the five parameters listed above should be carefully modeled to obtain appropriate calculation results for transient types such as the total-loss-of feedwater accident and its recovery modes.



## 6. REFERENCES

1. Information Systems Laboratories, Inc., *RELAP5/MOD3.3Beta Code Manuals*, NUREG/CR-5535/Rev.1, May 2001.
2. United States Atomic Energy Commission, *Reactor Safety Study*, WASH-1400, NUREG-75/012, October 1975.
3. Charles L. Nalezny, *Summary of the Nuclear Regulatory Commission's LOFT Program Research Findings*, NUREG/CR-3005, April 1985.
4. Young Seok Bang, et al., *Assessment of RELAP5/MOD3 with the LOFT L9-1/L3-3 Experiment Simulating an Anticipated Transient with Multiple Failure*, NUREG/IA-0114, February 1994.
5. M. L. McCormick-Barger, et al., *Experiment Data Report for LOFT Anticipated Transient with Multiple Failures Experiment L9-1 and Small Break Experiment L3-3*, NUREG/CR-2119, June 1981.
6. Douglas L. Reeder, *LOFT System and Test Description*, NUREG/CR-0247, July 1978.
7. James P. Adams, *Quick-Look Report on LOFT Nuclear Experiment L9-1/L3-3*, EGG-LOFT-5430, April 1981.
8. B. Sheron, *Generic Assessment of Delayed Reactor Coolant Pump Trip during Small Break Loss-of-Coolant Accidents in Pressurized Water Reactors*, NUREG-0623, November 1979.
9. J. K. Suh, et. al., *Assessment of RELAP5/MOD3.2.2Gamma with the LOFT L9-3 Experiment Simulating an Anticipated Transient Without Scram*, NUREG/IA-0192, January 2001.
10. J. C. Birchley, *RELAP5/MOD2 Analysis of LOFT Experiment L9-3*, NUREG/IA-0058, April 1992.
11. R. Beelman, *RELAP5 Reference Calculation and Posttest Analysis of Anticipated Transient with Multiple Failures Experiment L9-1/L3-3*, EGG-LOFT-5895, September 1982.



## **Appendix A**

### **Steady State Input Deck for Base Case**







```

0000381 pmphead 135 * pcp1 head
0000382 pmphead 165 * pcp2 head
0000384 cntrivar 2 * pcr level
0000385 cntrivar 3 * rx vessel level
0000386 mflowj 185010000
0000387 mflowj 185030000
0000388 mflowj 200020000
0000389 pmpvel 135
0000390 pmpvel 165
*****
*
* trips
*
*****
* variable trips
*****
0000501 p 100010000 le null 0 14.193103e6 l
* ecc check valve
0000502 p 600010000 ge p 185010000 20.e6 n
* accumulator check valve
0000503 p 615010000 ge p 185010000 20.e6 n
* isolation valve hot leg
0000504 time 0 lt null 0 0.0 l
* isolation valve cold leg
0000505 time 0 lt null 0 0.0 l
* qobv hot leg
0000506 time 0 lt null 0 0.0 l
* qobv cold leg
0000507 time 0 lt null 0 0.0 l
* check valve surge line pressurizer
0000508 time 0 ge null 0 0.0 l
* pressurizer relief valve
0000509 tempf 100010000 ge null 0 597.0 l
* steam control valve
0000510 time 0 lt null 0 0.0 l
* boundary system valve
0000511 time 0 lt null 0 0.0 l
* lpiis trip
0000512 time 0 ge null 0 10000.0 l
* hpis trip
0000513 time 0 ge null 0 10000.0 l
*
0000520 p 530020000 gt null 0 7.103448e6 n
0000521 p 530020000 lt null 0 7.0344827e6 n
0000522 p 530020000 gt null 0 6.3448275e6 n
0000523 p 530020000 lt null 0 6.4137931e6 n
0000530 time 0 ge null 0 3600.0 n
0000531 p 530020000 gt p 547010000 0.0 n
0000536 time 0 ge null 0 10000.0 n
0000540 tempf 100010000 gt null 0 583.16 l
0000541 p 100010000 gt null 0 1.574553e7 l
0000550 time 0 ge null 0 10000.0 l
0000551 time 0 ge timeof 625 0.0 l
0000552 time 0 ge timeof 509 1580. l
0000560 p 100010000 le null 0 13.15862e6 n
0000561 time 0 ge timeof 552 265.0 l
0000562 time 0 gt null 0 5400.0 n
0000563 cntrivar 1 lt null 0 2.1844 n
0000564 cntrivar 1 gt null 0 2.9464 n
0000565 time 0 ge timeof 669 966. l

```

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0000570 p 420010000 gt null 0 1.620058e7 n
0000571 p 420010000 lt null 0 1.606269e7 n
0000572 p 420010000 lt null 0 1.486300e7 n
0000573 p 420010000 gt null 0 1.506980e7 n
0000574 p 420010000 gt null 0 1.533874e7 n
0000575 p 420010000 lt null 0 1.505000e7 n
0000576 p 420010000 lt null 0 1.482853e7 n
0000577 p 420010000 gt null 0 1.495950e7 n
*****
* logical trips
*****
0000600 670
0000601 563 and 561 n
0000602 -563 and -564 n
0000603 655 and 602 n
0000604 609 or 609 l
0000605 572 and -509 n
0000606 -572 and -573 n
0000607 608 and 606 n
0000608 605 or 607 n
0000609 504 or 504 l
0000610 612 or 520 n
0000611 -521 and -616 n
0000612 611 and 610 n
0000613 616 or 523 n
0000614 -522 and 613 n
0000615 -612 and 609 n
0000616 615 and 614 n
0000617 612 or 616 n
0000618 605 or 607 n
0000621 623 or 570 n
0000622 -571 and -571 n
0000623 621 and 622 n
0000624 509 and -552 n
0000625 623 or 624 n
0000626 576 and -509 n
0000627 -576 and -577 n
0000628 629 and 627 n
0000629 626 or 628 n
0000635 504 and 504 n
0000636 509 and -536 n
0000650 -652 and 550 n
0000651 650 or 652 n
0000652 -509 and 651 n
0000655 601 or 603 n
0000656 508 or 609 n
0000659 561 or 562 n
0000660 504 or 504 n
0000669 561 and 564 l
0000670 565 and -655 n
0000680 530 or 530 n
0000688 690 or 574 n
0000689 -575 and -551 n
0000690 688 and 689 n
*****
*
* intact loop
*
*****
* reactor vessel nozzle - intact loop hot leg

```

```

*****
1000000 rvnihl      branch
1000001 2      0
1000101 0.0634 1.5373 0.0 0.0 0.0 0.0
1000102 4.0e-5 0.0 00000
1000200 0      14901000. 1346300.0 2462060.0 0.0
1001101 25000000 10000000 0.0634 0.0 0.0 000100
1002101 100010000 105000000 0.0 0.05 0.05 000100
1001201 10.582000 11.005000 0.0
1002201 10.582000 10.625000 0.0
*****
* pressurizer connection tee reactor vessel side
*****
1050000 pztrvs      branch
1050001 1      0
1050101 0.0634 1.634 0.0 0.0 0.0 0.0
1050102 4.0e-5 0.0 00000
1050200 0      14896100. 1346300. 2462190.0 0.0
1051101 105010000 110000000 0.0 0.05 0.05 000100
1051201 13.795000 13.974000 0.0
*****
* steam generator inlet piping
*****
1100000 sginlp      branch
1100001 1      0
1100101 0.0 0.623 0.0303 0.0 0.0 0.0
1100102 4.0e-5 0.0 00000
1100200 0      14857200. 1346340. 24629400.0 0.000000
1101101 110010000 115000000 0.0 0.1 0.1 000100
1101201 13.801000 13.692000 0.0
*****
* steam generator plus piping
*****
1150000 sgppip      pipe
1150001 19
1150101 0.0 3
1150102 0.151 15
1150103 0.0 18
1150104 0.0634 19
1150201 0.0 1
1150202 0.0512 2
1150203 0.0 15
1150204 0.0512 16
1150205 0.0 18
1150301 1.4385 1
1150302 0.708 2
1150303 0.63 3
1150304 0.26675 7
1150305 1.067 8
1150306 0.45 10
1150307 1.067 11
1150308 0.26675 15
1150309 0.63 16
1150310 0.547 17
1150311 0.689 18
1150312 0.559 19
1150401 0.09 1
1150402 0.057 2
1150403 0.335 3
1150404 0.0 15
1150405 0.335 16
1150406 0.0437 17
1150407 0.0462 18
1150408 0.0 19
1150501 0.0 19
1150601 0.0 1
1150602 90.0 9
1150603 -90.0 19
1150701 0.0 1
1150702 0.246 2
1150703 0.513 3
1150704 0.26675 7
1150705 1.067 8
1150706 0.2865 9
1150707 -0.2865 10
1150709 -1.067 11
1150710 -0.26675 15
1150711 -0.513 16
1150712 -0.498 17
1150713 -0.689 18
1150714 -0.356 19
1150801 4.0e-5 0.0 2
1150802 4.0e-5 0.0102 3
1150803 1.0e-5 0.0103 15
1150804 4.0e-5 0.0102 16
1150805 4.0e-5 0.0 19
1150901 0.15 0.15 1
1150902 0.05 0.05 2
1150903 0.0 0.0 7
1150904 0.1 0.1 8
1150905 0.2 0.2 9
1150906 0.1 0.1 10
1150907 0.0 0.0 15
1150908 0.05 0.05 16
1150909 0.1 0.1 18
1151001 00000 19
1151101 000100 2
1151102 100100 3
1151103 000000 14
1151104 000100 18
1151201 0      14871600. 1346350. 2462710.0 0.0 0.0 01
1151202 0      14877200. 1346350. 2462600.0 0.0 0.0 02
1151203 0      14793300. 1346370. 2464340.0 0.0 0.0 03
1151204 0      14770000. 1321980. 2464840.0 0.0 0.0 07
1151205 0      14746400. 1301720. 2465340.0 0.0 0.0 08
1151206 0      14729700. 1283950. 2465690.0 0.0 0.0 09
1151207 0      14721700. 1268380. 2465870.0 0.0 0.0 10
1151208 0      14715000. 1254890. 2466020.0 0.0 0.0 11
1151209 0      14707300. 1242570. 2466180.0 0.0 0.0 15
1151210 0      14707600. 1242600. 2466180.0 0.0 0.0 16
1151211 0      14631100. 1242600. 2467720.0 0.0 0.0 17
1151212 0      14621800. 1242600. 2467980.0 0.0 0.0 18
1151213 0      14616700. 1242600. 2468100.0 0.0 0.0 19
1151300 0
1151301 10.728000 10.670000 0.0 01
1151302 8.3370000 8.4284000 0.0 02
1151303 4.4456000 4.7693000 0.0 03
1151304 4.3865000 4.2164000 0.0 07
1151305 4.3407000 4.6700000 0.0 08
1151306 4.3009000 4.6296000 0.0 09

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1151307 4.2676000 4.5954000 0.0 10
1151308 4.2398000 4.5671000 0.0 11
1151309 4.2249000 4.5338000 0.0 15
1151310 7.9665000 8.1922000 0.0 16
1151311 9.4925000 9.9460000 0.0 17
1151312 10.040000 10.5050000 0.0 18
1151401 1.0224e-2 0. 1. 1. 18
*****
*
*      pump data
*
*****
* pump suction tee
*****
1200000  pmpscct      branch
1200001  3          0
1200101  0.0634  0.76   0.0   0.0   0.0   0.0
1200102  4.0e-5  0.0    00000
1200200  0        14613100. 1242600. 2468180.0 0.0
1201101  115010000 120000000 0.0 0.1 0.1 000000
1202101  120010000 125000000 0.0317 0.2 0.2 000100
1203101  120010000 155000000 0.0317 0.2 0.2 000100
1201201  10.040000 10.5050000 0.0
1202201  5.2077000 5.2983000 0.0
1203201  5.2071000 5.2944000 0.0
*****
* pump1 suction tee outlet
*****
1250000  pmp1scct      branch
1250001  2          0
1250101  0.0        1.003  0.0613  0.0   90.0  0.521
1250102  4.0e-5    0.0    00000
1250200  0          14600300. 1242600. 2468180.0 0.0
1251101  125010000 130000000 0.0 0.1 0.1 000100
1252101  125000000 155000000 0.0 0.0 0.0 000100
1251201  7.8711000 8.2528000 0.0
1252201  -.11855000 -1.13539000 0.0
*****
* pump 1 inlet
*****
1300000  pmp1inlet      snglvol
1300101  0.0        0.457  0.0189  0.0   90.0  0.457
1300102  4.0e-5    0.0    00000
1300200  0          14578200. 1242600. 2468900.0 0.0
*****
* primary coolant pump 1
*****
1350000  pcump1      pump
1350101  0.0366  0.0   0.099  0.0   90.0  0.319
1350102  00000
1350108  130010000 0.0   0.0   0.0  000100
1350109  140000000 0.0   0.05  0.05  000100
1350200  0        14818100. 1242890. 2463900.0 0.0
1350201  0        8.8943000 9.2942000 0.0
1350202  0        8.8928000 8.1177000 0.0
1350301  0 0 0      -1  -1      504  0
1350302  369.00 .90178860 .315500 96.00 500.600 1.43100
1350303  613.6  0.0   207.0000 0.0040000 19.598000 0.0
1350310  0.0   0.0   0.0
*

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```

*****
* single phase head curves
*****
* head curve no. 1
*---1---1---1---1---1---1---
1351100  1          1
1351101  0.000000e+00  1.403600e+00
1351102  1.906100e-01  1.363600e+00
1351103  3.896300e-01  1.318600e+00
1351104  5.939600e-01  1.232800e+00
1351105  7.902000e-01  1.133600e+00
1351106  1.000000e+00  1.000000e+00
*---1---1---1---1---1---1---
* head curve no. 2
*---1---1---1---1---1---1---
1351200  1          2
1351201  0.000000e+00  -6.700000e-01
1351202  2.000000e-01  -5.000000e-01
1351203  4.000000e-01  -2.500000e-01
1351204  5.755400e-01  0.000000e+00
1351205  7.443200e-01  2.583000e-01
1351206  7.734800e-01  3.778000e-01
1351207  8.631300e-01  6.326000e-01
1351208  1.000000e+00  1.000000e+00
*---1---1---1---1---1---1---
* head curve no. 3
*---1---1---1---1---1---1---
1351300  1          3
1351301  -1.000000e+00  2.472200e+00
1351302  -8.057400e-01  2.047400e+00
1351303  -6.069000e-01  1.831000e+00
1351304  -4.068300e-01  1.624000e+00
1351305  -2.001710e-01  1.470500e+00
1351306  0.000000e+00  1.403600e+00
*---1---1---1---1---1---1---
* head curve no. 4
*---1---1---1---1---1---1---
1351400  1          4
1351401  -1.000000e+00  2.472200e+00
1351402  -8.229700e-01  1.996800e+00
1351403  -6.333200e-01  1.589700e+00
1351404  -4.553400e-01  1.327900e+00
1351405  -2.710900e-01  1.194900e+00
1351406  -1.771600e-01  1.060500e+00
1351407  -9.073000e-02  1.015600e+00
1351408  0.000000e+00  9.342790e-01
*---1---1---1---1---1---1---
* head curve no. 5
*---1---1---1---1---1---1---
1351500  1          5
1351501  0.000000e+00  2.500000e-01
1351502  2.000000e-01  2.800000e-01
1351503  4.000000e-01  3.400000e-01
1351504  4.118000e-01  2.768000e-01
1351505  5.976300e-01  4.584000e-01
1351506  7.934670e-01  6.992000e-01
1351507  1.000000e+00  1.000000e+00
*---1---1---1---1---1---1---
* head curve no. 6
*---1---1---1---1---1---1---

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```

1351600 1 6
1351601 0.000000e+00 9.342790e-01
1351602 9.109900e-02 9.229000e-01
1351603 1.865090e-01 8.963000e-01
1351604 2.717620e-01 8.750000e-01
1351605 4.558720e-01 8.433000e-01
1351606 5.744060e-01 8.355000e-01
1351607 7.405760e-01 8.466000e-01
1351608 7.666190e-01 8.469000e-01
1351609 8.714710e-01 8.838000e-01
1351610 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----1-----
* head curve no. 7
*-----1-----1-----1-----1-----1-----1-----
1351700 1 7
1351701 -1.000000e+00 -1.000000e+00
1351702 -8.000000e-01 -6.300000e-01
1351703 -6.000000e-01 -3.000000e-01
1351704 -4.000000e-01 -5.000000e-02
1351705 -2.000000e-01 1.500000e-01
1351706 0.000000e+00 2.500000e-01
*-----1-----1-----1-----1-----1-----1-----
* head curve no. 8
*-----1-----1-----1-----1-----1-----1-----
1351800 1 8
1351801 -1.000000e+00 -1.000000e+00
1351802 -8.000000e-01 -9.700000e-01
1351803 -6.000000e-01 -9.500000e-01
1351804 -4.000000e-01 -8.800000e-01
1351805 -2.000000e-01 -8.000000e-01
1351806 0.000000e+00 -6.700000e-01
*****
* single phase torque data
*****
* torque curve no. 1
*-----1-----1-----1-----1-----1-----1-----
1351900 2 1
1351901 0.000000e+00 6.032000e-01
1351902 1.930000e-01 6.325000e-01
1351903 3.930000e-01 7.369000e-01
1351904 5.952000e-01 8.331000e-01
1351905 7.978200e-01 9.229000e-01
1351906 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 2
*-----1-----1-----1-----1-----1-----1-----
1352000 2 2
1352001 0.000000e+00 -6.700000e-01
1352002 4.000000e-01 -2.500000e-01
1352003 5.000000e-01 1.500000e-01
1352004 7.372550e-01 5.265860e-01
1352005 7.680490e-01 6.065940e-01
1352006 8.672300e-01 7.436600e-01
1352007 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 3
*-----1-----1-----1-----1-----1-----1-----
1352100 2 3
1352101 -1.000000e+00 1.984300e+00
1352102 -8.009600e-01 1.394000e+00

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1352103 -6.063800e-01 1.097500e+00
1352104 -4.068600e-01 8.220000e-01
1352105 -1.992800e-01 6.648000e-01
1352106 0.000000e+00 6.032000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 4
*-----1-----1-----1-----1-----1-----1-----
1352200 2 4
1352201 -1.000000e+00 1.984300e+00
1352202 -8.223400e-01 1.830800e+00
1352203 -6.337100e-01 1.682400e+00
1352204 -4.585300e-01 1.557000e+00
1352205 -2.670230e-01 1.436200e+00
1352206 -1.761070e-01 1.387900e+00
1352207 -8.931000e-02 1.348100e+00
1352208 0.000000e+00 1.233610e+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 5
*-----1-----1-----1-----1-----1-----1-----
1352300 2 5
1352301 0.000000e+00 -4.500000e-01
1352302 4.000000e-01 -2.500000e-01
1352303 5.000000e-01 0.000000e+00
1352304 1.000000e+00 3.569000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 6
*-----1-----1-----1-----1-----1-----1-----
1352400 2 6
1352401 0.000000e+00 1.233610e+00
1352402 9.064300e-02 1.196500e+00
1352403 1.885690e-01 1.109600e+00
1352404 2.734700e-01 1.041600e+00
1352405 4.586690e-01 8.958000e-01
1352406 5.744800e-01 7.807000e-01
1352407 7.381600e-01 6.134000e-01
1352408 7.685200e-01 5.849000e-01
1352409 8.700570e-01 4.877000e-01
1352410 1.000000e+00 3.569000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 7
*-----1-----1-----1-----1-----1-----1-----
1352500 2 7
1352501 -1.000000e+00 -1.000000e+00
1352502 -3.000000e-01 -9.000000e-01
1352503 -1.000000e-01 -5.000000e-01
1352504 0.000000e+00 -4.500000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 8
*-----1-----1-----1-----1-----1-----1-----
1352600 2 8
1352601 -1.000000e+00 -1.000000e+00
1352602 -2.500000e-01 -9.000000e-01
1352603 -8.000000e-02 -8.000000e-01
1352604 0.000000e+00 -6.700000e-01
*****
* two - phase multiplier data from I9-1 test data
*****
* head curve
*-----1-----1-----1-----1-----1-----1-----
1353000 0

```

1353001	0.000000e+00	0.000000e+00
1353002	2.000000e-02	2.000000e-02
1353003	6.000000e-02	5.000000e-02
1353004	1.000000e-01	1.000000e-01
1353005	2.000000e-01	4.600000e-01
1353006	2.400000e-01	8.000000e-01
1353007	3.000000e-01	9.600000e-01
1353008	4.000000e-01	9.800000e-01
1353009	6.000000e-01	9.700000e-01
1353010	8.000000e-01	9.000000e-01
1353011	9.000000e-01	8.000000e-01
1353012	9.600000e-01	5.000000e-01
1353013	1.000000e+00	0.000000e+00
* torque curve		
1353100	0	
1353101	0.000000e+00	0.000000e+00
1353102	1.250000e-01	7.000000e-02
1353103	1.650000e-01	1.250000e-01
1353104	2.400000e-01	5.600000e-01
1353105	8.000000e-01	5.600000e-01
1353106	9.600000e-01	4.500000e-01
1353107	1.000000e+00	0.000000e+00
*****		
* pump 2-phase difference data		
*****		
* head curve no. 1		
1354100	1	1
1354101	0.000000e+00	0.000000e+00
1354102	1.000000e-01	8.300000e-01
1354103	2.000000e-01	1.090000e+00
1354104	5.000000e-01	1.020000e+00
1354105	7.000000e-01	1.010000e+00
1354106	9.000000e-01	9.400000e-01
1354107	1.000000e+00	1.000000e+00
* head curve no. 2		
1354200	1	2
1354201	0.000000e+00	0.000000e+00
1354202	1.000000e-01	-4.000000e-02
1354203	2.000000e-01	0.000000e+00
1354204	3.000000e-01	1.000000e-01
1354205	4.000000e-01	2.100000e-01
1354206	8.000000e-01	6.700000e-01
1354207	9.000000e-01	8.000000e-01
1354208	1.000000e+00	1.000000e+00
* head curve no. 3		
1354300	1	3
1354301	-1.000000e+00	-1.160000e+00
1354302	-9.000000e-01	-1.240000e+00
1354303	-8.000000e-01	-1.770000e+00
1354304	-7.000000e-01	-2.360000e+00
1354305	-6.000000e-01	-2.790000e+00
1354306	-5.000000e-01	-2.910000e+00
1354307	-4.000000e-01	-2.670000e+00

1354308	-2.500000e-01	-1.690000e+00
1354309	-1.000000e-01	-5.000000e-01
1354310	0.000000e+00	0.000000e+00
* head curve no. 4		
1354400	1	4
1354401	-1.000000e+00	-1.160000e+00
1354402	-9.000000e-01	-7.800000e-01
1354403	-8.000000e-01	-5.000000e-01
1354404	-7.000000e-01	-3.100000e-01
1354405	-6.000000e-01	-1.700000e-01
1354406	-5.000000e-01	-8.000000e-02
1354407	-3.500000e-01	0.000000e+00
1354408	-2.000000e-01	5.000000e-02
1354409	-1.000000e-01	8.000000e-02
1354410	0.000000e+00	1.100000e-01
* head curve no. 5		
1354500	1	5
1354501	0.000000e+00	0.000000e+00
1354502	2.000000e-01	-3.400000e-01
1354503	4.000000e-01	-6.500000e-01
1354504	6.000000e-01	-9.300000e-01
1354505	8.000000e-01	-1.190000e+00
1354506	1.000000e+00	-1.470000e+00
* head curve no. 6		
1354600	1	6
1354601	0.000000e+00	1.100000e-01
1354602	1.000000e-01	1.300000e-01
1354603	2.500000e-01	1.500000e-01
1354604	4.000000e-01	1.300000e-01
1354605	5.000000e-01	7.000000e-02
1354606	6.000000e-01	-4.000000e-02
1354607	7.000000e-01	-2.300000e-01
1354608	8.000000e-01	-5.100000e-01
1354609	9.000000e-01	-9.100000e-01
1354610	1.000000e+00	-1.470000e+00
* head curve no. 7		
1354700	1	7
1354701	-1.000000e+00	0.000000e+00
1354702	0.000000e+00	0.000000e+00
* head curve no. 8		
1354800	1	8
1354801	-1.000000e+00	0.000000e+00
1354802	0.000000e+00	0.000000e+00
* torque curve no. 1		
1354900	2	1
1354901	0.000000e+00	6.032000e-01
1354902	1.930000e-01	6.325000e-01
1354903	3.930000e-01	7.369000e-01

```

1354904 5.955200e-01 8.331000e-01
1354905 7.978200e-01 9.229000e-01
1354906 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 2
*-----1-----1-----1-----1-----1-----1-----
1355000 2 2
1355001 0.000000e+00 -6.700000e-01
1355002 4.000000e-01 -2.500000e-01
1355003 5.000000e-01 1.500000e-01
1355004 7.372550e-01 5.265860e-01
1355005 7.680490e-01 6.065940e-01
1355006 8.672300e-01 7.436600e-01
1355007 1.000000e+00 1.000000e+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 3
*-----1-----1-----1-----1-----1-----1-----
1355100 2 3
1355101 -1.000000e+00 1.984300e+00
1355102 -8.009600e-01 1.394000e+00
1355103 -6.063800e-01 1.097500e+00
1355104 -4.068600e-01 8.220000e-01
1355105 -1.992800e-01 6.648000e-01
1355106 0.000000e+00 6.032000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 4
*-----1-----1-----1-----1-----1-----1-----
1355200 2 4
1355201 -1.000000e+00 1.984300e+00
1355202 -8.223400e-01 1.830800e+00
1355203 -6.337100e-01 1.682400e+00
1355204 -4.585300e-01 1.557000e+00
1355205 -2.670230e-01 1.436200e+00
1355206 -1.761070e-01 1.387900e+00
1355207 -8.931000e-02 1.348100e+00
1355208 0.000000e+00 1.233610e+00
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 5
*-----1-----1-----1-----1-----1-----1-----
1355300 2 5
1355301 0.000000e+00 -4.500000e-01
1355302 4.000000e-01 -2.500000e-01
1355303 5.000000e-01 0.000000e+00
1355304 1.000000e+00 3.569000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 6
*-----1-----1-----1-----1-----1-----1-----
1355400 2 6
1355401 0.000000e+00 1.233610e+00
1355402 9.064300e-02 1.196500e+00
1355403 1.885690e-01 1.109600e+00
1355404 2.734700e-01 1.041600e+00
1355405 4.586690e-01 8.958000e-01
1355406 5.744800e-01 7.807000e-01
1355407 7.381600e-01 6.134000e-01
1355408 7.685200e-01 5.849000e-01
1355409 8.700570e-01 4.877000e-01
1355410 1.000000e+00 3.569000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 7

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*-----1-----1-----1-----1-----1-----1-----
1355500 2 7
1355501 -1.000000e+00 -1.000000e+00
1355502 -3.000000e-01 -9.000000e-01
1355503 -1.000000e-01 -5.000000e-01
1355504 0.000000e+00 -4.500000e-01
*-----1-----1-----1-----1-----1-----1-----
* torque curve no. 8
*-----1-----1-----1-----1-----1-----1-----
1355600 2 8
1355601 -1.000000e+00 -1.000000e+00
1355602 -2.500000e-01 -9.000000e-01
1355603 -8.000000e-02 -8.000000e-01
1355604 0.000000e+00 -6.700000e-01
*****
* pcp1 pump velocity table
*****
*1356100 536
*1356101 0.0 0.0
*1356102 1.0 220.
*****
* pump 1 outlet pump side
*****
1400000 pmp1outp sngivol
1400101 0.0366 0.502 0.0 0.0 0.0 0.0
1400102 4.0e-5 0.0 00000
1400200 0 15165000. 1242900. 2458470. 0.0
*****
* pump1 outlet pipe tee side
*****
1450000 pmp1outt branch
1450001 2 0
1450101 0.0 1.4084 0.0633 0.0 0.0 0.0
1450102 4.0e-5 0.0 00000
1450200 0 15069300. 1242900. 2458230.0 0.0
1451101 140010000 145000000 0.0 0.1 0.1 000100
1452101 145010000 150000000 0.0 0.0 0.0 000100
1451201 8.8901000 8.6110000 0.0
1452201 10.611000 10.694000 0.0
*****
* pump outlet tee
*****
1500000 pmpoutt branch
1500001 3 0
1500101 0.0634 0.4966 0.0 0.0 0.0 0.0
1500102 4.0e-5 0.0 00000
1500200 0 15048800. 1242900. 2458680.0 0.0
1501101 170010000 150000000 0.0183 0.2 0.2 000100
1502101 150010000 175000000 0.0 0.1 0.1 000100
1503101 150010000 406000000 0.0 0.0 0.0 000100
1501201 4.3528000 5.2611000 0.0
1502201 10.035000 10.103000 0.0
1503201 .08890000 0.2735000 0.0
*****
* pump 2 suction tee outlet
*****
1550000 pmp2sctt branch
1550001 1 0
1550101 0.0 1.003 0.0613 0.0 90.0 0.521
1550102 4.0e-5 0.0 00000

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1550200 0 14601200. 1242600. 2468430.0 0.0
1551101 155010000 160000000 0.0 0.1 0.1 000100
1551201 7.5199000 7.8923000 0.0
*****
* pump 2 inlet pipe
*****
1600000 pmp2inet snglvol
1600101 0.0 0.457 0.0189 0.0 90.0 0.457
1600102 4.0e-5 0.0 00000
1600200 0 14580700. 1242600. 2468050.0 0.0
*****
* primary coolant pump 2
*****
1650000 pcpump2 pump
1650101 0.0366 0.0 0.099 0.0 90.0 0.319
1650102 00000
1650108 160010000 0.0 0.0 0.0 000100
1650109 170000000 0.0 0.1 0.1 000100
1650200 0 14832700. 1242890. 2463590.0 0.0
1650201 0 8.4974000 8.8872000 0.0
1650202 0 8.4959000 6.6507000 0.0
1650301 135 135 135 -1 -1 504 0
1650302 369.00 .89699187 .315500 96.00 500.600 1.431
1650303 613.6 0.0 207.433 0.004 19.5980 0.0
1650310 0.0 0.0 0.0
*****
* pump 2 outlet
*****
1700000 pmp2outt branch
1700001 1 0
1700101 0.0366 0.514 0.0 0.0 0.0 0.0
1700102 4.0e-5 0.0 00000
1700200 0 15089900. 1242900. 2457860.0 0.0
1701101 145010000 170010000 0.0183 0.2 0.2 000100
1701201 -4.140400 -4.242200 0.0
*****
* cold leg pipe to ecc connection tee
*****
1750000 ilcpipe pipe
1750001 2
1750101 0.0634 2
1750201 0.0 1
1750301 0.559 1
1750302 0.613 2
1750401 0.0 2
1750501 0.0 2
1750601 0.0 2
1750701 0.0 2
1750801 4.0e-5 0.0 2
1750901 0.15 0.15 1
1751001 00000 2
1751101 000100 1
1751201 0 15044100. 1242900. 2458830.0 0.0 0.0 01
1751202 0 15037400. 1242900. 2458990.0 0.0 0.0 02
1751300 0
1751301 10.035000 10.106000 0.0 01
*****
* ecc connection tee pump side
*****
1800000 ecc branch

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1800001 1 0
1800101 0.0634 1.152 0.0 0.0 0.0 0.0
1800102 4.0e-5 0.0 00000
1800200 0 15034000. 1242910. 2259090.0 0.0
1801101 175010000 180000000 0.0 0.05 0.05 000100
1801201 10.035000 10.083000 0.0
*****
* cold leg pipe from ecc connection to reactor vessel
*****
1850000 rvnoid branch
1850001 3 0
1850101 0.0634 1.01 0.0 0.0 0.0 0.0
1850102 4.0e-5 0.0 00000
1850200 0 15032100. 1242910. 2459140.0 0.0
1851101 185010000 205000000 0.0634 1.0 1.0 000100
1852101 180010000 185000000 0.0 0.0 0.0 000100
1853101 185010000 223000000 0.0 45.0 45.0 000100
1851201 9.2743000 9.3795000 0.0
1852201 10.035000 10.064000 0.0
1853201 1.6570000 1.7271000 0.0
*****
* reactor vessel
*
* ---1---1---1---1---1---1---
* inlet annulus top volume
* ---1---1---1---1---1---1---
2000000 inantop branch
2000001 2 0
2000101 0.0 0.33 0.0855 0.0 90.0 0.33
2000102 4.0e-5 0.178 00000
2000200 0 15017400. 1243540. 2459500.0 0.0
2001101 200000000 205000000 0.0 0.0 0.0 000100
2002101 200000000 245010000 0.001 1800. 1800.
000100
2001201 -.0306700 -.03023076 .0
2002201 .06975000 .07019300 0.0
* ---1---1---1---1---1---1---
* inlet annulus bottom volume
* ---1---1---1---1---1---1---
2050000 inanbot branch
2050001 1 0
2050101 0.0 0.424 0.11 0.0 -90.0 -0.424
2050102 4.0e-5 0.172 00000
2050200 0 15018400. 1242920. 2459460.0 0.0
2051101 205010000 210000000 0.0 0.0 0.0 000100
2051201 4.0266000 4.3312000 0.0
* ---1---1---1---1---1---1---
* downcomer
* ---1---1---1---1---1---1---
2100000 downcomr annulus
2100001 4
2100101 0.142 4
2100201 0.0 3
2100301 0.958 4
2100401 0.0 4
2100501 0.0 4
2100601 -90.0 4
2100801 4.0e-5 0.102 4
2100901 0.0 0.0 3

```





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2351202 0 15002400.1242980. 2459850.0 0.0 0.0 02
2351203 0 14981700.1243020. 2460330.0 0.0 0.0 03
2351300 0
2351301 2.2307000 2.3978000 0.0 01
2351302 2.2307000 2.3980000 0.0 02
*-----1-----1-----1-----1-----1-----1-----
* upper core support structure
*-----1-----1-----1-----1-----1-----1-----
2400000 ucosst branch
2400001 2 0
2400101 0.297 1.118 0.0 0.0 90.0 1.118
2400102 4.0e-5 0.145 00000
2400200 0 14966500.1348980. 2460680.0 0.0
2401101 230010000 240000000 0.12 0.3 0.3 000100
2402101 235010000 240000000 0.0 0.0 0.0 000100
2401201 3.6456000 3.6509000 0.0
2402201 2.3080000 2.3981000 0.0
*-----1-----1-----1-----1-----1-----1-----
* upper flow skirt region
*-----1-----1-----1-----1-----1-----1-----
2450000 ufosre branch
2450001 1 0
2450101 0.114 0.843 0.0 0.0 90.0 0.843
2450102 4.0e-5 0.131 00000
2450200 0 14945200.1347660. 2461140.0 0.0
2451101 240010000 245000000 0.0 0.0 0.0 000100
2451201 5.7436 6.0742 0.0
*-----1-----1-----1-----1-----1-----1-----
* dead end of fuel modules
*-----1-----1-----1-----1-----1-----1-----
2460000 fumodu branch
2460001 1 0
2460101 0.183 0.7 0.0 0.0 90.0 0.7
2460102 4.0e-5 0.214 00000
2460200 0 14961800.1343000. 2460790.0 0.0
2461101 240010000 246000000 0.0 0.0 0.0 000100
2461201 -.74932e-5 -.74932e-5 0.0
*-----1-----1-----1-----1-----1-----1-----
* upper plenum lower volume
*-----1-----1-----1-----1-----1-----1-----
2500000 uplvol branch
2500001 1 0
2500101 0.268 1.566 0.0 0.0 90.0 1.566
2500102 4.0e-5 0.0 00000
2500200 0 14947600.1346300. 2461140.0 0.0
2501101 245010000 250000000 0.0 0.0 0.0 000100
2501201 5.8130000 6.1784000 0.0
*****
*
* broken loop
*
*****
* reactor vessel nozzle - broken loop hot leg
*-----1-----1-----1-----1-----1-----1-----
3000000 rvblhl branch
3000001 2 0
3000101 0.0634 0.876 0.0 0.0 0.0 0.0
3000102 4.0e-5 0.0 00000
3000200 0 14953100.1239820. 2460990.0 0.0
3001101 250000000 300000000 0.0634 0.0 0.0 000100

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```

3002101 300010000 305000000 0.0 0.1 0.1 000000
3001201 -.1303100 -.1795200 0.0
3002201 -.1303200 -.1304000 0.0
*-----1-----1-----1-----1-----1-----1-----
* hot leg pipe to reflood assist bypass tee
*-----1-----1-----1-----1-----1-----1-----
3050000 hlpras branch
3050001 1 0
3050101 0.0634 0.698 0.0 0.0 0.0 0.0
3050102 4.0e-5 0.0 00000
3050200 0 14953100.1239750. 2460990.0 0.0
3051101 305010000 310000000 0.0 0.1 0.1 000100
3051201 -.1761300 -.1768800 0.0
*-----1-----1-----1-----1-----1-----1-----
* broken loop hot leg contraction
*-----1-----1-----1-----1-----1-----1-----
3100000 sgsl branch
3100001 2 0
3100101 0.0 1.424 0.0668 0.0 0.0 0.0
3100102 4.0e-5 0.0 00000
3100200 0 14953100.1239700. 2460990.0 0.0
3101101 370010000 310000000 0.0 0.0 0.0 000100
3102101 310010000 315000000 0.0 0.0 0.0 000100
3101201 .21294000 .26136000 0.0
3102201 .00000000 .00320000 0.0
*-----1-----1-----1-----1-----1-----1-----
* steam generator and pump simulator
*-----1-----1-----1-----1-----1-----1-----
3150000 sgpsi pipe
3150001 12
3150101 0.00836 2
3150102 0.108 8
3150103 0.0 10
3150104 0.00836 11
3150105 0.0525 12
3150201 0.0 2
3150202 0.0326 4
3150203 0.108 5
3150204 0.0326 7
3150205 0.0 8
3150206 0.0 9
3150207 0.0081 10
3150208 0.0 11
3150301 0.4054 1
3150302 0.5265 2
3150303 0.362 3
3150304 1.692 4
3150305 0.8495 6
3150306 1.692 7
3150307 0.362 8
3150308 1.346 9
3150309 1.325 10
3150310 1.842 11
3150311 0.667 12
3150401 0.0 8
3150402 0.0162 9
3150403 0.0648 10
3150404 0.0 12
3150601 90.0 5
3150602 -90.0 10

```



```

3500201 0.0 1 * break plane
3500301 0.488 1
3500302 1.6085 2
3500401 0.00541 1
3500402 0.07770 2
3500601 0.0 2
3500801 4.0e-5 0.0 1
3500802 4.0e-5 0.0 2
3500901 0.0 0.0 1
3501001 00000 2
3501101 000100 1
3501201 0 15018600.1067100. 2459470.0 0.0 0.0 01
3501202 0 15018600.1173730. 2459470.0 0.0 0.0 02
3501300 0
3501301 .0 .0 0.0 01
*-----1-----1-----1-----1-----1-----1-----
* isolation valve cold leg
*-----1-----1-----1-----1-----1-----1-----
3550000 isvd valve
3550101 350010000 360000000 0.0 0.0 0.0 000100
3550201 1 0.0 0.0 0.0
3550300 trpvlv
3550301 505
*-----1-----1-----1-----1-----1-----1-----
* pipe section between isolation valve and qobv cold leg
*-----1-----1-----1-----1-----1-----1-----
3600000 vvcld snglvcl
3600101 0.0525 0.813 0.0 0.0 0.0 0.0
3600102 4.0e-5 0.0 00000
3600200 3 14.74e6 558.
*-----1-----1-----1-----1-----1-----1-----
* quick opening blowdown cold leg
*-----1-----1-----1-----1-----1-----1-----
3650000 qobvcl valve
3650101 360010000 805000000 0.0466 0.0 0.0 000100
3650201 1 0.0 0.0 0.0
3650300 trpvlv
3650301 507
*-----1-----1-----1-----1-----1-----1-----
* reflood assist bypass piping - cold leg side
*-----1-----1-----1-----1-----1-----1-----
3700000 rabsphl branch
3700001 1 0
3700101 0.0388 2.203 0.0 0.0 90.0 0.653
3700102 4.0e-5 0.0 00000
3700200 0 14755500.1239680.0 2460930.0 0.0
3701101 375010000 370000000 0.0 0.0 0.0 000100
3701201 .21294000.24585000 0.0
*-----1-----1-----1-----1-----1-----1-----
* reflood assist bypass parrel pipes hot leg side
*-----1-----1-----1-----1-----1-----1-----
3750000 rabphl snglvcl
3750101 0.0776 0.0 0.0858 0.0 0.0 0.0
3750102 4.0e-5 0.0 00000
3750200 0 14957900.1239760.0 2460880.0 0.0
*-----1-----1-----1-----1-----1-----1-----
* reflood assist bypass valves
*-----1-----1-----1-----1-----1-----1-----
3770000 rabsvly sngljun

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```

3770101 380010000 375000000 0.0 1.4e+4 1.4e+4
000000
3770201 0 .106460 .25646 0.0
*-----1-----1-----1-----1-----1-----1-----
* reflood assist bypass parrel pipes cold leg side
*-----1-----1-----1-----1-----1-----1-----
3800000 rabppcl snglvcl
3800101 0.0776 0.0 0.0855 0.0 0.0 0.0
3800102 4.0e-5 0.0 00000
3800200 0 15023400.1240020.0 2459350.0 0.0
*-----1-----1-----1-----1-----1-----1-----
* reflood assist bypass single pipe cold leg side
*-----1-----1-----1-----1-----1-----1-----
3850000 rabspcl branch
3850001 1 0
3850101 0.0388 0.0 0.11802 0.0 -90.0 -0.653
3850102 4.0e-5 0.0 00000
3850200 0 15021000.1240850.0 2459410.0 0.0
3851101 385010000 380000000 0.0 0.0 0.0 000100
3851201 .212920 .260740 0.0
*****
*
* pressurizer
*
*****
* surge line pcs side
*-----1-----1-----1-----1-----1-----1-----
4000000 sipcs branch
4000001 2 0
4000101 0.00145 3.45 0.0 0.0 90.0 0.54
4000102 4.0e-5 0.0 00000
4000200 0 14923700.1458370. 2461610.0 0.0
4001101 110000000 400000000 0.00145 0.93 0.93
100100
4001101 0. 0. 1. 1.
4002101 400010000 405000000 0.0 0.93 0.93 000000
4001201 -.17675e-4 -.17772e-4 0.0
4002201 -.17696e-5 -.17696e-5 0.0
*-----1-----1-----1-----1-----1-----1-----
* surge line pressurizer vessel
*-----1-----1-----1-----1-----1-----1-----
4050000 sprv snglvcl
4050101 0.00145 3.45 0.0 0.0 90.0 0.60
4050102 4.0e-5 0.0 00000
4050200 0 14920000.1494210.0 2461690.0 0.0
*-----1-----1-----1-----1-----1-----1-----
* spray line
*-----1-----1-----1-----1-----1-----1-----
4060000 spray branch
4060001 1 0
4060101 0.0003363 6.322 0.0 0.0 90.0
4060102 3.161 4.0e-5 0.0 00000
4060200 0 15075000.1244040.0 2458090.0 0.0
4061101 406010000 420010000 2.40e-6 1.039242 1.039242
000100
4061201 .08890000 .08890000 0.0
*-----1-----1-----1-----1-----1-----1-----
* spray valve
*-----1-----1-----1-----1-----1-----1-----
*4070000 sprvly valve

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```

11152100 0 1
11152101 19 0.623795
11152201 5 19
11152301 0.0 19
11152401 577.0 20
11152501 115030000 0 1 1 0.1579621 1
11152502 115160000 0 1 1 0.1579621 2
11152601 515030000 0 1 1 0.1579621 2
11152701 0 0.0 0.0 0.0 2
11152801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
11152901 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
*****
* intact loop piping
*****
11001000 12 11 2 1 0.142
11001100 0 1
11001101 10 0.1780
11001201 4 10
11001301 0.0 10
11001401 540.0 11
11001501 100010000 0 1 1 1.5373 1
11001502 105010000 0 1 1 1.634 2
11001503 110010000 0 1 1 0.623 3
11001504 115010000 0 1 1 1.4385 4
11001505 115180000 0 1 1 0.689 5
11001506 115190000 0 1 1 0.559 6
11001507 120010000 0 1 1 0.76 7
11001508 150010000 0 1 1 0.4966 8
11001509 175010000 0 1 1 0.559 9
11001510 175020000 0 1 1 0.613 10
11001511 180010000 0 1 1 0.701 11
11001512 185010000 0 1 1 1.461 12
11001601 -939 0 3949 1 1.5373 1
11001602 -939 0 3949 1 1.634 2
11001603 -939 0 3949 1 0.623 3
11001604 -939 0 3949 1 1.4385 4
11001605 -939 0 3949 1 0.689 5
11001606 -939 0 3949 1 0.559 6
11001607 -939 0 3949 1 0.76 7
11001608 -939 0 3949 1 0.4966 8
11001609 -939 0 3949 1 0.559 9
11001610 -939 0 3949 1 0.613 10
11001611 -939 0 3949 1 0.701 11
11001612 -939 0 3949 1 1.461 12
11001701 0 0 0 0 12
11001801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
11001802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
11001803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
11001804 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 4 * mod 3
11001805 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 5 * mod 3
11001806 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 6 * mod 3
11001807 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 7 * mod 3
11001808 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 8 * mod 3
11001809 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 9 * mod 3
11001810 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 10 * mod 3
11001811 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 11 * mod 3
11001812 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 12 * mod 3
*-----1-----1-----1-----1-----1-----1-----
* steam generator connections
*-----1-----1-----1-----1-----1-----1-----

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```

11002000 2 11 2 1 0.1625
11002100 0 1
11002101 10 0.203
11002201 4 10
11002301 0.0 10
11002401 540.0 11
11002501 115020000 0 1 1 0.708 1
11002502 115170000 0 1 1 0.547 2
11002601 -939 0 3949 1 0.708 1
11002602 -939 0 3949 1 0.547 2
11002701 0 0 0 0 2
11002801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
11002802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
*-----1-----1-----1-----1-----1-----1-----
* 216 meter diameter piping
*-----1-----1-----1-----1-----1-----1-----
11003000 7 11 2 1 0.108
11003100 0 1
11003101 10 0.1365
11003201 4 10
11003301 0.0 10
11003401 540.0 11
11003501 125010000 0 1 1 1.00 1
11003502 130010000 0 1 1 0.457 2
11003503 140010000 0 1 1 0.502 3
11003504 145010000 0 1 1 1.4084 4
11003505 155010000 0 1 1 1.003 5
11003506 160010000 0 1 1 0.457 6
11003507 170010000 0 1 1 0.514 7
11003601 -939 0 3949 1 1.00 1
11003602 -939 0 3949 1 0.457 2
11003603 -939 0 3949 1 0.502 3
11003604 -939 0 3949 1 1.4084 4
11003605 -939 0 3949 1 1.003 5
11003606 -939 0 3949 1 0.457 6
11003607 -939 0 3949 1 0.514 7
11003701 0 0 0 0 7
11003801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
11003802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
11003803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
11003804 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 4 * mod 3
11003805 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 5 * mod 3
11003806 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 6 * mod 3
11003807 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 7 * mod 3
*-----1-----1-----1-----1-----1-----1-----
* steam generator plena
*-----1-----1-----1-----1-----1-----1-----
11004000 2 11 3 1 0.6858
11004100 0 1
11004101 10 0.7747
11004201 5 10
11004301 0.0 10
11004401 540.0 11
11004501 115030000 0 1 1 0.25 1
11004502 115160000 0 1 1 0.25 2
11004601 -939 0 3949 1 0.25 1
11004602 -939 0 3949 1 0.25 2
11004701 0 0 0 0 2
11004801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
11004802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3

```

```

11004901 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
*****
* reactor vessel heat structures
*****
* the reactor vessel wall is not modelled above the nozzles.
* the vessel to filler gap is assumed to insulate the vessel
* from the fillers. the vessel to filler gap is not modelled
* at this elevation.
* filler blocks inlet annulus top volume
* station 264 to 277
*****
12000000 1 21 2 1 0.508
12000100 0 1
12000101 20 0.7264
12000201 4 20
12000301 0.0 20
12000401 558.0 21
12000501 200010000 0 1 1 0.33 1
12000601 0 0 0 1 0.33 1
12000701 0 0.0 0.0 0.0 1
12000801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* core support barrel
* station 96.44 to 277
*****
12001000 6 11 2 1 0.381
12001100 0 1
12001101 10 0.419
12001201 4 10
12001301 0.0 10
12001401 558.0 11
12001501 0 0 0 1 0.33 1
12001502 0 0 0 1 0.424 2
12001503 0 0 0 1 0.958 3
12001504 0 0 0 1 0.958 4
12001505 0 0 0 1 0.958 5
12001506 0 0 0 1 0.958 6
12001601 200010000 0 1 1 0.33 1
12001602 205010000 0 1 1 0.424 2
12001603 210010000 0 1 1 0.958 3
12001604 210020000 0 1 1 0.958 4
12001605 210030000 0 1 1 0.958 5
12001606 210040000 0 1 1 0.958 6
12001701 0 0.0 0.0 0.0 6
12001901 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
12001902 0.0 11.0 11.0 0.0 0.0 0.0 1.0 2 * mod 3
12001903 0.0 11.0 11.0 0.0 0.0 0.0 1.0 6 * mod 3
*****
* filler blocks inlet annulus lower volume
* station 247.3 to 264.0
*****
12050000 1 21 2 1 0.501
12050100 0 1
12050101 20 0.7264
12050201 4 20
12050301 0.0 20
12050401 558.0 21
12050501 205010000 0 1 1 0.424 1
12050601 223010000 0 1 1 0.424 1
12050701 0 0.0 0.0 0.0 1

```

```

12050801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
12050901 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* downcomer and lower plenum
* station 67.7 to 247.3
*****
12100000 6 21 2 1 0.47
12100100 0 1
12100101 20 0.7264
12100201 4 20
12100301 0.0 20
12100401 558.0 21
12100501 210010000 10000 1 1 0.958 4
12100505 215010000 0 1 1 0.36 5
12100506 220010000 0 1 1 0.37 6
12100601 223020000 0 1 1 0.958 1
12100602 223030000 0 1 1 0.958 2
12100603 223040000 0 1 1 0.958 3
12100604 223050000 0 1 1 0.958 4
12100605 223060000 0 1 1 0.36 5
12100606 223070000 0 1 1 0.37 6
12100701 0 0.0 0.0 0.0 6
12100801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 4 * mod 3
12100802 0.0 11.0 11.0 0.0 0.0 0.0 1.0 5 * mod 3
12100803 0.0 11.0 11.0 0.0 0.0 0.0 1.0 6 * mod 3
12100901 0.0 11.0 11.0 0.0 0.0 0.0 1.0 4 * mod 3
12100902 0.0 11.0 11.0 0.0 0.0 0.0 1.0 5 * mod 3
12100903 0.0 11.0 11.0 0.0 0.0 0.0 1.0 6 * mod 3
*****
* reactor vessel wall above station 178 - 5.50 inches thick
* station 178 to 258 rv not modelled above bottom of nozzles
*****
12110000 3 11 2 1 0.7328
12110100 0 1
12110101 10 0.8725
12110201 5 10
12110301 0.0 10
12110401 558.0 11
12110501 223010000 0 1 1 0.424 1
12110502 223020000 0 1 1 0.958 2
12110503 223030000 0 1 1 0.6500 3
12110601 -939 0 3949 1 0.424 1
12110602 -939 0 3949 1 0.958 2
12110603 -939 0 3949 1 0.6500 3
12110701 0 0.0 0.0 0.0 3
12110801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
12110802 0.0 11.0 11.0 0.0 0.0 0.0 1.0 2 * mod 3
12110803 0.0 11.0 11.0 0.0 0.0 0.0 1.0 3 * mod 3
*****
* reactor vessel wall below station 178 - 3.62 inches thick
* station 67.7 to 178
*****
12120000 5 7 2 1 0.7328
12120100 0 1
12120101 6 0.8247
12120201 5 6
12120301 0.0 6
12120401 558.0 7
12120501 223030000 0 1 1 0.308 1
12120502 223040000 10000 1 1 0.958 3

```

```

12120503 223060000 0 1 1 0.3600 4
12120504 223070000 0 1 1 0.37 5
12120601 -939 0 3949 1 0.308 1
12120602 -939 0 3949 1 0.958 3
12120603 -939 0 3949 1 0.36 4
12120604 -939 0 3949 1 0.37 5
12120701 0 0.0 0.0 0.0 0.0 5
12120801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
12120802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
12120803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 4 * mod 3
12120804 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 5 * mod 3

```

\* reactor vessel bottom station 67.7

```

12200000 1 11 1 1 0.0
12200100 0 1
12200101 10 0.092
12200201 5 10
12200301 0.0 10
12200401 558.0 11
12200501 220010000 0 1 0 1.68 1
12200601 -939 0 3949 0 1.68 1
12200701 0 0.0 0.0 0.0 1
12200801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
12200901 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3

```

\* flow skirt - core filler assembly station 96.44 to 261.13

```

12250000 7 11 2 1 0.3
12250100 0 1
12250101 10 0.38
12250201 4 10
12250301 0.0 10
12250401 558.0 11
12250501 225010000 0 1 1 0.52 1
12250502 230010000 0 1 1 0.559 2
12250503 230020000 0 1 1 0.559 3
12250504 230030000 0 1 1 0.657 4
12250505 240010000 0 1 1 1.118 5
12250506 245010000 0 1 1 0.42 6
12250507 246010000 0 1 1 0.35 7
12250601 0 0 0 1 0.52 1
12250602 0 0 0 1 0.559 2
12250603 0 0 0 1 0.559 3
12250604 0 0 0 1 0.657 4
12250605 0 0 0 1 1.118 5
12250606 0 0 0 1 0.42 6
12250607 0 0 0 1 0.35 7
12250701 0 0.0 0.0 0.0 7
12250801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
12250802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
12250803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 4 * mod 3
12250804 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 5 * mod 3
12250805 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 6 * mod 3
12250806 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 7 * mod 3

```

\* lower core support structure station 96.44 to 116.91

\* includes core support barrel lip, lower core support structure, and fuel module lower end boxes

```

12260000 1 7 2 1 0.282
12260100 0 1
12260101 6 0.3
12260201 4 6
12260301 0.0 6
12260401 558.0 7
12260501 225010000 0 1 1 0.52 1
12260601 0 0 0 1 0.52 1
12260701 0 0.0 0.0 0.0 1
12260801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3

```

\* active core station 116.91 to 182.94

```

12300000 3 10 2 1 0.0
12300100 0 1
12300101 5 4.647e-3
12300102 1 4.742e-3
12300103 3 5.359e-3
12300201 1 5
12300202 2 6
12300203 3 9
12300301 1.0 5
12300302 0.0 9
12300401 558.0 10
12300501 0 0 0 1 725.1 3
12300601 230010000 0 1 1 725.1 1
12300602 230020000 0 1 1 725.1 2
12300603 230030000 0 1 1 725.1 3
12300701 1000 0.41209 0.0 0.0 1
12300702 1000 0.44565 0.0 0.0 2
12300703 1000 0.14226 0.0 0.0 3
12300901 0.0124 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3

```

\* upper core support structure station 190.5 to 234.5

```

12400000 1 7 2 1 0.282
12400100 0 1
12400101 6 0.31
12400201 4 6
12400301 0.0 6
12400401 558.0 7
12400501 240010000 0 1 1 1.118 1
12400601 0 0 0 1 1.118 1
12400701 0 0.0 0.0 0.0 1
12400801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3

```

\* fuel modules station 187.6 to 258.4

```

12460000 1 5 1 1 0.0
12460100 0 1
12460101 4 0.01
12460201 4 4
12460301 0.0 4
12460401 558.0 5
12460501 245010000 0 1 1 1.8 1
12460601 246010000 0 1 1 1.8 1
12460701 0 0.0 0.0 1.8 1
12460801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
12460901 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3

```

```

*****
* core support barrel - upper plenum lower volume
* station 264 to 297.6
* reactor vessel not modelled above bottom of nozzles
* the vessel to filler gap is assumed to insulate the vessel
* from the fillers, the vessel to filler gap is not modelled
* at this elevation.
*****
1250000 1 11 2 1 0.381
12500100 0 1
12500101 10 0.419
12500201 5 10
12500301 0.0 10
12500401 558.0 11
12500501 250010000 0 1 1 0.854 1
12500601 0 0 0 1 0.854 1
12500701 0 0.0 0.0 0.0 1
12500801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* internals upper plenum
*****
12510000 2 5 1 1 0.0
12510100 0 1
12510101 4 0.005
12510201 4 4
12510301 0.0 4
12510401 558.0 5
12510501 250010000 0 1 1 1.0 1
12510502 250010000 0 1 1 1.0 2
12510601 0 0 0 1 1.0 2
12510701 0 0.0 0.0 0.0 2
12510801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
*****
* core support barrel - upper plenum top volume
* station 297.6 to 325
* reactor vessel not modelled above bottom of nozzles
* the vessel to filler gap is assumed to insulate the vessel
* from the fillers, the vessel to filler gap is not modelled
* at this elevation.
*****
12501000 1 21 2 1 0.381
12501100 0 1
12501101 20 0.728
12501201 5 20
12501301 0.0 20
12501401 558.0 21
12501501 250010000 0 1 1 0.712 1
12501601 0 0 0 1 0.712 1
12501701 0 0.0 0.0 0.0 1
12501801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* upper head top plate station 325
*****
12550000 1 21 1 1 0.0
12550100 0 1
12550101 20 0.474
12550201 5 20
12550301 0.0 20
12550401 558.0 21
12550501 250010000 0 1 1 0.712 1

```

```

12550601 -939 0 3949 1 0.712 1
12550701 0 0.0 0.0 0.0 1
12550801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* broken loop hot leg piping heat structures
*****
13150000 2 11 2 1 0.0515
13150100 0 1
13150101 10 0.0705
13150201 4 10
13150301 0.0 10
13150401 540.0 11
13150501 315010000 0 1 1 0.4054 1
13150502 315020000 0 1 1 0.5265 2
13150601 -939 0 3979 1 0.4054 1
13150602 -939 0 3979 1 0.5265 2
13150701 0 0 0 0 2
13150801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
13150802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
*****
13151000 1 11 2 1 0.0550
13151100 0 1
13151101 10 0.0705
13151201 4 10
13151301 0.0 10
13151401 540.0 11
13151501 315090000 0 1 1 0.0120357 1
13151601 -939 0 3979 1 0.0120357 1
13151701 0 0 0 0 1
13151801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
13152000 1 11 2 1 0.0660
13152100 0 1
13152101 10 0.0840
13152201 4 10
13152301 0.0 10
13152401 540.0 11
13152501 315110000 0 1 1 0.00836 1
13152601 -939 0 3979 1 0.00836 1
13152701 0 0 0 0 1
13152801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
13153000 6 11 2 1 0.1835
13153100 0 1
13153101 10 0.2285
13153201 4 10
13153301 0.0 10
13153401 540.0 11
13153501 315030000 10000 1 1 0.108 6
13153601 -939 0 3979 1 0.108 6
13153701 0 0 0 0 6
13153801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 6 * mod 3
*****
13154000 1 11 2 1 0.1285
13154100 0 1
13154101 10 0.1620
13154201 4 10
13154301 0.0 10
13154401 540.0 11
13154501 315120000 0 1 1 0.0525 1

```

```

13154601 -939 0 3979 1 0.0525 1
13154701 0 0 0 0 1
13154801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
13155000 1 11 2 1 0.1420
13155100 0 1
13155101 10 0.1780
13155201 4 10
13155301 0.0 10
13155401 540.0 11
13155501 315100000 0 1 1 0.0489057 1
13155601 -939 0 3979 1 0.0489057 1
13155701 0 0 0 0 1
13155801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* nozzle piping
*****
13000000 3 11 2 1 0.1420
13000100 0 1
13000101 10 0.1780
13000201 4 10
13000301 0.0 10
13000401 540.0 11
13000501 300010000 0 1 1 0.876 1
13000502 305010000 0 1 1 0.698 2
13000503 310010000 0 1 1 1.424 3
13000601 -939 0 3979 1 0.876 1
13000602 -939 0 3979 1 0.698 2
13000603 -939 0 3979 1 1.424 3
13000701 0 0 0 0 3
13000801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
13000802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
13000803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
*****
* broken loop cold leg
*****
* nozzle piping
*****
13350000 3 11 2 1 0.1420
13350100 0 1
13350101 10 0.1780
13350201 4 10
13350301 0.0 10
13350401 540.0 11
13350501 335010000 0 1 1 0.7495 1
13350502 340010000 0 1 1 0.698 2
13350503 345010000 0 1 1 0.974 3
13350601 -939 0 3949 1 0.7495 1
13350602 -939 0 3949 1 0.698 2
13350603 -939 0 3949 1 0.974 3
13350701 0 0 0 0 3
13350801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
13350802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
13350803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
*****
13501000 1 11 2 1 0.0550
13501100 0 1
13501101 10 0.1780
13501201 4 10
13501301 0.0 10

```

```

13501401 540.0 11
13501501 350010000 0 1 1 0.488 1
13501601 -939 0 3949 1 0.488 1
13501701 0 0 0 0 1
13501801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
13502000 1 11 2 1 0.0865
13502100 0 1
13502101 10 0.1095
13502201 4 10
13502301 0.0 10
13502401 540.0 11
13502501 350020000 0 1 1 1.6085 1
13502601 -939 0 3949 1 1.6085 1
13502701 0 0 0 0 1
13502801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* refeed assist piping and valves [rabvs]
*****
13700000 4 11 2 1 0.111
13700100 0 1
13700101 10 0.1365
13700201 4 10
13700301 0.0 10
13700401 540.0 11
13700501 370010000 0 1 1 2.00 1
13700502 375010000 0 1 1 1.10567 2
13700503 380010000 0 1 1 1.101804 3
13700504 385010000 0 1 1 3.04201 4
13700601 -939 0 3979 1 2.00 1
13700602 -939 0 3979 1 1.10567 2
13700603 -939 0 3949 1 1.101804 3
13700604 -939 0 3949 1 3.04201 4
13700701 0 0 0 0 4
13700801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
13700802 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 2 * mod 3
13700803 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 3 * mod 3
13700804 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 4 * mod 3
*****
* pressurizer heat structures
*****
* vessel bottom
*---1---1---1---1---1---1---
14151000 1 11 1 1 0.0
14151100 0 1
14151101 10 0.0762
14151201 5 10
14151301 0.0 10
14151401 617.0 11
14151501 415010000 0 1 1 0.362 1
14151601 -939 0 3969 1 0.362 1
14151701 0 0 0 0 1
14151801 0.0 11.0 11.0 0.0 0.0 0.0 0.0 1.0 1 * mod 3
*---1---1---1---1---1---1---
* vessel sides - large diameter section
*---1---1---1---1---1---1---
14152000 7 11 2 1 0.42291
14152100 0 1
14152101 10 0.49911
14152201 5 10

```

```

14152301 0.0 10
14152401 617.0 11
14152501 415010000 0 1 1 0.224 1
14152502 415020000 10000 1 1 0.403 3
14152503 415040000 10000 1 1 0.207 5
14152504 415060000 10000 1 1 0.1705 7
14152601 -939 0 3969 1 0.224 1
14152602 -939 0 3969 1 0.403 3
14152603 -939 0 3969 1 0.207 5
14152604 -939 0 3969 1 0.1705 7
14152701 0 0 0 0 0 7
14152801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 7 * mod 3
*-----1-----1-----1-----1-----1-----1-----
* vessel sides - small diameter section
*-----1-----1-----1-----1-----1-----1-----
14162000 1 11 2 1 0.2032
14162100 0 1
14162101 10 0.3683
14162201 5 10
14162301 0.0 10
14162401 617.0 11
14162501 415080000 0 1 1 0.118 1
14162601 -939 0 3969 1 0.118 1
14162701 0 0 0 0 0 1
14162801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* pressurizer heaters
*****
14172000 12 9 2 1 0.0
14172100 0 1
14172101 3 4.0132e-3
14172102 2 4.3942e-3
14172103 1 5.6642e-3
14172104 2 8.3820e-3
14172201 7 3
14172202 8 5
14172203 7 6
14172204 4 8
14172301 0.0 3
14172302 1.0 5
14172303 0.0 8
14172401 617.6 9
14172501 0 0 0 1 0.6096 12
14172601 415020000 0 1 1 0.6096 12
14172701 417 1.0 0.0 0.0 9 *cycli
14172702 418 1.0 0.0 0.0 12 *backu
14172901 1.6764e-2 11.0 11.0 0.0 0.0 0.0 1.0 12 *
mod 3
*****
* pressurizer cycling heaters
*-----1-----1-----1-----1-----1-----1-----
* pressurizer backup heaters
*-----1-----1-----1-----1-----1-----1-----
14201000 1 11 2 1 0.2032
14201100 0 1
14201101 10 0.3683
14201201 5 10
14201301 0.0 10
14201401 617. 11
14201501 420010000 0 1 1 0.118 1

```

```

14201601 -939 0 3969 1 0.118 1
14201701 0 0 0 0 0 1
14201801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
14202000 1 11 1 1 0.0
14202100 0 1
14202101 10 0.18415
14202201 5 10
14202301 0.0 10
14202401 617. 11
14202501 420010000 0 1 1 0.13 1
14202601 -939 0 3969 1 0.13 1
14202701 0 0 0 0 0 1
14202801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 1 * mod 3
*****
* steam generator heat structures
*****
* shroud secondary side steam generator - upper section
*-----1-----1-----1-----1-----1-----1-----
15000000 3 4 2 1 0.3048
15000100 0 1
15000101 3 0.314325
15000201 5 3
15000301 0.0 3
15000401 540.0 4
15000501 500010000 0 1 1 0.7725 1
15000502 505010000 0 1 1 0.7725 -2
15000503 510010000 0 1 1 0.152 3
15000601 520010000 0 1 1 0.7725 1
15000602 515110000 0 1 1 0.7725 2
15000603 515100000 0 1 1 0.152 3
15000701 0 0.0 0.0 0.0 0.0 3
15000801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 3 * mod 3
15000901 0.0 11.0 11.0 0.0 0.0 0.0 1.0 3 * mod 3
*-----1-----1-----1-----1-----1-----1-----
* shroud - lower section
*-----1-----1-----1-----1-----1-----1-----
15150000 4 4 2 1 0.6445
15150100 0 1
15150101 3 0.6572
15150201 5 3
15150301 0.0 3
15150401 540.0 4
15150501 510010000 0 1 1 0.152 1
15150502 515010000 10000 1 1 0.7113 4
15150601 515100000 0 1 1 0.152 1
15150602 515090000 0 1 1 0.7113 2
15150603 515080000 0 1 1 0.7113 3
15150604 515060000 0 1 1 0.7113 4
15150701 0 0 0 0 0 4
15150801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 4 * mod 3
15150901 0.0 11.0 11.0 0.0 0.0 0.0 1.0 4 * mod 3
*-----1-----1-----1-----1-----1-----1-----
* vessel wall
*-----1-----1-----1-----1-----1-----1-----
15300000 8 10 2 1 0.7112
15300100 0 1
15300101 9 0.765165
15300201 5 9
15300301 0.0 9
15300401 530.0 10

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15300501 530010000 0 1 1 0.762 1
15300502 525010000 0 1 1 0.762 2
15300503 500010000 0 1 1 0.718 3
15300504 505010000 0 1 1 0.718 4
15300505 510010000 0 1 1 0.518 5
15300506 515010000 10000 1 1 0.7102 8
15300601 -939 0 3959 1 0.762 2
15300602 -939 0 3959 1 0.718 4
15300603 -939 0 3959 1 0.518 5
15300604 -939 0 3959 1 0.7102 8
15300701 0 0.0 0.0 0.0 0.0 8
15300801 0.0 11.0 11.0 0.0 0.0 0.0 1.0 8 * mod 3
*****
*
* heat structure thermal property data
*
*****
*-----1-----1-----1-----1-----1-----1-----
20100100 tbl/fctr 1 1 * uo2
20100200 tbl/fctr 1 1 * gap
20100300 tbl/fctr 1 1 * zr
20100400 tbl/fctr 1 1 * s-steel
20100500 c-steel
20100600 tbl/fctr 1 1 * inconel 600
20100700 tbl/fctr 1 1 * mgo
20100800 tbl/fctr 1 1 * nicr
*-----1-----1-----1-----1-----1-----1-----
* uo2 - thermal conductivity
*-----1-----1-----1-----1-----1-----1-----
20100101 2.7315e2 8.44
20100102 4.1667e2 6.46
20100103 5.3315e2 5.782385
20100104 6.99817e2 4.633177
20100105 8.66483e2 3.880307
20100106 1.03315e3 3.357625
20100107 1.08871e3 3.155129
20100108 1.19982e3 2.983787
20100109 1.28315e3 2.836674
20100110 1.36648e3 2.713792
20100111 1.53315e3 2.521680
20100112 1.61648e3 2.448990
20100113 1.69982e3 2.391875
20100114 1.97759e3 2.289762
20100115 2.25537e3 2.307069
20100116 2.53315e3 2.433413
20100117 2.81093e3 2.661870
20100118 3.08871e3 2.994171
*-----1-----1-----1-----1-----1-----1-----
* gap - thermal conductivity
*-----1-----1-----1-----1-----1-----1-----
20100201 273.15 0.14
20100202 590.0 0.24
20100203 810.0 0.29
20100204 1090.0 0.36
20100205 1370.0 0.42
20100206 3260.0 0.75
*-----1-----1-----1-----1-----1-----1-----
* zircaloy-4 - thermal conductivity from matpro
*-----1-----1-----1-----1-----1-----1-----
20100301 380.4 13.6

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20100302 469.3 14.6
20100303 577.6 15.8
20100304 685.9 17.3
20100305 774.8 18.4
20100306 872.0 19.8
20100307 973.2 21.8
20100308 1073.2 23.2
20100309 1123.2 25.4
20100310 1152.3 24.2
20100311 1232.2 25.5
20100312 1331.2 26.6
20100313 1404.2 28.2
20100314 1576.2 33.0
20100315 1625.2 36.7
20100316 1755.2 41.2
20100317 2273.2 55.0
*-----1-----1-----1-----1-----1-----1-----
* s-steel - thermal conductivity
*-----1-----1-----1-----1-----1-----1-----
20100401 273.15 12.98
20100402 1199.82 25.1
*-----1-----1-----1-----1-----1-----1-----
* inconel-600 - thermal conductivity
*-----1-----1-----1-----1-----1-----1-----
20100601 366.5 13.85
20100602 477.6 15.92
20100603 588.7 18.17
20100604 700.0 20.42
20100605 810.9 22.50
20100606 922.0 24.92
20100607 1033.2 26.83
20100608 1144.3 29.42
20100609 1477.6 36.06
*-----1-----1-----1-----1-----1-----1-----
* uo2 - volumetric heat capacity
*-----1-----1-----1-----1-----1-----1-----
20100151 2.73150e2 2.310427e6
20100152 3.23150e2 2.571985e6
20100153 3.73150e2 2.746357e6
20100154 6.7315e2 3.138694e6
20100155 1.37315e3 3.443844e6
20100156 1.77315e3 3.531030e6
20100157 1.97315e3 3.792588e6
20100158 2.17315e3 4.228518e6
20100159 2.37315e3 4.882412e6
20100160 2.67315e3 6.015829e6
20100161 2.77315e3 6.320980e6
20100162 2.87315e3 6.582538e6
20100163 2.97315e3 6.713317e6
20100164 3.11315e3 6.800503e6
20100165 4.69982e3 6.800503e6
*-----1-----1-----1-----1-----1-----1-----
* gap - volumetric heat capacity
*-----1-----1-----1-----1-----1-----1-----
20100251 273.15 5.4
20100252 3260.0 5.4
*-----1-----1-----1-----1-----1-----1-----
* zircaloy-4 - volumetric heat capacity from matpro
*-----1-----1-----1-----1-----1-----1-----
20100351 255.4 1.904e6

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20100352	1077.6	2.312e6
20100353	1185.9	5.712e6
20100354	1248.4	2.311e6
20100355	2199.8	2.312e6
* ---1---1---1---1---1---1---		
* s-steel - volumetric heat capacity		
* ---1---1---1---1---1---1---		
20100451	273.15	3.83e6
20100452	366.5	3.83e6
20100453	1366.5	5.376e6
* ---1---1---1---1---1---1---		
* inconel-600 - volumetric heat capacity		
* ---1---1---1---1---1---1---		
20100651	366.5	3.908+6
20100652	477.6	4.084+6
20100653	588.7	4.260+6
20100654	700.0	4.436+6
20100656	810.9	4.665+6
20100657	922.0	4.929+6
20100658	1033.2	5.105+6
20100659	1477.6	5.727+6
* ---1---1---1---1---1---1---		
* magnesium oxide - thermal conductivity		
* ---1---1---1---1---1---1---		
20100701	373.15	0.2451
20100702	422.04	0.2405
20100703	477.59	0.2352
20100704	533.15	0.2300
20100705	588.71	0.2249
20100706	644.26	0.2196
20100707	699.82	0.2143
20100708	755.37	0.2091
20100709	810.93	0.2039
20100710	866.48	0.1987
20100711	922.04	0.1934
20100712	977.59	0.1882
20100713	1033.15	0.1830
20100714	1088.71	0.1777
20100715	1144.26	0.1725
20100716	1199.82	0.1673
20100717	1255.37	0.1621
20100718	1310.93	0.1568
20100719	1366.48	0.1516
20100720	1422.04	0.1464
20100721	1477.59	0.1412
20100722	1533.15	0.1359
20100723	1588.71	0.1307
20100724	1644.26	0.1255
20100725	1699.82	0.1203
20100726	1755.37	0.1150
20100727	1810.93	0.1098
20100728	1866.48	0.1046
20100729	1922.04	0.0993
20100730	5000.00	0.0993
* ---1---1---1---1---1---1---		
* magnesium oxide - volumetric heat capacity		
* ---1---1---1---1---1---1---		
20100751	373.15	2033.52
20100752	422.04	2004.59
20100753	477.59	1917.74

20100754	533.15	1938.87
20100755	588.71	1906.01
20100756	644.26	1873.15
20100757	699.82	1840.29
20100758	755.37	1807.43
20100759	810.93	1774.56
20100760	866.48	1741.70
20100761	922.04	1708.84
20100762	977.59	1675.96
20100763	1033.15	1643.11
20100764	1088.71	1610.25
20100765	1144.26	1577.39
20100766	1199.82	1544.53
20100767	1255.37	1511.67
20100768	1310.93	1478.80
20100769	1366.48	1445.94
20100770	1422.04	1413.08
20100771	1477.59	1380.22
20100772	1533.15	1347.35
20100773	1588.71	1314.49
20100774	1644.26	1281.63
20100775	1699.82	1248.77
20100776	1755.37	1215.90
20100777	1810.93	1183.04
20100778	1866.48	1150.18
20100779	1922.04	1117.32
20100780	5000.00	1117.32
* ---1---1---1---1---1---1---		
* nichrome - thermal conductivity		
* ---1---1---1---1---1---1---		
20100801	373.15	1.1163
20100802	422.04	1.1163
20100803	5000.00	1.1163
* ---1---1---1---1---1---1---		
* nichrome - volumetric heat capacity		
* ---1---1---1---1---1---1---		
20100851	373.15	2180.80
20100852	422.04	2180.80
20100853	5000.00	2180.80
* ---1---1---1---1---1---1---		
* pressurizer cycling heaters		
* ---1---1---1---1---1---1---		
20241700	power	608
20241701	0.0	0.0
20241702	60.	4.e3
* ---1---1---1---1---1---1---		
* pressurizer backup heaters		
* ---1---1---1---1---1---1---		
20241800	power	629
20241801	0.0	0.0
20241802	60.	4.e3
* ---1---1---1---1---1---1---		
* scram reactivity data		
* ---1---1---1---1---1---1---		
20260900	"react "	609
20260901	0.0	0.0
20260902	0.5	-0.5
20260903	0.59	-3.13
20260904	0.65	-3.95
20260905	0.75	-6.27







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20504300 pcsvol3 sum 1.0 0.0 1
20504301 0.0 4.37000-2 rho 115170000
20504302 4.62000-2 rho 115180000
20504303 3.54406-2 rho 115190000
20504304 4.81840-2 rho 120010000
20504305 6.13000-2 rho 125010000
20504306 1.89000-2 rho 130010000
20504307 6.13000-2 rho 155010000
20504308 1.89000-2 rho 160010000
*-----1-----1-----1-----1-----1-----1-----
* cold leg intact loop
*-----1-----1-----1-----1-----1-----1-----
20500400 pcsvol4 sum 1.0 0.0 1
20500401 0.0 9.90000-2 rho 135010000
20500402 1.83732-2 rho 140010000
20500403 6.33000-2 rho 145010000
20500404 3.14844-2 rho 150010000
20500405 9.90000-2 rho 165010000
20500406 1.88124-2 rho 170010000
20500407 3.54406-2 rho 175010000
20500408 3.88642-2 rho 175020000
20500409 4.44434-2 rho 180010000
20500410 9.26274-2 rho 185010000
*-----1-----1-----1-----1-----1-----1-----
* reactor
*-----1-----1-----1-----1-----1-----1-----
20500500 pcsvol5 sum 1.0 0.0 1
20500501 0.0 2.66400-1 rho 215010000
20500502 2.92300-1 rho 220010000
20500503 1.30000-1 rho 225010000
20500504 9.53095-2 rho 230010000
20500505 9.53095-2 rho 230020000
20500506 0.1120185 rho 230030000
20500507 8.38500-3 rho 235010000
20500508 8.38500-3 rho 235020000
20500509 9.35500-3 rho 235030000
20500510 3.32046-1 rho 240010000
20500511 9.61020-2 rho 245010000
20500512 1.28100-1 rho 246010000
20500513 2.45952-1 rho 250010000
20500514 1.73728-1 rho 250010000
*-----1-----1-----1-----1-----1-----1-----
* hot leg broken loop
*-----1-----1-----1-----1-----1-----1-----
20500600 pcsvol6 sum 1.0 0.0 1
20500601 0.0 5.55384-2 rho 300010000
20500602 4.42532-2 rho 305010000
20500603 6.68000-2 rho 310010000
20500604 3.38914-3 rho 315010000
20500605 4.40154-3 rho 315020000
20500606 3.90960-2 rho 315030000
20500607 1.82736-1 rho 315040000
20500608 9.17460-2 rho 315050000
20500609 9.17460-2 rho 315060000
20500610 1.82736-1 rho 315070000
20500611 3.90960-2 rho 315080000
20500612 1.62000-2 rho 315090000
20500613 6.48000-2 rho 315100000
20500614 .01539912 rho 315110000
20500615 3.50175-2 rho 315120000

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20500616 8.54764-2 rho 370010000
20500617 8.58000-2 rho 375010000
*-----1-----1-----1-----1-----1-----1-----
* cold leg broken loop
*-----1-----1-----1-----1-----1-----1-----
20500700 pcsvol7 sum 1.0 0.0 1
20500701 0.0 4.75183-2 rho 335010000
20500702 4.42532-2 rho 340010000
20500703 6.17516-2 rho 345010000
20500704 5.41000-3 rho 350010000
20500705 0.07770 rho 350020000
20500706 8.55000-2 rho 380010000
20500707 1.18030-1 rho 385010000
*-----1-----1-----1-----1-----1-----1-----
* pressurizer
*-----1-----1-----1-----1-----1-----1-----
20500800 pcsvol8 sum 1.0 0.0 1
20500801 0.0 5.00250-3 rho 400010000
20500802 5.00250-3 rho 405010000
20500803 8.10880-2 rho 415010000
20500804 2.27695-1 rho 415020000
20500805 2.27695-1 rho 415030000
20500806 1.16955-1 rho 415040000
20500807 1.16955-1 rho 415050000
20500808 7.94530-2 rho 415060000
20500809 7.94530-2 rho 415070000
20500810 1.53400-2 rho 415080000
*-----1-----1-----1-----1-----1-----1-----
* reactor vessel downcomer mass
*-----1-----1-----1-----1-----1-----1-----
20500900 dwncrms sum 1.0 0.0 1
20500901 0.0 8.55000-2 rho 200010000
20500902 1.10000-1 rho 205010000
20500903 1.36036-1 rho 210010000
20500904 1.36036-1 rho 210020000
20500905 1.36036-1 rho 210030000
20500906 1.36036-1 rho 210040000
20500907 1.23426-2 rho 223010000
20500908 2.78874-2 rho 223020000
20500909 2.78874-2 rho 223030000
20500910 2.78874-2 rho 223040000
20500911 2.78874-2 rho 223050000
20500912 1.04796-2 rho 223060000
20500913 1.04796-2 rho 223070000
*-----1-----1-----1-----1-----1-----1-----
* pcs mass
*-----1-----1-----1-----1-----1-----1-----
20501000 pcsmass sum 1.0 0.0 1
20501001 0.0 1.0 cntrivar 41
20501002 1.0 cntrivar 42
20501003 1.0 cntrivar 43
20501004 1.0 cntrivar 4
20501005 1.0 cntrivar 5
20501006 1.0 cntrivar 6
20501007 1.0 cntrivar 7
20501008 1.0 cntrivar 8
20501009 1.0 cntrivar 9
*-----1-----1-----1-----1-----1-----1-----
* break energy computer
*-----1-----1-----1-----1-----1-----1-----

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20542500 pvfstm div 1.0 0.0 1
20542501 rhof 420010000 p 420010000
*
20542600 hfstm sum 1.0 0.0 1
20542601 0.0 1.0 uf 420010000
20542602 1.0 cntrivar 425
*
20542700 pvgstm div 1.0 0.0 1
20542701 rhog 420010000 p 420010000
*
20542800 hgstm sum 1.0 0.0 1
20542801 0.0 1.0 ug 420010000
20542802 1.0 cntrivar 427
*
20542900 xhgstm mult 1.0 0.0 1
20542901 quals 420010000 cntrivar 428
*
20543000 xhfstm mult 1.0 0.0 1
20543001 quals 420010000 cntrivar 426
*
20543100 yhfstm sum 1.0 0.0 1
20543101 0.0 1.0 cntrivar 426
20543102 -1.0 cntrivar 430
*
20543200 hsteam sum 1.0 0.0 1
20543201 0.0 1.0 cntrivar 429
20543202 1.0 cntrivar 431
*
20543300 brkpwr mult 1.0 0.0 1
20543301 mflowj 425000000 cntrivar 432
*
20543400 brkflow integral 1.0 0.0 1
20543401 mflowj 425000000
*
* 011 - 031 heat transfer rate calculator
*
* heat added to pcs from core
*
20511100 corhtr sum 1.0 0.0 1
20511101 0.0 24.374 htmr 230000101
20511102 24.374 htmr 230000201
20511103 24.374 htmr 230000301
*
* heat removed from pcs at to s/g tubes
*
20511200 sghttr sum 1.0 0.0 1
20511201 0.0 20.117 htmr 006000100
20511202 20.117 htmr 006000200
20511203 20.117 htmr 006000300
20511204 20.117 htmr 006000400
20511205 80.468 htmr 006000500
20511206 33.937 htmr 006000600
20511207 33.937 htmr 006000700
20511208 80.468 htmr 006000800
20511209 20.117 htmr 006000900
20511210 20.117 htmr 006001000
20511211 20.117 htmr 006001100
20511212 20.117 htmr 006001200
*
* heat loss from reactor vessel

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*
20511300 rvheat sum 1.0 0.0 1
20511301 0.0 2.3244 htmr 211000101
20511302 5.25183 htmr 211000201
20511303 3.56335 htmr 211000301
20511304 1.59598 htmr 212000101
20511305 4.96411 htmr 212000201
20511306 4.96411 htmr 212000301
20511307 1.86543 htmr 212000401
20511308 1.91724 htmr 212000501
20511309 1.68000 htmr 220000101
20511310 0.71200 htmr 255000101
*
* heat loss from pwr
*
20511400 pwrheat sum 1.0 0.0 1
20511401 0.0 0.362 htmr 415100101
20511402 0.702464 htmr 415200101
20511403 1.26381 htmr 415200201
20511404 1.26381 htmr 415200301
20511405 0.649152 htmr 415200401
20511406 0.649152 htmr 415200501
20511407 0.534688 htmr 415200601
20511408 0.534688 htmr 415200701
20511409 0.273063 htmr 416200101
20511410 0.130000 htmr 420100101
20511411 0.273063 htmr 420200101
*
* heat loss from s/g
*
20511500 sgheat sum 1.0 0.0 1
20511501 0.0 3.5343 htmr 530000101
20511502 3.5343 htmr 530000201
20511503 3.33022 htmr 530000301
20511504 3.33022 htmr 530000401
20511505 2.40258 htmr 530000501
20511506 3.29404 htmr 530000601
20511507 3.29404 htmr 530000701
20511508 3.29404 htmr 530000801
*
* total heat loss from major components
*
20511600 totheat sum 1.0 0.0 1
20511601 0.0 1.0 cntrivar 113
20511602 1.0 cntrivar 114
20511603 1.0 cntrivar 115
*
* heat loss from broken loop hot leg
*
20511700 blhheat sum 1.0 0.0 1
20511701 0.0 0.97972 htmr 300000101
20511702 0.78065 htmr 300000201
20511703 1.59260 htmr 300000301
*
* heat loss from broken loop cold leg
*
20511800 bclheat sum 1.0 0.0 1
20511801 0.0 0.83825 htmr 335000101
20511802 0.78065 htmr 335000201
20511803 1.0893 htmr 335000301

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20525319      1.0      cntrivar 252
*-----1-----1-----1-----1-----1-----1-----
* metal heating in broken loop (1st part)
*-----1-----1-----1-----1-----1-----1-----
20512600 bk1pmt sum      1.0      0.0      1
20512601 0.0      0.157878 htnr      300000100
20512602      0.622764 htnr      300000200
20512603      1.27051 htnr      300000300
20512616      0.668713 htnr      335000100
20512617      0.622764 htnr      335000200
20512618      0.869015 htnr      335000300
*-----1-----1-----1-----1-----1-----1-----
* metal heating in broken loop
*-----1-----1-----1-----1-----1-----1-----
20512700 bk1pmt sum      1.0      0.0      1
20512701 0.0      1.39487 htnr      370000100
20512702      0.771131 htnr      370000200
20512703      0.768435 htnr      370000300
20512704      2.12160 htnr      370000400
20512705      1.0      cntrivar 126
*-----1-----1-----1-----1-----1-----1-----
* metal heating in intact loop hot leg
*-----1-----1-----1-----1-----1-----1-----
20512800 ih1mht sum      1.0      0.0      1
20512801 0.0      1.3716 htnr      100100100
20512802      1.45787 htnr      100100200
20512803      0.55548 htnr      100100300
20512804      1.28345 htnr      100100400
20512805      0.72288 htnr      100200100
20512806      1.4772 htnr      100400100
*-----1-----1-----1-----1-----1-----1-----
* metal heating in intact loop cold leg
*-----1-----1-----1-----1-----1-----1-----
20512900 ic1mht sum      1.0      0.0      1
20512901 0.0      0.614734 htnr      100100500
20512902      0.498747 htnr      100100600
20512903      0.678081 htnr      100100700
20512904      0.443073 htnr      100100800
20512905      0.498747 htnr      100100900
20512906      0.546926 htnr      100101000
20512907      0.625441 htnr      100101100
20512908      1.30352 htnr      100101200
20512909      0.558497 htnr      100200200
20512910      0.678584 htnr      100300100
20512911      0.310113 htnr      100300200
20512912      0.340649 htnr      100300300
20512913      0.955718 htnr      100300400
20512914      0.680620 htnr      100300500
20512915      0.310113 htnr      100300600
20512916      0.348792 htnr      100300700
20512917      1.4772 htnr      100400200
*-----1-----1-----1-----1-----1-----1-----
* metal heating in broken loop simulators
*-----1-----1-----1-----1-----1-----1-----
20513000 bl1sim sum      1.0      0.0      1
20513001 0.0      0.1312 htnr      315000100
20513002      0.1703 htnr      315000200
20513003      0.0042 htnr      315100100
20513004      0.00347 htnr      315200100
20513005      0.12452 htnr      315300100

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20513006      0.12452 htnr      315300200
20513007      0.12452 htnr      315300300
20513008      0.12452 htnr      315300400
20513009      0.12452 htnr      315300500
20513010      0.12452 htnr      315300600
20513011      0.04239 htnr      315400100
20513012      0.04363 htnr      315500100
*-----1-----1-----1-----1-----1-----1-----
* metal heating in steam generator
*-----1-----1-----1-----1-----1-----1-----
20555100 sgmth1 sum      1.0      0.0      1
20555101 0.0      1.47943 htnr      500000100
20555102      1.47943 htnr      500000200
20555103      0.291097 htnr      500000300
20555104      1.52566 htnr      500000101
20555105      1.52566 htnr      500000201
20555106      0.300194 htnr      500000301
20555107      0.615526 htnr      515000100
20555108      2.88042 htnr      515000200
20555109      2.88042 htnr      515000300
20555110      2.88042 htnr      515000400
20555111      0.627655 htnr      515000101
20555112      2.93718 htnr      515000201
20555113      2.93718 htnr      515000301
20555114      2.93718 htnr      515000401
*
20555200 sgmth2 sum      1.0      0.0      1
20555201 0.0      3.40507 htnr      530000100
20555202      3.40507 htnr      530000200
20555203      3.20846 htnr      530000300
20555204      3.30846 htnr      530000400
20555205      2.31474 htnr      530000500
20555206      3.17360 htnr      530000600
20555207      3.17360 htnr      530000700
20555208      3.17360 htnr      530000800
*-----1-----1-----1-----1-----1-----1-----
* pcs-tubesheet heat transfer
*-----1-----1-----1-----1-----1-----1-----
20513200 pcstub sum      1.0      0.0      1
20513201 0.0      56.4226 htnr      115100100
20513202      56.4226 htnr      115100200
20513203      0.157962 htnr      115200100
20513204      0.157962 htnr      115200200
*-----1-----1-----1-----1-----1-----1-----
* tubesheet-scs heat transfer
*-----1-----1-----1-----1-----1-----1-----
20513300 tushscs sum      1.0      0.0      1
20513301 0.0      0.157962 htnr      115200101
20513302      0.157962 htnr      115200201
*-----1-----1-----1-----1-----1-----1-----
* metal hx in rabs
*-----1-----1-----1-----1-----1-----1-----
20517000 rabs sum      1.0      0.0      1
20517001 0.0      1.39487 htnr      370000100
20517002      0.77113 htnr      370000200
20517003      0.77278 htnr      370000300
20517004      2.12160 htnr      370000400
*****
* bl total metal hx

```

```

*****
20517100 qbitotal sum 1.0 0.0 1
20517101 0.0 1.0 cntrivar 127
*20517102 1.0 cntrivar 170
20517103 1.0 cntrivar 130 * only for simula
*****
* pcs stored energy excluding pressurizer
*****
20557000 pcsqre sum 1.0 0.0 1
20557001 0.0 1.0 cntrivar 253 * rv metal heat
20557002 1.0 cntrivar 113 * rv ambloss
20557003 1.0 cntrivar 171 * only for simula
20557004 1.0 cntrivar 117 * ihl ambloss
20557005 1.0 cntrivar 118 * bld ambloss
20557006 1.0 cntrivar 119 * rabv ambloss
20557007 1.0 cntrivar 128 * ihl heat
20557008 1.0 cntrivar 120 * ihl ambloss
20557009 1.0 cntrivar 129 * icl heat
20557010 1.0 cntrivar 121 * icl ambloss
20557011 1.0 cntrivar 132 * pcs-tubesheet
20557012 1.0 cntrivar 133 * tubesheet-scs
*****
* scs stored energy
*****
20557300 scsqse sum 1.0 0.0 1
20557301 0.0 1.0 cntrivar 552 * sg heat
20557302 1.0 cntrivar 115 * sg ambloss
*****
* heat flow calculations
*****
* ecc energy flow
*****
20515300 pvecc div 1.0 0.0 1
20515301 rhofj 630000000 p 600010000
20515400 hecc sum 1.0 0.0 1
20515401 0.0 1.0 ufj 630000000
20515402 1.0 cntrivar 153
20515500 mdothecc mult 1.0 0.0 1
20515501 mflowj 630000000
20515502 cntrivar 154
20515600 qecc/v mult 0.126646 0.0 1
20515601 cntrivar 155
20515700 mdotev mult 0.126646 0.0 1
20515701 mflowj 630000000
*****
* sg hx per unit pcs volume
*****
20516000 qsg/v mult 0.126646 0.0 1
20516001 cntrivar 112
*****
* core hx per unit pcs volume
*****
20516100 qcore/v mult 0.126646 0.0 1
20516101 cntrivar 111
*****
* pump power
*****
20516200 p1edotv mult 0.04136 0.0 1
20516201 voidgj 135020000
20516202 velgj 135020000

```

```

20516203 pmphead 135
20516300 p1edot mult 0.04136 0.0 1
20516301 voidfj 135020000
20516302 velfj 135020000
20516303 pmphead 135
20516400 p2edotv mult 0.04136 0.0 1
20516401 voidgj 165020000
20516402 velgj 165020000
20516403 pmphead 165
20516500 p2edot mult 0.04136 0.0 1
20516501 voidfj 165020000
20516502 velfj 165020000
20516503 pmphead 165
20516600 qpmp sum 1.0 0.0 1
20516601 0.0 1.0 cntrivar 162
20516602 1.0 cntrivar 163
20516603 1.0 cntrivar 164
20516604 1.0 cntrivar 165
20516700 qpmp/v mult 0.126646 0.0 1
20516701 cntrivar 166
*****
* energy to fluid in vessel from structures
*****
20562000 rvhx sum 6.2832 0.0 1
20562001 0.0 0.3080 htmr 205000101
20562002 0.6959 htmr 210000101
20562003 0.6959 htmr 210000201
20562004 0.6959 htmr 210000301
20562005 0.6959 htmr 210000401
20562006 0.2615 htmr 210000501
20562007 0.2688 htmr 210000601
20562008 0.3107 htmr 211000100
20562009 0.7020 htmr 211000200
20562010 0.7020 htmr 212000100
20562011 0.7020 htmr 212000200
20562012 0.7030 htmr 212000300
20562013 0.6 htmr 212000400
20562014 0.2 htmr 212000500
20562015 1.0 cntrivar 253
*---1---1---1---1---1---1---1---1---
* total vessel hx/v
*---1---1---1---1---1---1---1---1---
20562100 rvhx/v mult 1.0 0.0 1
20562101 cntrivar 620
*****
* total massless energy flows from pcs excluding qcore and qsg
*****
20562200 qstruc sum 1.0 0.0 1
20562201 0.0 1.0 cntrivar 123 * przr
20562202 1.0 cntrivar 620 * rv
20562203 1.0 cntrivar 171 * bl
20562204 1.0 cntrivar 128 * ihl
20562205 1.0 cntrivar 129 * icl
20562300 qstruc/v mult 0.126646 0.0 1
20562301 cntrivar 622
*****
* sum of all massless energy flows from pcs
*****
20562400 de/dt sum 1.0 0.0 1
20562401 0.0 1.0 cntrivar 111 * core

```

```

20562402      1.0  cntrivar  112  * sg
20562403      1.0  cntrivar  622  * structure
20562404      1.0  cntrivar  166  * pumps
20562500  de/dt/vv  mult    0.126646  0.0  1
20562501      cntrivar  624
*****
* sum of mass flow energy flows and massless energy flows
*****
20562600  dtqflo sum    1.0    0.0    1
20562601  0.0    1.0  cntrivar  624  * de/dt
20562602      -1.0  cntrivar  433  * parv
20562700  dtqf/v  mult    0.126646  0.0  1
20562701      cntrivar  626
*-----1-----1-----1-----1-----1-----
* primary coolant pump speed controllers
*-----1-----1-----1-----1-----1-----
* calculate mass flow error
*-----1-----1-----1-----1-----1-----
20590100  msserr sum    1.0    0.0    1
20590101  479.30  -1.0  mflowj  100010000
*-----1-----1-----1-----1-----1-----
* pump 1 speed
*-----1-----1-----1-----1-----1-----
20590200  pcp1spd  integral  0.34482  333.7236  1
20590201  cntrivar  901
*-----1-----1-----1-----1-----1-----
* pcp1 pump velocity table
*-----1-----1-----1-----1-----1-----
1356100  508  cntrivar  902
1356101  0.0  0.0
1356102  369.0  369.0
*-----1-----1-----1-----1-----1-----
* modify pcp1 pump data
*-----1-----1-----1-----1-----1-----
1350301  0  0  0  -1  0  504  0
*-----1-----1-----1-----1-----1-----
* pump 2 speed
*-----1-----1-----1-----1-----1-----
20590300  pcp2spd  integral  0.34482  331.9524  1
20590301  cntrivar  901
*-----1-----1-----1-----1-----1-----
* pcp2 pump velocity table
*-----1-----1-----1-----1-----1-----
1656100  508  cntrivar  903
1656101  0.0  0.0
1656102  369.0  369.0
*-----1-----1-----1-----1-----1-----
* modify pcp2 pump data
*-----1-----1-----1-----1-----1-----
1650301  135  135  135  -1  0  504  0
*-----1-----1-----1-----1-----1-----
* pressurizer spray valve controller
*-----1-----1-----1-----1-----1-----
* spray valve
*-----1-----1-----1-----1-----1-----
4070000  sprlv  valve
4070101  406010000  420010000  3.3451e-4  1.2  1.2  000100
4070201  0  .000000000  .000000000  0.0
4070300  srwlv
4070301  904  999

```

```

*-----1-----1-----1-----1-----1-----
* spray valve position calculator
*-----1-----1-----1-----1-----1-----
20590400  spray  sum    -1.0    0.0    1  * contin
+ 3  0.0  1.0
20590401  14.93+6  -1.0  p  420010000
*-----1-----1-----1-----1-----1-----
* position vs area table
*-----1-----1-----1-----1-----1-----
20299900  normarea
20299901  0.0  0.0
20299902  0.0001  0.0
20299903  1.0  1.0
*-----1-----1-----1-----1-----1-----
* pressurizer level control using charging and letdown components
*-----1-----1-----1-----1-----1-----
* charging reservoir
*-----1-----1-----1-----1-----1-----
*9800000  chrg  tmdpvcl
*9800101  1.0  1.0  0.0  0.0  0.0  0.0
*9800102  4.0-5  0.0  00000
*9800200  3
*9800201  0.0  2.07+07  558.9
*-----1-----1-----1-----1-----1-----
* charging valve
*-----1-----1-----1-----1-----1-----
*9850000  chrg  valve
*9850101  980000000  185000000  3.8e-05  0.0  0.0  000100
*9850201  0  .000000000  .000000000  0.0
*9850300  srwlv
*9850301  905  999
*-----1-----1-----1-----1-----1-----
* charging valve position calculator
*-----1-----1-----1-----1-----1-----
*20590500  charge  sum    7.7    0.0    1
*contin
*+ 3  0.0  1.0
*20590501  0.92  -1.0  cntrivar  2
*-----1-----1-----1-----1-----1-----
* letdown sink
*-----1-----1-----1-----1-----1-----
*9900000  ltdwn  tmdpvcl
*9900101  1.0  1.0  0.0  0.0  0.0  0.0
*9900102  4.0-5  0.0  00000
*9900200  3
*9900201  0.0  1.4+7  558.9
*-----1-----1-----1-----1-----1-----
* letdown valve
*-----1-----1-----1-----1-----1-----
*9950000  ltdwn  valve
*9950101  185000000  990000000  2.5-5  0.0  0.0  000100
*9950201  0  .000000000  .000000000  0.0
*9950300  srwlv
*9950301  906  999
*-----1-----1-----1-----1-----1-----
* letdown valve position calculator
*-----1-----1-----1-----1-----1-----
*20590600  letdown  sum    -7.7    0.0    1
*contin
*+ 3  0.0  1.0

```



```

*20590601 1.10 -1.0 cntrivar 2
*---1---1---1---1---1---1---1---
* steam valve controller
*---1---1---1---1---1---1---1---
* changes to steam valve
*---1---1---1---
*5500201 0 19.758 22.082 0.0
*5500300 srwlv
*5500301 910 540
*20254000 normarea
*20254001 0.0 0.0
*20254002 0.0001 0.0
*20254003 1.0 1.0
*---1---1---1---
* compute delta t error
*---1---1---1---
*20590700 delta sum 1.0 0.0 1
*20590701 559.0 -1. tempf 185010000
*---1---1---1---
* filter delta t thru deadband
*---1---1---1---
*20590800 deadband function 1.0 0.0 1
*20590801 cntrivar 907 908
*20290800 reac-t
*20290801 -100. -100.
*20290802 -0.25 -0.25
*20290803 -0.25 0.0
*20290804 0.25 0.0
*20290805 0.25 0.25
*20290806 100. 100.
*---1---1---1---
* integrate delta t error
*---1---1---1---
*20590900 int integral 1.0 0.0 1
*20590901 cntrivar 908
*---1---1---1---
* steam valve position calculator
*---1---1---1---
*20591000 tcontrol sum 1.0 0.645229 0 *conti
*+ 3 0.6 0.90
*20591001 0.645229 -0.07126 cntrivar 908
*20591002 -0.01492 cntrivar 909
*---1---1---1---1---1---1---1---
* simplified feed system controller
*---1---1---1---1---1---1---1---
20591100 sgjvierr sum 1.0 0.0 1
20591101 3.09 -1.0 cntrivar 001
20591200 feedflow sum 1.0 0.0 1
20591201 0.0 1.0 mflowj 550000000
20591202 48.4 cntrivar 911
*---1---1---1---1---
* replace feed junction table
*---1---1---1---1---
5600200 1 0 cntrivar 912
5600201 -100.0 25.553 0.0 0.0
5600202 -1.0 0.0 0.0 0.0
5600203 0.0 0.0 0.0 0.0
5600204 50.0 50.0 0.0 0.0

```



## **Appendix B**

### **Transient Input Deck for Base Case**



=loft 19-1 post test analysis deck

\*---1---1---1---1---1---1---

\* initial conditions

\*  
\* pcp pressure = 14.901 mpa  
\* core power = 50. mw  
\* pcs flow = 479.3 kg/s  
\* that = 578. k  
\* tcold = 559.0 k  
\*

\*---1---1---1---1---1---1---

0000100 restart transnt  
0000101 run  
0000102 si  
0000103 15808  
0000105 5. 10.  
0000201 200.00 1.e-6 1.0 3 1 30 100  
0000202 1000.0 1.e-6 1.0 3 5 300 500  
0000203 2000.0 1.e-6 0.1 3 50 3000 5000  
0000204 4000.0 1.e-6 0.5 3 10 1000 2000  
0000205 8000.0 1.e-6 0.1 3 50 4000 5000  
0000206 10000. 1.e-6 0.5 3 10 2000 2000

\*\*\*\*\*

\* minor edit variables

\*

\*\*\*\*\* pressure

\*\*\*\*\*0000301 p 345010000 \* pe-bl-1

0000301 p 310010000 \* pe-bl-2  
\*0000303 p 315110000 \* pe-bl-3  
\*0000304 p 350010000 \* pe-bl-4  
\*0000305 p 315090000 \* pe-bl-6  
\*0000306 p 350020000 \* pe-bl-8  
0000302 p 185010000 \* pe-pc-1  
0000303 p 100010000 \* pe-pc-2  
0000304 p 420010000 \* porv inlet  
\*0000310 p 110010000 \* pt-139-2,3,4  
0000305 p 245010000 \* pe-1up-1a,1b  
0000306 p 215010000 \* pe-1st-1a,b/pe-2st-1a,b  
\*0000313 p 200010000 \* pe-1st-3a,3b  
0000307 p 530010000 \* pe-sgs-01  
0000308 p 535010000 \* pt-p4-85

\*\*\*\*\* temperatures

\*\*\*\*\*0000309 tempf 406010000 \* spray tempf

0000310 tempf 310010000 \* te-bl-2a,2b,2c  
0000311 tempf 100010000 \* te-pc-2a,2b,2c  
0000312 tempf 185010000 \* te-pc-1  
0000313 tempf 115030000 \* te-sg-1  
0000314 tempf 115100000 \* te-sg-2  
0000315 tempf 515070000 \* te-sg-4  
\*0000328 tempf 415050000 \* pzz volume 5  
0000316 tempf 415040000 \* te-139-19  
\*0000330 tempf 415030000 \* te-139-20  
\*0000331 tempf 315120000 \* te-p138-171  
\*0000332 tempf 350020000 \* te-p138-170  
\*0000333 tempf 205010000 \* te-1st-1/te-2st-1  
0000317 tempf 210010000 \* te-1st-2/te-2st-2  
\*0000335 tempf 345010000 \* te-bl-1  
\*0000336 tempf 210030000 \* te-1st-14/te-2st-14  
\*0000337 tempf 210040000 \* te-3up-2  
\*0000338 tempf 245010000 \* te-1up-6  
\*0000339 tempf 246010000 \* te-2up-4  
\*0000340 tempf 250010000 \* te-1up-3

\*\*\*\*\* densities

```

*****0000341 rho 345010000 * de-bl-1
0000318 rho 310010000 * de-bl-2
0000319 rho 185010000 * de-pc-1
0000320 rho 100010000 * de-pc-2
*0000345 rho 115120000 * de-pc-3
0000321 voidgj 400010000 * surge line density
*0000347 rho 115040000 * s/g tubes
*0000348 rho 115050000 * s/g tubes
*0000349 rho 115060000 * s/g tubes
*0000350 rho 115070000 * s/g tubes
***** velocities
*****0000351 voidf 100010000 * ihl nozzle
*0000352 velf 100010000 * ihl nozzle
*0000353 velf 115030000 * s/g inlet
*0000354 velf 400010000 * surge line
*0000355 velfj 425000000 * porv liq vel
*0000356 velg 100010000 * ihl nozzle
*0000357 velg 115030000 * s/g inlet
*0000358 velg 400010000 * surge line
*0000359 velgj 425000000 * porv vap vel
***** mass flow rates
*****0000322 mflowj 100010000 * ihl nozzle
*0000361 mflowj 150010000 * pump outlet
*0000362 mflowj 185020000 * dtl-rake icl
0000323 mflowj 400010000 * pres. surge line flow
0000324 mflowj 407000000 * p2r spray flow
0000325 mflowj 425000000 * pres. relief valve flow
0000326 mflowj 550000000 * steam flow control valve
0000327 mflowj 548000000 * aux feed
*0000369 mflowj 560000000 * main feed
***** cladding temperatures center module
*****0000371 httemp 230000110 * te-5h5-015
*0000372 httemp 230000210 * te-5h5-034
*0000373 httemp 230000310 * te-5h5-049
***** peak centerline temperatures
*****0000374 httemp 230000101 * core lower region
*0000375 httemp 230000201 * core middle region
*0000376 httemp 230000301 * core upper region
***** reactor kinetic parameters
*****
0000328 rktpow 0 * total reactor power
*0000378 rkfpow 0 * fission decay power
*0000379 rkgapow 0 * gamma decay power
*0000380 rkreact 0 * reactivity
*0000381 pmphead 135 * pcp1 head
*0000382 pmphead 165 * pcp2 head
0000329 mflowj 185010000
0000330 mflowj 185030000
*0000388 mflowj 200020000
0000331 pmpvel 135
***** control variable requests
*****0000332 cntrivar 001
0000333 cntrivar 002
0000334 cntrivar 003
0000335 cntrivar 041
0000336 cntrivar 042
0000337 cntrivar 043
0000338 cntrivar 004
0000339 cntrivar 005
0000340 cntrivar 006
0000341 cntrivar 007
0000342 cntrivar 008
0000343 cntrivar 009

```

```

0000344  cntrivar  010
0000345  cntrivar  433
0000346  cntrivar  434
0000347  cntrivar  111
0000348  cntrivar  112
0000349  cntrivar  113
0000350  cntrivar  114
0000351  cntrivar  115
0000352  cntrivar  116
0000353  cntrivar  117
0000354  cntrivar  118
0000355  cntrivar  119
0000356  cntrivar  120
0000357  cntrivar  121
0000358  cntrivar  122
0000359  cntrivar  123
0000360  cntrivar  251
0000361  cntrivar  252
0000362  cntrivar  253
0000363  cntrivar  126
0000364  cntrivar  127
0000365  cntrivar  128
0000366  cntrivar  129
0000367  cntrivar  130
0000368  cntrivar  551
0000369  cntrivar  552
0000370  cntrivar  132
0000371  cntrivar  133
0000372  cntrivar  170
0000373  cntrivar  171
0000374  cntrivar  570
0000375  cntrivar  573
0000376  cntrivar  153
0000377  cntrivar  154
0000378  cntrivar  155
0000379  cntrivar  156
0000380  cntrivar  157
0000381  cntrivar  160
0000382  cntrivar  161
0000383  cntrivar  166
0000384  cntrivar  167
0000385  cntrivar  620
0000386  cntrivar  621
0000387  cntrivar  622
0000388  cntrivar  623
0000389  cntrivar  624
0000390  cntrivar  625
0000391  cntrivar  626
0000392  cntrivar  627
0000393  tempg     515070000
0000394  rho       420010000
0000395  cputime   0
20800095  dt        0
20800096  dtcont    0

```

```
*****
```

```
* trips
*
```

```
***** variable trips
*****0000501 p 100010000 le null 0 14.193103e6 l
```

```
* ecc check valve
0000502 p 600010000 ge p 185010000 20.e6 n
* accumulator check valve
0000503 p 615010000 ge p 185010000 20.e6 n
```

```

* isolation valve hot leg
0000504 time 0 lt null 0 0.0 |
* isolation valve cold leg
0000505 time 0 lt null 0 0.0 |
* qobv hot leg
0000506 time 0 lt null 0 0.0 |
* qobv cold leg
0000507 time 0 lt null 0 0.0 |
* check valve surge line pressurizer
0000508 time 0 ge null 0 0.0 |
* pressurizer relief valve
0000509 tempf 100010000 ge null 0 597.0 |
* steam control valve
0000510 time 0 lt null 0 0.0 |
* boundary system valve
0000511 time 0 lt null 0 0.0 |
* lps trip
0000512 time 0 ge null 0 10000.0 |
* hpis trip
0000513 time 0 ge null 0 10000.0 |
*
0000520 p 530020000 gt null 0 7.103448e6 n
0000521 p 530020000 lt null 0 7.0344827e6 n
0000522 p 530020000 gt null 0 6.3448275e6 n
0000523 p 530020000 lt null 0 6.4137931e6 n
0000530 time 0 ge null 0 3600.0 n
0000531 p 530020000 gt p 547010000 0.0 n
0000536 time 0 ge null 0 10000.0 n
0000540 tempf 100010000 gt null 0 583.16 |
0000541 p 100010000 gt null 0 1.574553e7 |
0000550 time 0 ge null 0 10000.0 |
0000551 time 0 ge timeof 625 0.0 |
0000552 time 0 ge timeof 509 1580. |
0000560 p 100010000 le null 0 13.15862e6 n
0000561 time 0 ge timeof 552 265.0 |
0000562 time 0 gt null 0 5400.0 n
0000563 cntrvar 1 lt null 0 2.1844 n
0000564 cntrvar 1 gt null 0 2.9464 n
0000565 time 0 ge timeof 669 966. |
0000570 p 420010000 gt null 0 1.620058e7 n
0000571 p 420010000 lt null 0 1.606269e7 n
0000572 p 420010000 lt null 0 1.486300e7 n
0000573 p 420010000 gt null 0 1.506980e7 n
0000574 p 420010000 gt null 0 1.533874e7 n
0000575 p 420010000 lt null 0 1.505000e7 n
0000576 p 420010000 lt null 0 1.482853e7 n
0000577 p 420010000 gt null 0 1.495950e7 n

```

```

***** logical trips
*****0000600 536

```

```

0000601 563 and 561 n
0000602 -563 and -564 n
0000603 655 and 602 n
0000604 609 or 609 |
0000605 572 and -509 n
0000606 -572 and -573 n
0000607 608 and 606 n
0000608 605 or 607 n
0000609 540 or 541 |
0000610 612 or 520 n
0000611 -521 and -616 n
0000612 611 and 610 n
0000613 616 or 523 n
0000614 -522 and 613 n

```



```

0000615 -612 and 609 n
0000616 615 and 614 n
0000617 612 or 616 n
0000618 605 or 607 n
0000621 623 or 570 n
0000622 -571 and -571 n
0000623 621 and 622 n
0000624 509 and -552 n
0000625 623 or 624 n
0000626 576 and -509 n
0000627 -576 and -577 n
0000628 629 and 627 n
0000629 626 or 628 n
0000635 504 and 504 n
0000636 509 and -536 n
0000650 -652 and 550 n
0000651 650 or 652 n
0000652 -509 and 651 n
0000655 601 or 603 n
0000656 508 or 609 n
0000659 561 or 562 n
0000660 504 or 504 n
0000669 561 and 564 l
0000670 565 and -655 n
0000680 530 or 530 n
0000688 690 or 574 n
0000689 -575 and -551 n
0000690 688 and 689 n

* p2r heater delete
14201000 delete
14202000 delete
*-----1-----1-----1
* control variable 114 re-define
*-----1-----1-----1
20511400 p2rheat sum 1.0 0.0 1
20511401 0.0 0.362 htmr 415100101
20511402 0.702464 htmr 415200101
20511403 1.26381 htmr 415200201
20511404 1.26381 htmr 415200301
20511405 0.649152 htmr 415200401
20511406 0.649152 htmr 415200501
20511407 0.534688 htmr 415200601
20511408 0.534688 htmr 415200701
20511409 0.273063 htmr 416200101
*-----1-----1-----1
* control variable 123 re-define
*-----1-----1-----1
20512300 p2r sum 1.0 0. 1
20512301 0.0 0.362 htmr 415100100
20512302 0.59522 htmr 415200100
20512303 1.07086 htmr 415200200
20512304 1.07086 htmr 415200300
20512305 0.550045 htmr 415200400
20512306 0.550045 htmr 415200500
20512307 0.453056 htmr 415200600
20512308 0.453056 htmr 415200700
20512309 0.150656 htmr 416200100
***** primary coolant pump 1
*****1350000 pcpump1 pump
1350101 0.0366 0.0 0.099 0.0 90.0 0.319
1350102 00000
1350108 130010000 0.0 0.0 0.0 000100
1350109 140000000 0.0 0.05 0.05 000100

```

```

1350200 0 14818100.1242890. 2463900.0 0.0
1350201 0 8.8943000 9.2942000 0.0
1350202 0 8.8928000 8.1177000 0.0
1350301 0 0 0 -1 0 509 0
1350302 369.000 .90178860 .315500 96.0000 500.600 1.4310000
1350303 613.6 0.0 207.0000 0.0040000 19.598000 0.0
1350310 0.0 0.0 0.0

```

```

*
***** single phase head curves
***** head curve no. 1

```

```

*---1---1---1---1---1---
1351100 1 1
1351101 0.000000e+00 1.403600e+00
1351102 1.906100e-01 1.363600e+00
1351103 3.896300e-01 1.318600e+00
1351104 5.939600e-01 1.232800e+00
1351105 7.902000e-01 1.133600e+00
1351106 1.000000e+00 1.000000e+00

```

```

* head curve no. 2
*---1---1---1---1---1---
1351200 1 2
1351201 0.000000e+00 -6.700000e-01
1351202 2.000000e-01 -5.000000e-01
1351203 4.000000e-01 -2.500000e-01
1351204 5.755400e-01 0.000000e+00
1351205 7.443200e-01 2.583000e-01
1351206 7.734800e-01 3.778000e-01
1351207 8.631300e-01 6.326000e-01
1351208 1.000000e+00 1.000000e+00

```

```

* head curve no. 3
*---1---1---1---1---1---
1351300 1 3
1351301 -1.000000e+00 2.472200e+00
1351302 -8.057400e-01 2.047400e+00
1351303 -6.069000e-01 1.831000e+00
1351304 -4.068300e-01 1.624000e+00
1351305 -2.001710e-01 1.470500e+00
1351306 0.000000e+00 1.403600e+00

```

```

* head curve no. 4
*---1---1---1---1---1---
1351400 1 4
1351401 -1.000000e+00 2.472200e+00
1351402 -8.229700e-01 1.996800e+00
1351403 -6.333200e-01 1.589700e+00
1351404 -4.553400e-01 1.327900e+00
1351405 -2.710900e-01 1.194900e+00
1351406 -1.771600e-01 1.060500e+00
1351407 -9.073000e-02 1.015600e+00
1351408 0.000000e+00 9.342790e-01

```

```

* head curve no. 5
*---1---1---1---1---1---
1351500 1 5
1351501 0.000000e+00 2.500000e-01
1351502 2.000000e-01 2.800000e-01
1351503 4.000000e-01 3.400000e-01
1351504 4.118000e-01 2.768000e-01
1351505 5.976300e-01 4.584000e-01
1351506 7.934670e-01 6.992000e-01
1351507 1.000000e+00 1.000000e+00

```

\*---1---1---1---1---1---1---1---

\* head curve no. 6

\*---1---1---1---1---1---1---1---

1351600	1	6
1351601	0.000000e+00	9.342790e-01
1351602	9.109900e-02	9.229000e-01
1351603	1.865090e-01	8.963000e-01
1351604	2.717620e-01	8.750000e-01
1351605	4.558720e-01	8.433000e-01
1351606	5.744060e-01	8.355000e-01
1351607	7.405760e-01	8.466000e-01
1351608	7.666190e-01	8.469000e-01
1351609	8.714710e-01	8.838000e-01
1351610	1.000000e+00	1.000000e+00

\*---1---1---1---1---1---1---1---

\* head curve no. 7

\*---1---1---1---1---1---1---1---

1351700	1	7
1351701	-1.000000e+00	-1.000000e+00
1351702	-8.000000e-01	-6.300000e-01
1351703	-6.000000e-01	-3.000000e-01
1351704	-4.000000e-01	-5.000000e-02
1351705	-2.000000e-01	1.500000e-01
1351706	0.000000e+00	2.500000e-01

\*---1---1---1---1---1---1---1---

\* head curve no. 8

\*---1---1---1---1---1---1---1---

1351800	1	8
1351801	-1.000000e+00	-1.000000e+00
1351802	-8.000000e-01	-9.700000e-01
1351803	-6.000000e-01	-9.500000e-01
1351804	-4.000000e-01	-8.800000e-01
1351805	-2.000000e-01	-8.000000e-01
1351806	0.000000e+00	-6.700000e-01

\*\*\*\*\* single phase torque data

\*\*\*\*\* torque curve no. 1

\*---1---1---1---1---1---1---1---

1351900	2	1
1351901	0.000000e+00	6.032000e-01
1351902	1.930000e-01	6.325000e-01
1351903	3.930000e-01	7.369000e-01
1351904	5.952000e-01	8.331000e-01
1351905	7.978200e-01	9.229000e-01
1351906	1.000000e+00	1.000000e+00

\*---1---1---1---1---1---1---1---

\* torque curve no. 2

\*---1---1---1---1---1---1---1---

1352000	2	2
1352001	0.000000e+00	-6.700000e-01
1352002	4.000000e-01	-2.500000e-01
1352003	5.000000e-01	1.500000e-01
1352004	7.372550e-01	5.265860e-01
1352005	7.680490e-01	6.065940e-01
1352006	8.672300e-01	7.436600e-01
1352007	1.000000e+00	1.000000e+00

\*---1---1---1---1---1---1---1---

\* torque curve no. 3

\*---1---1---1---1---1---1---1---

1352100	2	3
1352101	-1.000000e+00	1.984300e+00
1352102	-8.009600e-01	1.394000e+00
1352103	-6.063800e-01	1.097500e+00
1352104	-4.068600e-01	8.220000e-01

1352105 -1.992800e-01 6.648000e-01  
1352106 0.000000e+00 6.032000e-01

\*---1---1---1---1---1---1---1---

\* torque curve no. 4

\*---1---1---1---1---1---1---1---

1352200 2 4  
1352201 -1.000000e+00 1.984300e+00  
1352202 -8.223400e-01 1.830800e+00  
1352203 -6.337100e-01 1.682400e+00  
1352204 -4.585300e-01 1.557000e+00  
1352205 -2.670230e-01 1.436200e+00  
1352206 -1.761070e-01 1.387900e+00  
1352207 -8.931000e-02 1.348100e+00  
1352208 0.000000e+00 1.233610e+00

\*---1---1---1---1---1---1---1---

\* torque curve no. 5

\*---1---1---1---1---1---1---1---

1352300 2 5  
1352301 0.000000e+00 -4.500000e-01  
1352302 4.000000e-01 -2.500000e-01  
1352303 5.000000e-01 0.000000e+00  
1352304 1.000000e+00 3.569000e-01

\*---1---1---1---1---1---1---1---

\* torque curve no. 6

\*---1---1---1---1---1---1---1---

1352400 2 6  
1352401 0.000000e+00 1.233610e+00  
1352402 9.064300e-02 1.196500e+00  
1352403 1.885690e-01 1.109600e+00  
1352404 2.734700e-01 1.041600e+00  
1352405 4.586690e-01 8.958000e-01  
1352406 5.744800e-01 7.807000e-01  
1352407 7.381600e-01 6.134000e-01  
1352408 7.685200e-01 5.849000e-01  
1352409 8.700570e-01 4.877000e-01  
1352410 1.000000e+00 3.569000e-01

\*---1---1---1---1---1---1---1---

\* torque curve no. 7

\*---1---1---1---1---1---1---1---

1352500 2 7  
1352501 -1.000000e+00 -1.000000e+00  
1352502 -3.000000e-01 -9.000000e-01  
1352503 -1.000000e-01 -5.000000e-01  
1352504 0.000000e+00 -4.500000e-01

\*---1---1---1---1---1---1---1---

\* torque curve no. 8

\*---1---1---1---1---1---1---1---

1352600 2 8  
1352601 -1.000000e+00 -1.000000e+00  
1352602 -2.500000e-01 -9.000000e-01  
1352603 -8.000000e-02 -8.000000e-01  
1352604 0.000000e+00 -6.700000e-01

\*\*\*\*\* two - phase multiplier data from I9-1 test data  
\*\*\*\*\* head curve

\*---1---1---1---1---1---1---1---

1353000 0  
1353001 0.000000e+00 0.000000e+00  
1353002 2.000000e-02 2.000000e-02  
1353003 6.000000e-02 5.000000e-02  
1353004 1.000000e-01 1.000000e-01  
1353005 2.000000e-01 4.600000e-01  
1353006 2.400000e-01 8.000000e-01  
1353007 3.000000e-01 9.600000e-01

1353008	4.000000e-01	9.800000e-01
1353009	6.000000e-01	9.700000e-01
1353010	8.000000e-01	9.000000e-01
1353011	9.000000e-01	8.000000e-01
1353012	9.600000e-01	5.000000e-01
1353013	1.000000e+00	0.000000e+00

\* ---1---1---1---1---1---1---1---  
 \* torque curve  
 \* ---1---1---1---1---1---1---1---

1353100	0	
1353101	0.000000e+00	0.000000e+00
1353102	1.250000e-01	7.000000e-02
1353103	1.650000e-01	1.250000e-01
1353104	2.400000e-01	5.600000e-01
1353105	8.000000e-01	5.600000e-01
1353106	9.600000e-01	4.500000e-01
1353107	1.000000e+00	0.000000e+00

\*\*\*\*\* pump 2-phase difference data  
 \*\*\*\*\* head curve no. 1

1354100	1	1
1354101	0.000000e+00	0.000000e+00
1354102	1.000000e-01	8.300000e-01
1354103	2.000000e-01	1.090000e+00
1354104	5.000000e-01	1.020000e+00
1354105	7.000000e-01	1.010000e+00
1354106	9.000000e-01	9.400000e-01
1354107	1.000000e+00	1.000000e+00

\* ---1---1---1---1---1---1---1---  
 \* head curve no. 2  
 \* ---1---1---1---1---1---1---1---

1354200	1	2
1354201	0.000000e+00	0.000000e+00
1354202	1.000000e-01	-4.000000e-02
1354203	2.000000e-01	0.000000e+00
1354204	3.000000e-01	1.000000e-01
1354205	4.000000e-01	2.100000e-01
1354206	8.000000e-01	6.700000e-01
1354207	9.000000e-01	8.000000e-01
1354208	1.000000e+00	1.000000e+00

\* ---1---1---1---1---1---1---1---  
 \* head curve no. 3  
 \* ---1---1---1---1---1---1---1---

1354300	1	3
1354301	-1.000000e+00	-1.160000e+00
1354302	-9.000000e-01	-1.240000e+00
1354303	-8.000000e-01	-1.770000e+00
1354304	-7.000000e-01	-2.360000e+00
1354305	-6.000000e-01	-2.790000e+00
1354306	-5.000000e-01	-2.910000e+00
1354307	-4.000000e-01	-2.670000e+00
1354308	-2.500000e-01	-1.690000e+00
1354309	-1.000000e-01	-5.000000e-01
1354310	0.000000e+00	0.000000e+00

\* ---1---1---1---1---1---1---1---  
 \* head curve no. 4  
 \* ---1---1---1---1---1---1---1---

1354400	1	4
1354401	-1.000000e+00	-1.160000e+00
1354402	-9.000000e-01	-7.800000e-01
1354403	-8.000000e-01	-5.000000e-01
1354404	-7.000000e-01	-3.100000e-01
1354405	-6.000000e-01	-1.700000e-01

1354406	-5.000000e-01	-8.000000e-02
1354407	-3.500000e-01	0.000000e+00
1354408	-2.000000e-01	5.000000e-02
1354409	-1.000000e-01	8.000000e-02
1354410	0.000000e+00	1.100000e-01
*---1---1---1---1---1---1---		
* head curve no. 5		
*---1---1---1---1---1---1---		
1354500	1	5
1354501	0.000000e+00	0.000000e+00
1354502	2.000000e-01	-3.400000e-01
1354503	4.000000e-01	-6.500000e-01
1354504	6.000000e-01	-9.300000e-01
1354505	8.000000e-01	-1.190000e+00
1354506	1.000000e+00	-1.470000e+00
*---1---1---1---1---1---1---		
* head curve no. 6		
*---1---1---1---1---1---1---		
1354600	1	6
1354601	0.000000e+00	1.100000e-01
1354602	1.000000e-01	1.300000e-01
1354603	2.500000e-01	1.500000e-01
1354604	4.000000e-01	1.300000e-01
1354605	5.000000e-01	7.000000e-02
1354606	6.000000e-01	-4.000000e-02
1354607	7.000000e-01	-2.300000e-01
1354608	8.000000e-01	-5.100000e-01
1354609	9.000000e-01	-9.100000e-01
1354610	1.000000e+00	-1.470000e+00
*---1---1---1---1---1---1---		
* head curve no. 7		
*---1---1---1---1---1---1---		
1354700	1	7
1354701	-1.000000e+00	0.000000e+00
1354702	0.000000e+00	0.000000e+00
*---1---1---1---1---1---1---		
* head curve no. 8		
*---1---1---1---1---1---1---		
1354800	1	8
1354801	-1.000000e+00	0.000000e+00
1354802	0.000000e+00	0.000000e+00
*---1---1---1---1---1---1---		
* torque curve no. 1		
*---1---1---1---1---1---1---		
1354900	2	1
1354901	0.000000e+00	6.032000e-01
1354902	1.930000e-01	6.325000e-01
1354903	3.930000e-01	7.369000e-01
1354904	5.952000e-01	8.331000e-01
1354905	7.978200e-01	9.229000e-01
1354906	1.000000e+00	1.000000e+00
*---1---1---1---1---1---1---		
* torque curve no. 2		
*---1---1---1---1---1---1---		
1355000	2	2
1355001	0.000000e+00	-6.700000e-01
1355002	4.000000e-01	-2.500000e-01
1355003	5.000000e-01	1.500000e-01
1355004	7.372500e-01	5.265860e-01
1355005	7.680490e-01	6.065940e-01
1355006	8.672300e-01	7.436600e-01
1355007	1.000000e+00	1.000000e+00
*---1---1---1---1---1---1---		

\* torque curve no. 3  
 \*---1---1---1---1---1---1---  
 1355100 2 3  
 1355101 -1.000000e+00 1.984300e+00  
 1355102 -8.009600e-01 1.394000e+00  
 1355103 -6.063800e-01 1.097500e+00  
 1355104 -4.068600e-01 8.220000e-01  
 1355105 -1.992800e-01 6.648000e-01  
 1355106 0.000000e+00 6.032000e-01  
 \*---1---1---1---1---1---1---

\* torque curve no. 4  
 \*---1---1---1---1---1---1---  
 1355200 2 4  
 1355201 -1.000000e+00 1.984300e+00  
 1355202 -8.223400e-01 1.830800e+00  
 1355203 -6.337100e-01 1.682400e+00  
 1355204 -4.585300e-01 1.557000e+00  
 1355205 -2.670230e-01 1.436200e+00  
 1355206 -1.761070e-01 1.387900e+00  
 1355207 -8.931000e-02 1.348100e+00  
 1355208 0.000000e+00 1.233610e+00  
 \*---1---1---1---1---1---1---

\* torque curve no. 5  
 \*---1---1---1---1---1---1---  
 1355300 2 5  
 1355301 0.000000e+00 -4.500000e-01  
 1355302 4.000000e-01 -2.500000e-01  
 1355303 5.000000e-01 0.000000e+00  
 1355304 1.000000e+00 3.569000e-01  
 \*---1---1---1---1---1---1---

\* torque curve no. 6  
 \*---1---1---1---1---1---1---  
 1355400 2 6  
 1355401 0.000000e+00 1.233610e+00  
 1355402 9.064300e-02 1.196500e+00  
 1355403 1.885690e-01 1.109600e+00  
 1355404 2.734700e-01 1.041600e+00  
 1355405 4.586690e-01 8.958000e-01  
 1355406 5.744800e-01 7.807000e-01  
 1355407 7.381600e-01 6.134000e-01  
 1355408 7.685200e-01 5.849000e-01  
 1355409 8.700570e-01 4.877000e-01  
 1355410 1.000000e+00 3.569000e-01  
 \*---1---1---1---1---1---1---

\* torque curve no. 7  
 \*---1---1---1---1---1---1---  
 1355500 2 7  
 1355501 -1.000000e+00 -1.000000e+00  
 1355502 -3.000000e-01 -9.000000e-01  
 1355503 -1.000000e-01 -5.000000e-01  
 1355504 0.000000e+00 -4.500000e-01  
 \*---1---1---1---1---1---1---

\* torque curve no. 8  
 \*---1---1---1---1---1---1---  
 1355600 2 8  
 1355601 -1.000000e+00 -1.000000e+00  
 1355602 -2.500000e-01 -9.000000e-01  
 1355603 -8.000000e-02 -8.000000e-01  
 1355604 0.000000e+00 -6.700000e-01

\*\*\*\*\* pcp1 pump velocity table \*\*\*\*\*  
 \*\*\*\*\*1356100 536 \*\*\*\*\*  
 1356101 0.0 0.0  
 1356102 1.0 220.

```

***** primary coolant pump 2
*****1650000 pcpump2 pump
1650101 0.0366 0.0 0.099 0.0 90.0 0.319
1650102 00000
1650108 160010000 0.0 0.0 0.0 000100
1650109 170000000 0.0 0.1 0.1 000100
1650200 0 14832700.1242890. 2463590.0 0.0
1650201 0 8.4974000 8.8872000 0.0
1650202 0 8.4959000 6.6507000 0.0
1650301 135 135 135 -1 135 509 0
1650302 369.00000 .89699187 .31550000 96.000000 500.60000 1.431
1650303 613.6 0.0 207.433 0.004 19.5980 0.0
1650310 0.0 0.0 0.0
*~ ---1---1---1---1---1---1---1---
* spray valve
*~ ---1---1---1---1---1---1---1---
4070000 sprviv valve
4070101 406010000 420010000 3.3451e-4 1.0 1.0 000100
4070201 0 .000000 .000000 0.0
4070300 trpviv
4070301 690
*~ ---1---1---1---1---1---1---1---
* air cooled condenser
*~ ---1---1---1---1---1---1---1---
5470000 condens tmdpviv
5470101 0.21677 17.67 0.0 0.0 0.0 0.0
5470102 4.e-5 0.0 00000
5470200 1 680
5470201 0.0 559.15 0.999
5470202 18000. 334.15 0.999
*~ ---1---1---1---1---1---1---1---
* aux feed water
*~ ---1---1---1---1---1---1---1---
5480000 auxfeed tmdpviv
5480101 553000000 510000000 0.10
5480200 1 655
5480201 -1.0 0.0 0.0 0.0
5480202 0.0 0.0 0.0 0.0
5480203 0.0 2.5207 0.0 0.0
*~ ---1---1---1---1---1---1---1---
* main feed water valve
*~ ---1---1---1---1---1---1---1---
5600000 mnfeed tmdpviv
5600101 545000000 510000000 0.05
5600200 1 656
5600201 0.0 26.533 26.533 0.0
5600202 0.0 0.0 0.0 0.0
*****
* core collapsed liquid level
*****20255000 normarea 0 1.0 1.0
*20255001 0.0 9.25e-3
*20255002 9.25e-3 9.25e-3
*20255003 1.0 1.0
*****
* reactor kinetics data
*
*****30000000 point separabl
30000001 gamma-ac 49.6e+6 0.0 348.43 1.0 0.556
30000002 ans79-1
***** delayed neutron constants
*****30000101 0.0349 0.01275
30000102 0.2035 0.03177
30000103 0.1848 0.1181

```



```

30000104 0.4046 0.3160
30000105 0.1401 1.402
30000106 0.0321 3.914
***** power history
*****30000401 4.89e+7 70. hr
***** reactivity curve numbers
*****30000011 609
***** moderator density reactivity table
*****30000501 0.62626e+3 -4.4769
30000502 0.66396e+3 -3.2923
30000503 0.71617e+3 -1.5692
30000504 0.76112e+3 -0.1692
30000505 0.76837e+3 0.04615
30000506 0.79157e+3 0.6923
30000507 0.81188e+3 1.2398
30000508 0.86263e+3 2.2415
30000509 0.93804e+3 3.9231
30000510 0.99749e+3 5.1077
***** doppler reactivity table
*****30000601 293.16 1.375
30000602 338.72 1.125
30000603 422.05 0.682
30000604 477.60 0.419
30000605 505.38 0.274
30000606 570.72 0.000
30000607 588.72 -0.075
30000608 695.83 -0.526
30000609 922.05 -1.386
30000610 1310.94 -2.543
30000611 1810.94 -3.865
30000612 2088.72 -4.502
30000613 2499.83 -5.392
30000614 3027.60 -6.417
***** volume weighting factors
***** moderator temperature feedback
*****30000701 230010000 0 0.31493 0.0
30000702 230020000 0 0.31493 0.0
30000703 230030000 0 0.37014 0.0
***** doppler feedback
*****30000801 2300001 0 0.43153 0.0
30000802 2300002 0 0.51686 0.0
30000803 2300003 0 0.05161 0.0
*---1---1---1---1---1---1---1---
* scram reactivity data
*---1---1---1---1---1---1---1---
20260900 "react " 609
20260901 0.0 0.0
20260902 0.5 -0.5
20260903 0.59 -3.13
20260904 0.65 -3.95
20260905 0.75 -6.27
20260906 0.83 -8.72
20260907 0.90 -12.00
20260908 0.97 -17.12
20260909 1.125 -20.67
20260910 1.213 -22.10
20260911 1.3 -22.78
20260912 1.4 -23.17
20260913 1.6 -23.32
20260914 60.0 -23.32

```



**BIBLIOGRAPHIC DATA SHEET**

(See instructions on the reverse)

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A. Calvo, NRC Project Manager

11. ABSTRACT (200 words or less)

The purpose of this report is to assess the capability of the RELAP5/MOD3.3Beta computer code to simulate thermal-hydraulic behavior associated with the LOFT Experiment L9-1/L3-3. The Experiment L9-1/L3-3 was a simulation of the total loss-of-feedwater accident and its recovery modes. Experiment L9-1 simulated a loss-of-feedwater accident with delayed reactor scram and no auxiliary feedwater injection. The loss-of-feedwater accident led to a loss-of-coolant accident through the PORV cycling operation.

Generally, the RELAP5/MOD3.3Beta calculation results were in good agreement with the L9-1 experimental data. The discrepancies between the calculation and the experiment were also identified in the temperature behaviors of the SG secondary side after dryout of the SG. However, these discrepancies were not considered to be significant, since the SG was in a de-coupled state from the PCS after the dryout of the SG secondary side.

Experiment L3-3 simulated two recovery modes from the loss-of-feedwater accident L9-1 without the aid of the emergency core coolant system. The first recovery mode consisted of turning off the primary coolant pumps and latching open the PORV to depressurize the primary system. The second mode consisted of refilling the SG to restore the secondary heat sink and removing decay heat through the feed-and-bleed operation using the secondary side of the SG.

12. KEY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)

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