

FPL Energy Seabrook Station P.O. Box 300 Seabrook, NH 03874 (603) 773-7000

Xpril 30, 2008

Docket No. 50-443 SBK-L-08073

U.S. Nuclear Regulatory Commission Attn.: Document Control Desk Washington, DC 20555-0001

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Pursuant to 10CFR 50.36(a)(2) and Technical Specification 6.8.1.4, FPL Energy Seabrook, LLC submits the Annual Radioactive Effluent Release Report for 2007. A copy of the Offsite Dose Calculation Manual (ODCM) is also provided pursuant to Technical Specification 6.13.c. A summary of the changes to the ODCM is included in Enclosure 1, Appendix A.

The following information is provided in the enclosures:

Enclosure 1	Effluent release data as required by Regulatory Guide 1.21
Enclosure 2	Joint frequency distributions of wind speed, wind direction and
	atmospheric stability
Enclosure 3	Radiation dose assessment
Enclosure 4	Offsite Dose Calculation Manual (ODCM), Revision 31

Should you have any questions regarding this letter, please contact William T. Cash, Chemistry Department Manager, at (603) 773-7315.

Very truly yours,

FPL Energy Seabrook, LLC

Gene St. Pierre Site Vice President

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U.S. Nuclear Regulatory Commission SBK-L-08073/ Page 2

1

cc: S.J. Collins, NRC Region I Administrator G.E. Miller, NRC Project Manager, Project Directorate I-2 W.J. Raymond, NRC Senior Resident Inspector Robert A. Oliveira, ANI

ENCLOSURE 1 TO SBK-L-08073

Effluent Release Data as Required by Regulatory Guide 1.21

EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT Supplemental Information 2007

Facility: Seabrook Station Unit 1

Licensee: FPL Energy Seabrook, LLC

- 1. <u>Regulatory Limits</u>
 - A. Gaseous Effluents
 - a. 5.0 mrad per quarter gamma air dose.
 - b. 10.0 mrad per quarter beta air dose.
 - c. 7.5 mrem per quarter to any organ.
 - B. Liquid Effluents
 - a. 1.5 mrem per quarter total body.
 - b. 5.0 mrem per quarter any organ.
 - c. $2.0E-04 \mu Ci/ml$ dissolved or entrained gas.

2. <u>Effluent Concentration Limits</u>

Provide the ECL's used in determining allowable release rates or concentrations.

- a. Fission and activation gases: 10 ECL
- b. Iodines: 10 ECL
- c. Particulates, half-lives >8 days: 10 ECL
- d. Liquid Effluents: 10 ECL
- 3. <u>Average Energy</u>

· + - -

Not applicable

4. Measurements and Approximations of Total Radioactivity

Provide the methods used to measure or approximate the total radioactivity in effluents and the methods used to determine radionuclide composition.

- A. Fission and activation gases: Determined by gamma spectroscopy. Total error is based on stack flow error, analytical error, and calculated sampling error.
- B. Iodines: Determined by collection on charcoal with subsequent gamma spectroscopy analysis. Total error is based on stack flow error, analytical error, and calculated sampling error.

- C. Particulates: Determined by collection on fixed filter with subsequent gamma spectroscopy analysis. Strontium is determined by composite analysis of filters by liquid scintillation, gross alpha by proportional counter and iron 55 by liquid scintillation. Total error is based on stack flow error, analytical error, and calculated sampling error.
- D. Liquid Effluents: Determined by gamma spectroscopy. A composite sample is analyzed for strontium by liquid scintillation, tritium by liquid scintillation, gross alpha by proportional counter and iron 55 by liquid scintillation. Total error is based on the volume discharge error and analytical error.
- E. ND: None Detected or No Detectable Activity

5. <u>Batch Releases</u>

Provide the following information relating to batch releases of radioactive materials in liquid and gaseous effluents.

- A. Liquid
 - a. Number of batch releases: 146
 - b. Total time for batch releases: 30696 minutes
 - c. Maximum time period for batch release: 458 minutes
 - d. Average time period for batch release: 210 minutes
 - e. Minimum time period for batch release: 23 minutes
 - f. Average stream flow during periods of release of effluents into a flowing stream: 1.69E+06 liters per minute
- B. Gaseous
 - a. Number of batch releases: 35
 - b. Total time for batch releases: 4927 minutes
 - c. Maximum time period for batch release: 2194 minutes
 - d. Average time period for batch release: 259 minutes
 - e. Minimum time period for batch release: 1 minute

6. Abnormal Releases

- A. Liquid
 - a. Number of releases: 0
 - b. Total activity released: N/A
- B. Gaseous
 - a. Number of releases: 0
 - b. Total activity released: N/A

TABLE 1A

EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT 2007

GASEOUS EFFLUENTS-SUMMATION OF ALL RELEASES

	Unit	Quarter 1	Quarter 2	Quarter 3	Quarter 4	Est. Total Error, %
A. Fission and activation gases				·		
1. Total releases	Ci	3.17E-02	2.85E-03	2.30E-03	1.03E-02	1.70E+01
2. Average release rate for period	uCi/sec	4.08E-03	3.62E-04	2.89E-04	1.30E-03	
3. Percent of applicable Technical Specification limit	%	7.48E-04	1.22E-04	1.24E-04	3.00E-04	
B. lodines						
1. Total release	Ci	ND	ND	ND	ND	1.50E+01
2. Average release rate for period	uCi/sec	N/A	N/A	N/A	N/A	
3. Percent of applicable Technical Specification limit	%	N/A	N/A	N/A	N/A	
C. Particulates						
1. Total release	Ci	ND	ND	ND	ND	1.80E+01
2. Average release rate for period	uCi/sec	N/A	N/A	N/A	N/A	
3. Percent of applicable Technical Specification limit	%	N/A	N/A	N/A	N/A	
4. Total alpha radioactivity	Ci	ND	ND	ND	ND	
D. Tritium			·	r		
1. Total release	Ci	3.58E+01	4.79E+01	1.54E+01	1.88E+01	1.60E+01
2. Average release rate for period	uCi/sec	4.60E+00	6.09E+00	1.94E+00	2.37E+00	
3. Percent of applicable Technical Specification limit	%	4.80E-01	6.53E-01	2.08E-01	2.52E-01	

TABLE 1B

EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2007) GASEOUS EFFLUENTS-ELEVATED RELEASES

BATCH

Aluelides Released	11-14	Quarter	Quarter	Quarter	Quarter
Nuclides Released		1	2	3	4

1. Fission and activation gases

			10.000		
argon-41	Ci	3.14E-02	2.83E-03	2.19E-03	8.20E-03
krypton-85	Ci	ND	ND	ND	ND
krypton-85m	Ci	1.06E-04	ND	ND	ND
krypton-87	Ci	ND	ND	ND	ND
krypton-88	Ci	ND	ND	ND	ND
xenon-131m	Ci	ND	ND	ND	ND
xenon-133	Ci	1.54E-05	2.21E-05	ND	1.95E-03
xenon-133m	Ci	ND	ND	ND	ND
xenon-135	Ci	1.71E-04	ND	1.07E-04	1.51E-04
xenon-135m	Ci	ND	ND	ND	ND
xenon-138	Ci	ND	ND	7.73E-04	2.61E-03
	Ci				
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	3.17E-02	2.85E-03	3.07E-03	1.29E-02

2. Iodines

iodine-131	Ci	ND	ND	ND	ND
iodine-133	Ci	ND	ND	ND	ND
iodine-135	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

3. Particulates

strontium-89	Ci	ND	ND	ND	ND
strontium-90	Ci	ND	ND	ND	ND
cesium-134	Ci	ND	ND	ND	ND
cesium-137	Ci	ND	ND	ND	ND
barium-lanthanum-140	Ci	ND	ND	ND	ND
	Ci				
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

TABLE 1B

EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2007) GASEOUS EFFLUENTS-ELEVATED RELEASES

CONTINUOUS

Nuclides Released	Unit	Quarter	Quarter	Quarter	Quarter
	Unit	1	2	3	4

1. Fission and activation gases

argon-41	Ci	ND	ND	ND	ND
krypton-85	Ci	ND	ND	ND	ND
krypton-85m	Ci	ND	ND	ND	ND
krypton-87	Ci	ND	ND	ND	ND
krypton-88	Ci	ND	ND	ND	ND
xenon-131m	Ci	ND	ND	ND	ND
xenon-133	Ci	ND	ND	ND	ND
xenon-133m	Ci	ND	ND	ND	ND
xenon-135	Ci	ND	ND	ND	ND
xenon-135m	Ci	ND	ND	ND	ND
xenon-138	Ci	ND	ND	ND	ND
	Ci				
	Ci				
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

2. Iodines

iodine-131	Ci	ND	ND	ND	ND
iodine-133	Ci	ND	ND	ND	ND
iodine-135	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

3. Particulates

strontium-89	Ci	ND	ND	ND	ND
strontium-90	Ci	ND	ND	ND	ND
cesium-134	Ci	ND	ND	ND	ND
cesium-137	Ci	ND	ND	ND	ND
barium-lanthanum-140	Ci	ND	ND	ND	ND
cobalt-58	Ci	ND	ND	ND	ND
cobalt-60	Ci	ND	ND	ND	ND
chromium-51	· Ci	ND	ND	ND	ND
manganese-54	Ci	ND	ND	ND	ND
niobium-95	Ci	ND	ND	ND	ND
iron-59	Ci	ND	ND	ND	ND
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

TABLE 1C

EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2007) GASEOUS EFFLUENTS-GROUND LEVEL RELEASES

BATCH

Nuclides Released	Linit	Quarter	Quarter	Quarter	Quarter
	Unit	1	2	3	4

1. Fission and activation gases

argon-41	Ci	ND	ND	ND	ND
krypton-85	Ci	ND	ND	ND	ND
krypton-85m	Ci	ND	ND	ND	ND
krypton-87	Ci	ND	ND	ND	ND
krypton-88	Ci	ND	ND	ND	ND
xenon-131m	Ci	ND	ND	ND	ND
xenon-133m	Ci	ND	ND	ND	ND
xenon-133	Ci	ND	ND	ND	ND
xenon-135	Ci	ND	ND	ND	ND
xenon-135m	Ci	ND	ND	ND	ND
xenon-138	Ci	ND	ND	ND	ND
	Ci				
	Ci				
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

2. Iodines

iodine-131	Ci	ND	ND	ND	ND
iodine-132	Ci	ND	ND	ND	ND
iodine-133	Ci	ND	ND	ND	ND
iodine-135	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

3. Particu	llates				
strontium-89	Ci	ND	ND	ND	ND
strontium-90	Ci	ND	ND	ND	ND
cesium-134	Ci	ND	ND	ND	ND
cesium-136	Ci	ND	ND	ND	ND
cesium-137	Ci	ND	ND	ND	ND
barium-lanthanum-140	Ci	ND	ND	ND	ND
cobalt-57	Ci	ND	ND	ND	ND
cobalt-58	Ci	ND	ND	ND	ND
cobalt-60	Ci	ND	ND	ND	ND
manganese-54	Ci	ND	ND	ND	ND
iron-59	Ci	ND	ND	ND	ND
niobium/zirconium-95	Ci	ND	ND	ND	ND
chromium-51	Ci	ND	ND	ND	ND
technetium-99m	Ci	ND	ND	ND	ND
bromine-82	Ci	ND	ND	ND	ND
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	0.00F+00	0.00F+00	0.00E+00	0.00E+00

TABLE 1C

GASEOUS EFFLUENTS-GROUND LEVEL RELEASES

CONTINUOUS

Nuslides Balassed	l Init	Quarter	Quarter	Quarter	Quarter
	Unit	1	2	3	4

1. Fission and activation gases

argon-41	Ci	ND	ND	ND	ND
krypton-85	Ci	ND	ND	ND	ND
krypton-85m	Ci	ND	ND	ND	ND
krypton-87	Ci	ND	ND	ND	ND
krypton-88	Ci	ND	ND	ND	ND
xenon-133	Ci	ND	ND	ND	ND
xenon-135	Ci	ND	ND	ND	ND
xenon-135m	Ci	ND	ND	ND	ND
xenon-138	Ci	ND	ND	ND	ND
	Ci				
	Ci				
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

2. Iodines

iodine-131	Ci	ND	ND	ND	ND
iodine-133	Ci	ND	ND	ND	ND
	Ci				
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

3. Particu	lates				
strontium-89	Ci	ND	ND	ND	ND
strontium-90	Ci	ND	ND	ND	ND
cesium-134	Ci	ND	ND	ND	ND
cesium-136	Ci	ND	ND	ND	ND
cesium-137	Ci	ND	ND	ND	ND
barium-lanthanum-140	Ci	ND	ND	ND	ND
cobalt-58	Ci	ND	ND	ND	ND
cobalt-60	Ci	ND	ND	ND	ND
chromium-51	Ci	ND	ND	ND	ND
unidentified	Ci	ND	ND	ND	ND
Total for period	Ci	0.00E+00	0.00E+00	0.00E+00	0.00E+00

TABLE 2A

EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT 2007

LIQUID EFFLUENTS-SUMMATION OF ALL RELEASES

Unit Quarter 1 Quarter 2 Quarter 3 Quarter 4 Error, %

A. Fission and activation products

1. Total releases	Ci	1.09E-02	5.28E-03	2.80E-03	3.18E-03	6.00E+00
 Average diluted concentration during period 	uCi/ml	2.56E-11	1.30E-11	6.03E-12	7.07E-12	
3. Percent of applicable limit	%	9.73E-03	7.27E-03	2.99E-03	1.05E-02	

B. Tritium

1. Total release	Ci	6.41E+01	1.60E+02	1.62E+01	2.41E+02	8.00E+00
2. Average diluted concentration during period	uCi/ml	1.50E-07	3.95E-07	3.49E-08	5.36E-07	
3. Percent of applicable limit	%	1.40E-02	8.04E-03	3.52E-03	5.68E-03	

C. Dissolved and entrained gases

1. Total release	Ci	ND	ND	ND	ND	1.90E+01
2. Average diluted concentration during period	uCi/ml	N/A	N/A	N/A	N/A	
3. Percent of applicable limit	%	N/A	N/A	N/A	N/A	

D. Gross alpha radioactivity

1. Total release Ci ND ND ND 1.00E+0	1. Total release	Ci	ND	ND	ND	ND	1.00E+0 ⁻
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E. Volume of waste released (prior to dilution)	liters	1.67E+07	1.38E+07	1.71E+07	2.07E+07	1.30E+00
F. Volume of dilution water used during period	liters	4.26E+11	4.05E+11	4.64E+11	4.50E+11	9.00E+00

TABLE 2B EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT 2007 LIQUID EFFLUENTS

BATCH MODE

		•			
Nuclides Released	Unit	Quarter 1	Quarter 2	Quarter 3	Quarter 4
strontium-89	Ci	ND	ND	ND	ND
strontium-90	Ci	ND	ND	ND	ND
cesium-134	Ci	ND	ND	ND	ND
cesium-137	Ci	1.06E-05	ND	1.43E-06	ND
iodine-131	Ci	ND	ND	• ND	ND
iodine-133	Ci	ND	ND	ND	ND
cobalt-57	Ci	ND	ND	1.24E-06	1.32E-05
cobalt-58	Ci	1.26E-03	1.75E-04	3.55E-04	3.61E-04
cobalt-60	Ci	2.47E-04	6.64E-05	2.96E-04	1.29E-03
chromium-51	Ci	ND	ND	ND	ND
iron-55	Ci	8.60E-03	4.81E-03	2.06E-03	1.10E-03
iron-59	Ci	ND	ND	ND	ND
zinc-65	Ci	ND	ND	ND	ND
manganese-54	Ci	3.91E-05	ND	1.68E-05	3.66E-05
zirconium-niobium-95	Ci	ND	ND	ND	ND
molybdenum-99	Ci	ND	ND	ND	ND
technetium-99m	Ci	ND	ND	ND	ND
silver-110m	Ci	ND	ND	ND	ND
barium-lanthanum-140	Ci	ND	ND	ND	ND
cerium-141	Ci	ND	ND	ND	ND
antimony-124	Ci	ND	ND	ND	ND
antimony-125	Ci	7.41E-04	2.32E-04	7.31E-05	3.81E-04
antimony-126	Ci	ND	ND	ND	ND
niobium-97	Ci	ND	ND	ND	ND
tin-117m	Ci	ND	ND	ND	ND
sodium-24	Ci	ND	ND	ND	ND
Tellurium-129m	Ci	ND	ND	ND	ND
Tellurium-132	Ci	ND	ND	ND	ND
unidentified	Ci	ND	ND	ND	ND
· · · · · · · · · · · · · · · · · · ·	•				
Total for period(above)	Ci	1.09E-02	5.28E-03	2.80E-03	3.18E-03
xenon-133	Ci	ND			ND ND
i xenon-135	I Ci	I ND	I ND	I ND	I ND

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TABLE 2B EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT 2007 LIQUID EFFLUENTS

CONTINUOUS MODE

Nuclides Released	Unit	Quarter 1	Quarter 2	Quarter 3	Quarter 4
strontium-89	Ci	ND	ND	ND	ND
strontium-90	Ci	ND	ND	ND	ND
cesium-134	Ci	ND	ND	ND	ND
cesium-137	Ci	ND .	ND	ND	ND
iodine-131	Ci	ND	ND	ND	ND
iodine-133	Ci	ND	ND	ND	ND
cobalt-58	Ci	ND	ND	ND	ND
cobalt-60	Ci	ND	ND	ND	ND
iron-55	Ci	ND	ND	ND	ND
iron-59	Ci	ND	ND	ND	ND
zinc-65	Ci	ND	ND	ND	ND
manganese-54	Ci	ND	ND	ND	ND
chromium-51	Ci	ND	ND	ND	ND
zirconium-niobium-95	Ci	ND	ND	ND	ND
molybdenum-99	Ci	ND	ND	ND	- ND
technetium-99m	Ci	ND	ND	ND	ND
barium-lanthanum-140	Ci	ND	ND	ND	ND
cerium-141	Ci	ND	ND	ND	ND
unidentified	Ci	ND	ND	ND	ND

Total for period(above) Ci 0.00E+00 0.00E+00 0.00E+00 0.00E+00

xenon-131m	Ci	ND	ND	ND	ND
xenon-133m	Ci	ND	ND	ND	ND
xenon-133	Ci	ND	ND	ND	ND
xenon-135	Ci	ND	ND	ND	ND

EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT 2007 SOLID WASTE AND IRRADIATED FUEL SHIPMENTS

A. SOLID WASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL (Not irradiated fuel)

1. Type of waste	Unit	1 year Period	Est. Total Error, %
a. Spent resins, filter sludges, evaporator Bottoms, etc.	m ³ Ci	2.76E-01 4.12E+01	2.50E+01
b. Dry compressible waste, contaminated Equip, etc.	m ³ Ci	5.82E+01 2:30E+03	2.50E+01
c. Irradiated components, control Rods, etc.	m ³ Ci	N/A	N/A
d. Other (describe)	m ³ Ci	N/A	N/A

2. Estimate of major nuclide composition (by type of waste)

a.	Ni-63	%	7.09E+01
	Fe-55	%	1.34E+01
	Co-60.	%	6.63E+00
	Co-58	%	5.65E+00
	Mn-54	%	1.46E+00
	Cs-137	%	8.59E-01
	Sb-125	%	5.44E-01
	Co-57	%	3.45E-01
	H-3	%	1.41E-01
	Cs-134	%	1.26E-01
	Nb-94	%	4.71E-03
b.	Fe-55	%	4.96E+01
	Ni-63	%	2.15E+01
	H-3	%	1.50E+01
	Co-60	%	7.74E+00
	Co-58	%	4.94E+00
	Mn-54	%	3.11E-01
	Cs-137	%	2.43E-01
	Sb-125	%	2.34E-01
	Nb-95	%	1.25E-01
	Zr-95	%	1.05E-01
	Co-57	%	7.87E-02
	Cs-134	%	3.97E-02
	Tc-99	%	3.94E-02
c.	N/A	%	N/A
			······································
d.	N/A	%	<u>N/A</u>

3. Solid Waste Disposition

Number of Shipments	Waste Class	Container Type	Solidification Agent	Mode of Transportation	Destination
3	A	General	N/A	Truck	Duratek
	•	Design			Kingston, TN
2	Α	General	N/A	Truck	Duratek
		Design			Oak Ridge, TN
3	A	General	N/A	Truck	EnergySolutions
		Design			Clive, UT
2	В	Type A	N/A	Truck	Studsvik
					Erwin, TN

B. IRRADIATED FUEL SHIPMENTS (Disposition)

Number of Shipments	Mode of Transportation	Destination
N/A	N/A	N/A

C. REVIEW AND APPROVAL



3/26/08 3/29/08 **4/24/05** Date: Date: Date:

LIST OF APPENDICES

Appendix	Title
Α	Offsite Dose Calculation Manual
В	Process Control Program
С	Liquid Holdup Tanks
D	Radwaste Treatment Systems
Е	Unplanned Releases

Appendix A

Offsite Dose Calculation Manual

Requirement: Technical Specification 6.13.2c requires that licensee initiated changes to the Offsite Dose Calculation Manual be submitted to the Commission in the Annual Radioactive Effluent Release Report for the period in which the change(s) was made effective. Include in this changes to the Radiological Environmental Program in accordance with Offsite Dose Calculation Manual (ODCM)-C.9.1.1 and -C.9.2.1.

Response: The ODCM was changed in 2007.

The Change added a missing number "1" in Table A.5.2-1, item 4.c for minimum channels operable.

Appendix B

Process Control Program

Requirement: Technical Specification 6.12.2a requires that licensee initiated changes to the Process Control Program be submitted to the Commission in the Annual Radioactive Effluent Release Report for the period in which the change(s) was made.

Response: No changes were made to the process control program in 2007.

Appendix C

Liquid Holdup Tanks

Requirement: Technical Specification 3.11.1.4 limits the quantity of radioactive material contained in any outside temporary tank. With the quantity of radioactive material in any outside temporary tank exceeding the limits of Technical Specification 3.11.1.4, a description of the events leading to this condition is required in the next Annual Effluent Release Report in accordance with Tech. Spec. 6.8.1.4.

Response: From January 1, 2007 to December 31, 2007, there was no radioactive material stored in any temporary outdoor tank that exceeded the limits of T. S. 3.11.1.4.

Appendix D

Radwaste Treatment Systems

Requirement: Technical Specification 6.14.1a requires that licensee initiated changes to the Radwaste Treatment Systems (liquid, gaseous, and solid) be submitted to the Commission in the Annual Radioactive Effluent Release Report for the period in which the change was made.

Response: For 2007, FPL Energy Seabrook LLC, will submit any changes to the Radwaste Treatment Systems (liquid, gaseous and solid) as part of the FSAR update.

Appendix E

Unplanned Releases

Requirement: Technical Specification 6.8.1.4 requires a list and description of unplanned releases from the site to UNRESTRICTED AREAS of radioactive materials in gaseous and liquid effluents made during the reporting period.

• Submit all groundwater monitoring well sample results and a description of any significant onsite leaks/spills that impact groundwater

Response: A review of the January 1, 2007 to December 31, 2007 time period indicated there were no unplanned, unanticipated or abnormal releases from the site to unrestricted areas of radioactive materials of gaseous or liquid effluents.

2007 Groundwater Monitoring Well Tritium information

Well ID.	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sept-07	Oct-07	Nov-07	Dec-07
	(µCi/ml)	(µCi/ml)	(µCi/ml)	(µCi/ml)	(µCi/ml)	(µCi/ml)	(µCi/ml)	(µCi/ml)	(µCi/ml)	(µCi/mł)	(µCi/ml)	(µCi/ml)
BD-1			< 5.57E-07		< 5.64E-07		< 6.10E-07			< 6.14E-07		
BD-2	< 5.74E-07		< 5.56E-07		< 5.57E-07		< 6.01E-07			< 6.20E-07	< 6.14E-07	
BD-3			< 6.22E-07		< 6.14E-07		< 6.66E-07				< 5.76E-07	
BD-4			< 6.20E-07		< 5.61E-07		< 6.20E-07				< 6.17E-07	
BD-5			< 5.56E-07		< 6.07E-07		< 6.09E-07			< 5.74E-07		
SC-1			< 5.56E-07		< 6.07E-07							
SD-1	< 5.96E-07		< 5 56E-07		< 5 73E-07		< 6.01E-07			< 5 83F-07	< 6 14F-07	
SD-2			< 6 19E-07		< 5.55E-07		< 5.98E-07			< 6 12F-07	< 6 14E-07	
SD-3	· · · · ·		< 6.16E-07		< 5.54E-07		< 6.03E-07			- 0.122 01	< 6.04E-07	
SD-4			< 5.58E-07		< 6.04E-07					< 6.11E-07		
							<u> </u>					
SW-1	7.42E-07	1.11E-06	1.36E-06	1.19E-06	8.53E-07	9.29E-07	9.69E-07	< 6.01E-07	8.59E-07	9.66E-07	9.64E-07	
SW-2			< 6.56E-07		< 5.55E-07		1				Ì	
SW-3			< 5.74E-07		5.92E-07		< 6.03E-07			< 6.14E-07		
BU-1				< 6.27E-07	< 6.18E-07		< 6.23E-07				< 6.23E-07	
SU-1			< 6.16E-07		< 6.07E-07		< 6.03E-07				< 6.14E-07	
SP 12											< 6 22E 07	
30-12											< 0.22L-07	{
ND-10												< 5.54E-07
ND-15			•									< 5.90E-07
ND-20												< 5.54E-07
ND-25							1					< 5.54E-07

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ENCLOSURE 2 TO SBK-L-08073

Joint Frequency Distributions of Wind Speed, Wind Direction and Atmospheric Stability

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	43.0 FT	WIND D.	АТА		STABI	LITY C	LASS	A		CLASS	FREQU	JENCY	(PERCEN	IT) =	2.00				
								Ŵ	IND DI	RECTIC	N FROM	1							
	SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
	CALM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	00.	00.	00.	00.	00.	00.	.00	00.	00.	00	00.	00.	00.	00.	00.	00.	00.	00.
	(2)	00.	00.	00.	00.	00.	00.	.00	00.	00.	00	00.	00.	00.	00.	00.	00	00.	00.
	C-3	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	1
	(1)	00.	00.	.00	00.	00.	00.	.61	00.	00.	00.	00.	.00	.00	00.	00.	00.	00.	.61
	(2)	00.	00	.00	00.	00.	00.	.01	00.	00.	00.	00.	.00	.00	00.	00.	00.	00.	.01
	4-7	0	0	0	1	0	2	6	0	0	0	0	1	3	1	0	0	0	14
	(1)	00.	00.	.00	.61	00.	1.21	3.64	00	00:	00.	00.	.61	1.82	.61	.00	00.	00.	8.48
	(2)	00.	00.	.00	.01	00.	.02	.07	00	00	00.	00.	.01	.04	.01	.00	00.	00.	.17
	8-12	0	1	2	1	8	9	34	14	1	3	13	12	7	9	5	0	0	119
	(1)	00.	.61	1.21	.61	4.85	5.45	20.61	8.48	.61	1.82	7.88	7.27	4.24	5.45	3.03	00.	00.	72.12
	(2)	00.	.01	.02	.01	.10	.11	.41	.17	.01	.04	.16	.15	.08	.11	.06	00.	00.	1.44
	13-18	0	0	0	0	1	0	1	0	1	3	4	6	3	6	6	0	0	31
	(1)	.00.	00.	00.	.00	.61	00.	.61	00.	.61	1.82	2.42	3.64	1.82	3.64	3.64	00.	00.	18.79
	(2)	.00	00.	00.	.00	.01	00.	.01	00.	.01	.04	.05	.07	.04	.07	.07	00.	00.	.38
	19-24 (1) (2)	0 .00 .00	0 00. 00.	0 .00 .00	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 .00. .00	0 .00. .00	0 00. 00.	0 00. 00.	0 .00 .00	0 .00 .00	0 00. 00.	0 00. 00.	0 00. 00.	0 .00. .00	00.00
	GT 24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	00.	.00.	00.	00.	00.	00.	00.	00.	00.	00.	00:	00.	00.	00.	00.	.00	00.	.00.
	(2)	00.	.00	00.	00.	00.	00.	00	00.	00.	00.	00	00.	00.	00.	00.	.00	00.	.00
ALL	SPEEDS	0	1	2	2	9	11	42	14	2	6	17	19	13	16	11	0	0	165
	(1)	00.	.61	1.21	1.21	5.45	6.67	25.45	8.48	1.21	3.64	10.30	11.52	7.88	9.70	6.67	00.	00.	100.00
	(2)	00.	.01	.02	.02	.11	.13	.51	.17	.02	.07	.21	.23	.16	.19	.13	00.	00.	2.00

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE (2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD C= CALM (WIND SPEED LESS THAN OR EQUAL TO .95 MPH)

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	43.0 FT	WIND D	ATA		STABI	LITY C	LASS E	3		CLASS	FREQU	JENCY	(PERCEN	= (T)	3.56				
								W	IND DI	RECTIC	N FROM	4							
1	SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
	CALM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.	00.
	(2)	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.	00.
	C-3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	.00.	.00.	.00.	.00.	.00.	.00.	00.	.00.	00.	00.	00.	.00.	00.	00.	.00.	.00.	00.	00.
	(2)	.00.	.00	.00	.00	.00	.00	00.	.00	00	00	00.	.00	00.	00.	.00	.00	00.	00.
	4-7	1	2	0	1	1	1	6	4	2	2	1	4	5	5	1	0	0	36
	(1)	.34	.68	00.	.34	.34	.34	2.04	1.36	.68	.68	.34	1.36	1.70	1.70	.34	00.	00.	12.24
	(2)	.01	.02	00.	.01	.01	.01	.07	.05	.02	.02	.01	.05	.06	.06	.01	00.	00.	.44
	8-12	2	1	3	12	23	16	14	8	2	7	22	31	13	22	11	5	0	192
	(1)	.68	.34	1.02	4.08	7.82	5.44	4.76	2.72	.68	2.38	7.48	10.54	4.42	7.48	3.74	1.70	00.	65.31
	(2)	.02	.01	.04	.15	.28	.19	.17	.10,	.02	.08	.27	.38	.16	.27	.13	.06	00.	2.33
	13-18	0	0	1	4	3	1	2	0	0	1	7	6	4	14	16	1	0	60
	(1)	00.	00.	.34	1.36	1.02	.34	.68	.00.	00.	.34	2.38	2.04	1.36	4.76	5.44	.34	00.	20.41
	(2)	00.	00.	.01	.05	.04	.01	.02	.00	00.	.01	.08	.07	.05	.17	.19	.01	00.	.73
	19-24	0	0	0	0	0	0	0	0	0	0	0	0	0	3	2	0	0	5
	(1)	.00	.00.	00.	00.	.00.	00.	.00.	.00.	.00.	.00	00.	.00	00.	1.02	.68	00.	00.	1.70
	(2)	.00	.00	00.	00.	.00	00.	.00	.00	.00	.00	00.	.00	00.	.04	.02	00.	00.	.06
	GT 24	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	1
	(1)	.00	00.	00.	.00.	.00.	.00.	.00.	.00.	00.	00.	.00	.00	.00	.34	.00	.00.	.00.	.34
	(2)	.00	00.	00.	.00	.00	.00.	.00	.00	00.	00.	.00	.00	.00	.01	.00	.00	.00.	.01
ALL :	SPEEDS	3	3	4	17	27	18	22	12	4	10	30	41	22	45	30	6	0	294
	(1)	1.02	1.02	1.36	5.78	9.18	6.12	7.48	4.08	1.36	3.40	10.20	13.95	7.48	15.31	10.20	2.04	00.	100.00
	(2)	.04	.04	.05	.21	.33	.22	.27	.15	.05	.12	.36	.50	.27	.55	.36	.07	00.	3.56

WIND DIRECTION FROM																		
SPEED MPH	N	NNE	NĔ	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
CALM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	00.	00.	00.	00.	00.	00.	00.	.00.	00.	00.	00.	00.	.00	.00	00.	00.	00.	.00
(2)	00.	00.	00.	00.	00:	00.	00.	.00	00.	00.	00.	00.	.00	.00	00.	00.	00.	.00
C-3	0	0	1	1	0	0	0	0	0	1	1	0	0	1	0	0	0	5
(1)	00.	00.	.18	.18	00.	00.	00.	00.	00.	.18	.18	00.	00.	.18	00.	00.	00.	.92
(2)	00.	00.	.01	.01	00.	00.	00.	00.	00.	.01	.01	00.	00.	.01	00.	00.	00.	.06
4-7	5	2	1	5	11	10	16	3	1	6	10	11	25	10	8	3	0	127
(1)	.92	.37	.18	.92	2.03	1.85	2.96	.55	.18	1.11	1.85	2.03	4.62	1.85	1.48	.55	00.	23.48
(2)	.06	.02	.01	.06	.13	.12	.19	.04	.01	.07	.12	.13	.30	.12	.10	.04	00.	1.54
8-12	5	3	2	20	23	25	16	12	1	6	25	31	43	50	23	5	0	290
(1)	.92	.55	.37	3.70	4.25	4.62	2.96	2.22	.18	1.11	4.62	5.73	7.95	9.24	4.25	.92	00.	53.60
(2)	.06	.04	.02	.24	.28	.30	.19	.15	.01	.07	.30	.38	.52	.61	.28	.06	00.	3.51
13-18	0	0	1	1	0	0	0	0	0	0	2	7	19	34	34	1	0	99
(1)	.00.	00.	.18	.18	00.	00.	00.	00.	00.	.00	.37	1.29	3.51	6.28	6.28	.18	00.	18.30
(2)	.00	00.	.01	.01	00.	00.	00.	00.	00.	.00	.02	.08	.23	.41	.41	.01	00.	1.20
19-24	0	0	0	0	0	1	0	0	0	0	0	0	1	2	14	2	0	20
(1)	00.	00.	00.	00.	00.	.18	00.	00.	00.	00.	00.	00.	.18	.37	2.59	.37	.00	3.70
(2)	00.	00.	00.	00.	00.	.01	00.	00.	00.	00.	00.	00.	.01	.02	.17	.02	.00	.24
GT 24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.	00.	00.	00.	.00
(2)	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00	00.	00.	00.	.00
ALL SPEEDS	10	5	5	27	34	36	32	15	2	13	38	49	88	97	79	11	0	541
(1)	1.85	.92	.92	4.99	6.28	6.65	5.91	2.77	.37	2.40	7.02	9.06	16.27	17.93	14.60	2.03	00.	100.00
(2)	.12	.06	.06	.33	.41	.44	.39	.18	.02	.16	.46	.59	1.07	1.18	.96	.13	00	6.56

CLASS FREQUENCY (PERCENT) = 6.56

SEABROOK JAN07-DEC07 MET DATA JOINT FREQUENCY DISTRIBUTION (210-FOOT TOWER)

STABILITY CLASS C

43.0 FT WIND DATA

. 43.0 FI	WIND	DATA	•	STABI	LITY C	LASS I)		CLASS	FREQU	JENCY (PERCEN	T) =	50.68				
							M	IND DI	RECTIC	N FROM	i							
SPEED MPH	N	NNE	. NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	Ŵ	WNW	NW	NNW	VRBL	TOTAL
CALM	0	0	1	0	0	0	0	0	0	0	0	0	0	1	0	1	0	3
(1)	00.	00.	.02	.00.	00.	00.	00.	00.	00.	.00.	00.	00.	.00.	.02	.00.	.02	00.	.07
(2)	00.	00.	.01	.00	00.	00.	00.	00.	00	.00	00.	00.	.00	.01	.00	.01	00.	.04
C-3	31	31	18	27	16	17	9	11	24	15	23	29	38	45	43	36	0	413
(1)	.74	.74	.43	.65	.38	.41	.22	.26	.57	.36	.55	.69	.91	1.08	1.03	.86	00.	9.88
(2)	.38	.38	.22	.33	.19	.21	.11	.13	.29	.18	.28	.35	.46	.55	.52	.44	00.	5.01
4-7	105	59	74	101	110	57	44	58	66	83	98	129	153	165	149	117	0	1568
(1)	2.51	1.41	1.77	2.42	2.63	1.36	1.05	1.39	1.58	1.98	2.34	3.08	3.66	3.95	3.56	2.80	00.	37.49
(2)	1.27	.72	.90	1.22	1.33	.69	.53	.70	.80	1.01	1.19	1.56	1.85	2.00	1.81	1.42	00.	19.00
8-12	51	41	90	82	85	48	31	30	25	70	141	183	166	249	203	54	0	1549
(1)	1.22	.98	2.15	1.96	2.03	1.15	.74	.72	.60	1.67	3.37	4.38	3.97	5.95	4.85	1.29	00.	37.04
(2)	.62	.50	1.09	.99	1.03	.58	.38	.36	.30	.85	1.71	2.22	2.01	3.02	2.46	.65	00.	18.77
13-18	10	8	45	19	17	21	1	0	0	10	43	21	49	131	159	12	0	546
(1)	.24	.19	1.08	.45	.41	.50	.02	00.	00.	.24	1.03	.50	1.17	3.13	3.80	.29	.00.	13.06
(2)	.12	.10	.55	.23	.21	.25	.01	00.	00.	.12	.52	.25	.59	1.59	1.93	.15	.00	6.62
19-24 (1) (2)	0 - 00 - 00	1 .02 .01	17 .41 .21	3 .07 .04	15 .36 .18	.12 .06	0 .00. .00	0 .00. .00	0 00. 00.	0 00. 00.	4 .10 .05	0 00. 00.	3 .07 .04	21 .50 .25	22 .53 .27	0 00. 00.	0 .00.	91 2.18 1.10
GT 24	0	0	0	0	.12	0	0	0	0	0	0	0	0	0	0	0	0	12
(1)	00.	.00.	00.	.00.	.29	00.	00.	00.	.00.	00.	00.	.00.	00.	.00	00.	00.	00.	.29
(2)	00.	.00.	00.	.00	.15	00.	00.	00.	.00	00.	00.	.00	00.	.00	00.	00.	00.	.15
ALL SPEEDS (1) (2)	197 4.71 2.39	140 3.35 1.70	245 5.86 2.97	232 5.55 2.81	255 6.10 3.09	148 3.54 1.79	85 2.03 1.03	99 2.37 1.20	115 2.75 1.39	178 4.26 2.16	309 7.39 3.75	362 8.66 4.39	409 9.78 4.96	612 14.63 7.42	576 13.77 6.98	220 5.26 2.67	0 .00. .00	4182 100.00 50.68

	43.0 FT	WIND D	ATA		STABI	LITY C	LASS E	;	•	CLASS	FREQ	JENCY	(PERCE	NT) =	24.64				
								Ŵ	IND DI	RECTIC	N FROM	4							
-	SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
	CALM	1	2	0	0	0	0	0.	0	0	0	0	0	0	0	1	0	0	4
	(1)	.05	.10	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	.00	.05	00.	00.	.20
	(2)	.01	.02	00	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	.00	.01	00.	00.	.05
	C-3	21	13	16	34	14	18	10	10	15	25	34	39	57	57	45	22	0	430
	(1)	1.03	.64	.79	1.67	.69	.89	.49	.49	.74	1.23	1.67	1.92	2.80	2.80	2.21	1.08	00.	21.15
	(2)	.25	.16	.19	.41	.17	.22	.12	.12	.18	.30	.41	.47	.69	.69	.55	.27	00	5.21
	4-7	31	15	10	11	29	17	28	23	39	52	116	254	217	175	127	55	0	1199
	(1)	1.52	.74	.49	.54	1.43	.84	1.38	1.13	1.92	2.56	5.71	12.49	10.67	8.61	6.25	2.71	00.	58.98
	(2)	.38	.18	.12	.13	.35	.21	.34	.28	.47	.63	1.41	3.08	2.63	2.12	1.54	.67	00.	14.53
	8-12	2	3	1	10	8	6	6	14	8	17	63	107	46	37	22	4	0	354
	(1)	.10	.15	.05	.49	.39	.30	.30	.69	.39	.84	3.10	5.26	2.26	1.82	1.08	.20	00.	17.41
	(2)	.02	.04	.01	.12	.10	.07	.07	.17	.10	.21	.76	1.30	.56	.45	.27	.05	00.	4.29
	13-18	0	0	1	4	2	5	0	2	0	0	7	1	0	4	1	0	0	27
	(1)	00	00.	.05	.20	.10	.25	.00	.10	00.	00.	.34	.05	00.	.20	.05	00.	00.	1.33
	(2)	00	00.	.01	.05	.02	.06	.00	.02	00.	00.	.08	.01	00.	.05	.01	00.	00.	.33
	19-24	0	0	3	5	2	0	0	0	1	0	0	0	0	0	0	0	0	11
	(1)	.00	00.	.15	.25	.10	00.	00.	00.	.05	00.	.00	00.	00.	00.	00.	00.	00.	.54
	(2)	.00	00.	.04	.06	.02	00.	00.	00.	.01	00.	.00	00.	00.	00.	00.	00.	00.	.13
	GT 24	0	0	1	0	6	1	0	0	0	0	0	0	0	0	0	0	0	8
	(1)	00.	00.	.05	00.	.30	.05	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	.39
	(2)	00	00.	.01	00.	.07	.01	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	.10
ALI	L SPEEDS	55	33	32	64	61	47	44	49	63	94	220	401	320	273	196	81	0	2033
	(1)	2.71	1.62	1.57	3.15	3.00	2.31	2.16	2.41	3.10	4.62	10.82	19.72	15.74	13.43	9.64	3.98	00.	100.00
	(2)	.67	.40	.39	.78	.74	.57	.53	.59	.76	1.14	2.67	4.86	3.88	3.31	2.38	.98	00.	24.64

	43.0 FT	WIND D	ATA		STABI	LITY CI	LASS F			CLASS	FREQU	ÉNCY	(PERCE	NT) =	6.73				
								W	IND DI	RECTIO	N FROM	I							
	SPEED MPH	N	NNE	NE	ENÉ	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
	CALM	0	0	0	0	1	0	0	1	0	0	0	0	0	1	0	1	0	4
	(1)	00.	00.	00.	00.	.18	00.	00.	.18	00.	00.	00.	.00	00.	.18	00.	.18	00.	.72
	(2)	00.	00.	00.	00.	.01	00	00.	.01	00.	00.	00.	.00	00	.01	00.	.01	00.	.05
	C-3	9	2	7	11	9	4	1	1	3	6	17	30	71	65	40	13	0	289
	(1)	1.62	.36	1.26	1.98	1.62	.72	.18	.18	.54	1.08	3.06	5.41	12.79	11.71	7.21	2.34	00.	52.07
	(2)	.11	.02	.08	.13	.11	.05	.01	.01	.04	.07	.21	.36	.86	.79	.48	.16	00.	3.50
	4-7	3	0	0	3	5	1	3	1	1	5	16	53	53	63	45	7	0	259
	(1)	.54	00.	00.	.54	.90	.18	.54	.18	.18	.90	2.88	9.55	9.55	11.35	8.11	1.26	00.	46.67
	(2)	.04	00.	00.	.04	.06	.01	.04	.01	.01	.06	.19	.64	.64	.76	.55	.08	00.	3.14
	8-12	0	0	0	0	1	0	0	1	0	0	1	0	0	0	0	0	0	3
	(1)	00.	00.	00.	00.	.18	00.	00.	.18	00.	00.	.18	00.	00.	.00	00.	00.	00.	.54
	(2)	00.	00.	00.	00.	.01	00	00.	.01	00.	00.	.01	00.	00.	.00	00.	00.	00.	.04
	13-18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00.	00.	.00	00.	00.	00.	00.	.00
	(2)	00.	00.	00.	00.	00.	00.	00	00.	00.	00.	.00	00.	.00	00.	00.	00.	00.	.00
	19-24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00.	00.	00.	00.	00.	00.	00.	.00
	(2)	00.	00.	00.	00.	00.	00.	00	00.	00.	00.	.00	00.	00	00.	00.	00.	00.	.00
	GT 24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	00.	00.	00.	00.	00.	.00	00.	00.	.00.	00.	00.	00.	00.	00.	00.	00.	00.	.00
	(2)	00.	00.	00.	00.	00.	.00	00	00.	.00	00.	00.	00.	00.	00.	00.	00.	00.	.00
ALL,	SPEEDS	12	2	7	14	16	5	4	4	4	11	34	83	124	129	85	21	0	555
	(1)	2.16	.36	1.26	2.52	2.88	.90	.72	.72	.72	1.98	6.13	14.95	22.34	23.24	15.32	3.78	00.	100.00
	(2)	.15	.02	.08	.17	.19	.06	.05	.05	.05	.13	.41	1.01	1.50	1.56	1.03	.25	00.	6.73

43.0 FT WIND	DATA S	STABILITY CLAS	SG	CLASS	FREQUENCY	(PERCENT)	=	5.83

SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
CALM	0	0	1	0	0	0	0	0	0	0	1	1	0	0	0	0	0°	3
(1)	.00	00.	.21	00.	00	00.	00.	00.	00.	00.	.21	.21	00.	00.	00.	00.	.00	.62
(2)	.00	00.	.01	00.	00	00.	00	00.	00	00.	.01	.01	00.	00.	00.	00.	.00	.04
C-3	8	2	7	4	6	1	0	0	2	3	13	48	114	111	39	12	0	370
(1)	1.66	.42	1.46	.83	1.25	.21	.00.	00.	.42	.62	2.70	9.98	23.70	23.08	8.11	2.49	00.	76.92
(2)	.10	.02	.08	.05	.07	.01	.00	00.	.02	.04	.16	.58	1.38	1.35	.47	.15	00.	4.48
4-7	0	0	0	1	0	0	0	0	0	0	6	10	18	44	27	1	0	107
(1)	.00	00.	00.	.21	.00.	00.	00.	00.	00.	00.	1.25	2.08	3.74	9.15	5.61	.21	00.	22.25
(2)	.00	00.	00.	.01	.00	00.	00.	00.	00.	00.	.07	.12	.22	.53	.33	.01	00.	1.30
8-12	. 0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
(1)	.00	00.	00.	00.	.21	00.	00.	00.	.00.	00.	00.	00.	00.	.00	00.	00.	00.	.21
(2)	.00	00.	00.	00.	.01	00.	00.	00.	.00	00.	00.	00.	00.	.00	00.	00.	00.	.01
13-18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	.00	00.	00.	00.	00.	00.	00.	.00.	.00	00.	00.	00.	.00	.00	00.	00.	00.	00.
(2)	.00	00.	00.	00.	00.	00.	00.	.00	.00	00.	00.	00.	.00	.00	00.	00.	00.	00.
19-24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	.00	.00	00.	.00.	.00.	•00	.00.	.00	.00.	00.	00.	00.	00.	.00	00.	00.	00.	.00
(2)	.00	.00	00.	.00	.00	•00	.00	.00	.00	00.	00.	00.	00.	.00	00.	00.	00.	.00
GT 24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	.00	00.	00.	.00.	.00.	00.	00.	00.	00.	.00.	.00	00.	00.	00.	00.	00.	00.	.00
(2)	.00	00.	00.	.00	.00	00.	00.	00.	00.	.00	.00	00.	00.	00	00.	00.	00.	.00
ALL SPEEDS (1) (2)	8	2	8	5	7	1	0	0	2	3	20	59	132	155	66	13	0	481
	1.66	.42	1.66	1.04	1.46	.21	00.	00.	.42	.62	4.16	12.27	27.44	32.22	13.72	2.70	00.	100.00
	.10	.02	.10	.06	.08	.01	00.	00.	.02	.04	.24	.72	1.60	1.88	.80	.16	00.	5.83

WIND DIRECTION FROM

STABILITY CLASS ALL

	SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
	CALM	1	2	2	0	1	0	0	1	0	0	1	1	0	2	1	2	0	14
	(1)	.01	.02	.02	.00	.01	.00	.00	.01	.00	.00	.01	.01	.00	.02	.01	.02	.00	.17
	(2)	.01	.02	.02	.00	.01	.00	.00	.01	.00	.00	.01	.01	.00	.02	.01	.02	.00	.17
	C-3	69	48	49	77	45	40	21	22	44	50	88	146	280	279	167	83	0	1508
	(1)	.84	.58	.59	.93	.55	.48	.25	.27	.53	.61	1.07	1.77	3.39	3.38	2.02	1.01	.00	18.28
	(2)	.84	.58	.59	.93	.55	.48	.25	.27	.53	.61	1.07	1.77	3.39	3.38	2.02	1.01	.00	18.28
	4-7	145	78	85	123	156	88	103	89	109	148	247	462	474	463	357	183	0	3310
	(1)	1.76	.95	1.03	1.49	1.89	1.07	1.25	1.08	1.32	1.79	2.99	5.60	5.74	5.61	4.33	2.22	.00	40.12
	(2)	1.76	.95	1.03	1.49	1.89	1.07	1.25	1.08	1.32	1.79	2.99	5.60	5.74	5.61	4.33	2.22	.00	40.12
	8-12	60	49	98	125	149	104	101	.79	37	103	265	364	275	367	264	68	. 0	2508
	(1)	.73	.59	1.19	1.51	1.81	1.26	1.22	.96	.45	1.25	3.21	4.41	3.33	4.45	3.20	.82	.00	30.40
	(2)	.73	.59	1.19	1.51	1.81	1.26	1.22	.96	.45	1.25	3.21	4.41	3.33	4.45	3.20	.82	.00	30.40
	13-18	10	8	48	28	23	27	4	2	1	14	63	41	75	189	216	14	0	763
	(1)	.12	.10	.58	.34	.28	.33	.05	.02	.01	.17	.76	.50	.91	2.29	2.62	.17	.00	9.25
	(2)	.12	.10	.58	.34	.28	.33	.05	.02	.01	.17	.76	.50	.91	2.29	2.62	.17	.00	9.25
	19-24	0	1	20	8	17	6	0	0	1	0	4	0	4	26	38	2	0	127
	(1)	.00	.01	.24	.10	.21	.07	.00	.00	.01	.00	.05	.00	.05	.32	.46	.02	.00	1.54
	(2)	.00	.01	.24	.10	.21	.07	.00	.00	.01	.00	.05	.00	.05	.32	.46	.02	.00	1.54
	GT 24	0	0	1	0	18	1	0	0	0	0	0	0	0	1	0	0	0	21
	(1)	.00	.00	.01	.00	.22	.01	.00	.00	.00	00	.00	.00	.00	.01	.00	.00	.00	.25
	(2)	.00	.00	.01	.00	.22	.01	.00	.00	.00	.00	.00	.00	.00	.01	.00	.00	.00	.25
ALL	SPEEDS	285	186	303	361	409	266	229	193	192	315	668	1014	1108	1327	1043	352	0	8251
	(1)	3.45	2.25	3.67	4.38	4.96	3.22	2.78	2.34	2.33	3.82	8.10	12.29	13.43	16.08	12.64	4.27	.00	100.00
	(2)	3.45	2.25	3.67	4.38	4.96	3.22	2.78	2.34	2.33	3.82	8.10	12.29	13.43	16.08	12.64	4.27	.00	100.00

WIND DIRECTION FROM

CLASS FREQUENCY (PERCENT) = 100.00

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE (2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD C= CALM (WIND SPEED LESS THAN OR EQUAL TO .95 MPH)

43.0 FT WIND DATA

							1	WIND DI	RECTIC	N FROM	I							
SPEED MPH	N	NNE	NE	ENE	E	ESE	SĒ	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
CALM	0	0	0	0	0	0	0	. 0	0	0	0	0	0	0	0	0	0	0
(1)	.00.	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	.00.	00.	00.	.00.	00.	00.	.00
(2)	.00	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	.00	00.	00.	.00	00	00.	.00
C-3	00.00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)		00.	.00.	00.	.00.	00.	.00.	.00.	00.	.00.	00.	.00.	.00	.00.	.00.	00.	00.	.00.
(2)		00.	.00	00.	.00	00.	.00	.00	00.	.00	00.	.00	.00	.00	.00	00.	00.	.00
4-7	0	0	0	0	1	0	3	0	0	0	0	0	0	0	0	0	0	4
(1)	.00.	00.	.00.	.00.	.61	.00.	1.82	.00	.00.	.00	00.	.00.	00.	.00.	.00.	00.	00.	2.42
(2)	.00	00.	.00	.00	.01	.00	.04	.00	.00	.00	00.	.00	00.	.00	.00.	00.	00.	.05
8-12	0	0	0	0	8	2	28	6	0	2	1	5	4	2	2	0	0	60
(1)	.00.	00.	.00.	.00.	4.85	1.21	16.97	3.64	.00	1.21	.61	3.03	2.42	1.21	1.21	00.	.00.	36.36
(2)	.00	00.	.00	.00	.10	.02	.34	.07	.00	.02	.01	.06	.05	.02	.02	00.	.00	.73
13-18	0	1	2	1	2	1	12	12	1	3	9	16	5	11	2	0	0	78
(1)	.00	.61	1.21	.61	1.21	.61	7.27	7.27	.61	1.82	5.45	9.70	3.03	6.67	1.21	00.	00.	47.27
(2)	.00	.01	.02	.01	.02	.01	.15	.15	.01	.04	.11	.19	.06	.13	.02	00.	00.	.95
19-24	0	0	0	0	0	0	2	0	1	1	1	3	3	7	4	0	0	22
(1)	.00.	00.	00.	.00.	00.	00.	1.21	.00	.61	.61	.61	1.82	1.82	4.24	2.42	00.	00.	13.33
(2)	.00	00.	00.	.00	00.	00.	.02	.00	.01	.01	.01	.04	.04	.09	.05	00.	00.	.27
GT 24 (1) (2)	0 .00. .00	0 .00. .00	0 00. 00	. 00 . 00	- 0 . 00 . 00	0 .00 .00	0 00. 00.	0 .00 .00	0 00. 00.	0 .00 .00	0 00. 00.	0 00. 00.	1 .61 .01	0 .00 .00	0 00. 00.	0 00. 00.	0 00. 00.	1 .61 .01
ALL SPEEDS	0	1	2	1	11	3	45	18	2	6	11	24	13	20	8	0	0	165
(1)	00.	.61	1.21	.61	6.67	1.82	27.27	10.91	1.21	3.64	6.67	14.55	7.88	12.12	4.85	00.	00.	100.00
(2)	00.	.01	.02	.01	.13	.04	.55	.22	.02	.07	.13	.29	.16	.24	.10	00.	00.	2.01

CLASS FREQUENCY (PERCENT) = 2.01

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
 (2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
 C= CALM (WIND SPEED LESS THAN OR EQUAL TO .95 MPH)

STABILITY CLASS A

209.0 FT WIND DATA

SEABROOK JAN07-DEC07 MET DATA JOINT FREQUENCY DISTRIBUTION (210-FOOT TOWER)

209.0 F	T WIND I	DATA		STABI	LITY C	LASS E	3		CLASS	FREQU	UENCY	(PERCEN	VT) =	3.58				
							Ň	IND DI	RECTIC	N FROM	M							
SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW		NNW	VRBL	TOTAL
CALM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	.00	.00	00.	00.	00.	00.	00.	00.	.00.	.00	00.	.00	00.	00.	.00	00.	00.	00.
(2)	.00	.00	00.	00.	00.	00.	00.	00.	.00	.00	00.	.00	00.	00.	.00	00.	00.	00.
C-3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	00	00.	00.	00.	00.	00.	00.	.00.	.00	00.	00.	.00	.00	00.	.00	00.	00.	00.
(2)	00	00.	00.	00.	00	00.	00.	.00	.00	00.	00.	.00	.00	00.	.00	00.	00.	00.
4-7	2	1	0	0	1	0	4	0	0	0	1	1	3	1	0	0	0	14
(1)	.68	.34	00.	00.	.34	00.	1.36	.00.	.00.	00.	.34	.34	1.02	.34	.00	00.	00.	4.76
(2)	.02	.01	00.	00.	.01	00.	.05	.00	.00	00.	.01	.01	.04	.01	.00	00.	00.	.17
8-12	3	1	2	8	21	10	16	4	2	6	10	12	6	12	4	3	0	120
(1)	1.02	.34	.68	2.72	7.14	3.40	5.44	1.36	.68	2.04	3.40	4.08	2.04	4.08	1.36	1.02	00.	40.82
(2)	.04	.01	.02	.10	.26	.12	.19	.05	.02	.07	.12	.15	.07	.15	.05	.04	00.	1.46
13-18	0	1	3	5	6	2	6	9	0	3	16	24	10	21	13	1	0	120
(1)	00.	.34	1.02	1.70	2.04	.68	2.04	3.06	00.	1.02	5.44	8.16	3.40	7.14	4.42	.34	.00	40.82
(2)	00.	.01	.04	.06	.07	.02	.07	.11	00.	.04	.19	.29	.12	.26	.16	.01	.00	1.4€
19-24	0	0	0	1	0	0	1	0	0	0	3	3	3	9	9	2	0	31
(1)	.00	.00	.00	.34	00.	00.	.34	.00 [.]	00.	00.	1.02	1.02	1.02	3.06	3.06	.68	00.	10.54
(2)	.00	.00	.00	.01	00.	00.	.01	.00	00.	00.	.04	.04	.04	.11	.11	.02	00.	.38
GT 24 (1) (2)	0 00. 00.	0 .00. .00	0 .00. .00	0 00. 00.	0 00. 00.	0 .00 .00	1 .34 .01	3 1.02 .04	5 1.70 .06	0 00. 00.	00 00	9 3.06 .11						
LL SPEEDS	5	· 3	5	14	28	12	·27	13	2	9	30	40	23	46	31	6	0	294
(1)	1.70	1.02	1.70	4.76	9.52	4.08	9.18	4.42	.68	3.06	10.20	13.61	7.82	15.65	10.54	2.04	.00.	100.00
(2)	.06	.04	.06	.17	.34	.15	.33	.16	.02	.11	.37	.49	.28	.56	.38	.07	.00	3.58

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE (2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD C= CALM (WIND SPEED LESS THAN OR EQUAL TO .95 MPH)

SEABROOK JAN07-DEC07 MET DATA JOINT FREQUENCY DISTRIBUTION (210-FOOT TOWER)

:	209.0 FT WIND DATA STABILITY CLASS C									CLASS	FREQU	ENCY (PERCEI	NT) ≓	6.58				
								W	IND DI	RECTIO	N FROM	I							
	SPEED MPH	ท	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
	CALM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	(1)	.00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.
	(2)	.00	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.
	C-3 (1) (2)	0 .00. .00	1 .18 .01	0 00. 00.	0 00. 00.	1 .18 .01	0 00. 00.	0 00. 00.	0 00.00	0 00. 00.	0 00. 00.	1 .18 .01	0 00. 00.	1 .18 .01	0 00. 00.	0 00. 00.	0 00. 00.	0 .00. .00	4 .74 .05
	4-7	2	0	1	3	9	3	11	1	1	2	6	6	12	7	5	2	0	71
	(1)	.37	00.	.18	.55	1.66	.55	2.03	.18	.18	.37	1.11	1.11	2.22	1.29	.92	.37	00.	13.12
	(2)	.02	00.	.01	.04	.11	.04	.13	.01	.01	.02	.07	.07	.15	.09	.06	.02	00.	.86
	8-12	6	1	2	10	24	18	28	8	2	4	13	20	23	16	11	7	0	193
	(1)	1.11	.18	.37	1.85	4.44	3.33	5.18	1.48	.37	.74	2.40	3.70	4.25	2.96	2.03	1.29	00.	35.67
	(2)	.07	.01	.02	.12	.29	.22	.34	.10	.02	.05	.16	.24	.28	.19	.13	.09	00.	2.35
	13-18	1	3	3	9	2	1	2	8	1	4	11	26	30	51	25	3	0	180
	(1)	.18	.55	.55	1.66	.37	.18	.37	1.48	.18	.74	2.03	4.81	5.55	9.43	4.62	.55	00.	33.27
	(2)	.01	.04	.04	.11	.02	.01	.02	.10	.01	.05	.13	.32	.37	.62	.30	.04	00.	2.19
	19-24	0	0	0	0	0	0	1	0	0	0	1	1	15	19	28	2	0	67
	(1)	.00	.00.	00.	00.	00.	00.	.18	00.	00.	00.	.18	.18	2.77	3.51	5.18	.37	00.	12.38
	(2)	.00	.00	00.	00.	00.	00.	.01	00.	00.	00.	.01	.01	.18	.23	.34	.02	00.	.82
·	GT 24 (1) (2)	0 .00 .00	0 00. 00.	00.00	0 00. 00.	0 00. 00.	1 .18 .01	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	3 .55 .04	10 1.85 .12	11 2.03 .13	1 .18 .01	0 00. 00.	26 4.81 .32
ALL	SPEEDS	9	5	6	22	36	23	42	17	4	10	32	53	84	103	80	.15	0	541
	(1)	1.66	.92	1.11	4.07	6.65	4.25	7.76	3.14	.74	1.85	5.91	9.80	15.53	19.04	14.79	2.77	.00	100.00
	(2)	.11	.06	.07	.27	.44	.28	.51	.21	.05	.12	.39	.64	1.02	1.25	.97	.18	.00	6.58

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SEABROOK JAN07~DEC07 MET DATA JOINT FREQUENCY DISTRIBUTION (210-FOOT TOWER)

209.0 FT	WIND D	ATA		STABI	LITY C	LASS D	,		CLASS	FREQU	ENCY (PERCEN	UT) =	50.52				
						,	W	IND DI	RECTIC	N FROM	I							
SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
CALM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00.
(2)	00.	00.	00.	00.	00.	00.	.00	00.	00.	00.	00.	00.	00	00.	00.	00.	00.	.00
C-3	14	6	13	17	5	6	8	7	7	11	9	10	18	15	14	11	0	171
(1)	.34	.14	.31	.41	.12	.14	.19	.17	.17	.26	.22	.24	.43	.36	.34	.26	00.	4.12
(2)	.17	.07	.16	.21	.06	.07	.10	.09	.09	.13	.11	.12	.22	.18	.17	.13	00.	2.08
4 -7	72	52	51	56	57	63	39	30	37	38	46	47	54	83	69	68	0	862
(1).	1.73	1.25	1.23	1.35	1.37	1.52	•94	.72	.89	.92	1.11	1.13	1.30	2.00	1.66	1.64	00.	20.76
(2)	.88	.63	.62	.68	.69	.77	•47	.37	.45	.46	.56	.57	.66	1.01	.84	.83	00.	10.49
8-12	85	56	63	75	65	61	47	53	55	95	103	98	113	156	131	87	0	1343
(1)	2.05	1.35	1.52	1.81	1.57	1.47	1.13	1.28	1.32	2.29	2.48	2.36	2.72	3.76	3.16	2.10	00.	32.35
(2)	1.03	.68	.77	.91	.79	.74	.57	.64	.67	1.16	1.25	1.19	1.38	1.90	1.59	1.06	00.	16.34
13-18	42	49	77	34	22	14	9	23	20	44	125	130	136	240	188	26	0	1179
(1)	1.01	1.18	1.85	.82	.53	.34	.22	.55	.48	1.06	3.01	3.13	3.28	5.78	4.53	.63	00.	28.40
(2)	.51	.60	.94	.41	.27	.17	.11	.28	.24	.54	1.52	1.58	1.65	2.92	2.29	.32	00.	14.35
19-24	20	21	28	9	10	17	5	2	0	9	27	10	74	109	99	9	0	449
(1)	.48	.51	.67	.22	.24	.41	.12	.05	00.	.22	.65	.24	1.78	2.63	2.38	.22	00.	10.81
(2)	.24	.26	.34	.11	.12	.21	.06	.02	00.	.11	.33	.12	.90	1.33	1.20	.11	00.	5.46
GT 24	0	7	15	4	25	4	0	0	0	0	4	0	19	35	32	3	0	148
(1)	00.	.17	.36	.10	.60	.10	00.	00:	00.	00.	.10	00.	.46	.84	.77	.07	00.	3.56
(2)	00.	.09	.18	.05	.30	.05	00.	00	00.	00.	.05	00.	.23	.43	.39	.04	00.	1.80
ALL SPEEDS	233	191	247	195	184	165	108	115	119	197	314	295	414	638	533	204	0	4152
(1)	5.61	4.60	5.95	4.70	4.43	3:97	2.60	2.77	2.87	4.74	7.56	7.11	9.97	15.37	12.84	4.91	.00.	100.00
(2)	2.84	2.32	3.01	2.37	2.24	2.01	1.31	1.40	1.45	2.40	3.82	3.59	5.04	7.76	6.49	2.48	.00	50.52

							Ŵ	IND DI	RECTIC	N FROM	4							
SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	· NW	NNW	VRBL	TOTAL
CALM	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
(1)	.00	00.	00.	00	.05	.00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	.05
(2)	.00	00.	00	00	.01	.00	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00.	.01
C-3	1	2	5	5	3	6	3	4	8	2	5	3	3	4	1	2	0	57
(1)	.05	.10	.25	.25	.15	.30	.15	.20	.39	.10	.25	.15	.15	.20	.05	.10	00.	2.81
(2)	.01	.02	.06	.06	.04	.07	.04	.05	.10	.02	.06	.04	.04	.05	.01	.02	00.	.69
4-7	25	24	18	20	11	13	32	22	14	17	24	19	20	14	28	27	0	328
(1)	1.23	1.18	.89	.99	.54	.64	1.58	1.08	.69	.84	1.18	.94	.99	.69	1.38	1.33	00.	16.16
(2)	.30	.29	.22	.24	.13	.16	.39	.27	.17	.21	.29	.23	.24	.17	.34	.33	00.	3.99
8-12	44	23	15	4	8	14	17	20	46	68	108	158	97	125	109	59	0	915
(1)	2.17	1.13	.74	.20	.39	.69	.84	.99	2.27	3.35	5.32	7.78	4.78	6.16	5.37	2.91	00.	45.07
(2)	.54	.28	.18	.05	.10	.17	.21	.24	.56	.83	1.31	1.92	1.18	1.52	1.33	.72	00.	11.13
13-18	9	3	1	6	3	3	3	26	9	29	96	159	99	155	50	. 7	0	658
(1)	.44	.15	.05	.30	.15	.15	.15	1.28	.44	1.43	4.73	7.83	4.88	7.64	2.46	.34	00.	32.41
(2)	.11	.04	.01	.07	.04	.04	.04	.32	.11	.35	1.17	1.93	1.20	1.89	.61	.09	00.	8.01
19-24	0	1	0	2	3	5	1	3	2	1	10	2	4	9	1	0	0	44
(1)	.00.	.05	00.	.10	.15	.25	.05	.15	.10	.05	.49	.10	.20	.44	.05	00.	00.	2.17
(2)	.00	.01	00.	.02	.04	.06	.01	.04	.02	.01	.12	.02	.05	.11	.01	00.	00.	.54
GT 24 (1) (2)	0 00. 00.	0 00. 00.	6 .30 .07	10 .49 .12	7 .34 .09	1 .05 .01	0 00. 00.	0 00. 00.	1 .05 .01	0 00. 00.	0 00.00	0 00. 00.	0 00. 00.	2 .10 .02	0 00. 00.	0 00. 00.	0 .00 .00	27 1.33 .33
ALL SPEEDS (1) (2)	79 3.89 .96	53 2.61 .64	45 2.22 .55	47 2.32 .57	36 1.77 .44	42 2.07 .51	56 2.76 .68	75 3.69 .91	80 3.94 .97	117 5.76 1.42	243 11.97 2.96	341 16.80 4.15	223 10.99 2.71	309 15.22 3.76	189 9.31 2.30	95 4.68 1.16	0 00. 00.	2030 100.00 24.70

CLASS FREQUENCY (PERCENT) = 24.70

SEABROOK JAN07-DEC07 MET DATA JOINT FREQUENCY DISTRIBUTION (210-FOOT TOWER) STABILITY CLASS E

209.0 FT WIND DATA

STABILITY CLASS F

							٢	NIND DI	RECTIO	ON FROM	1							
SPEED MPH	N	NNÉ	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
CALM (1) (2)	0 00. 00.	0 .00. .00.	0 00. 00.	0 00. 00.	0 .00. .00	0 00. 00.	0 00. 00.	0 .00. .00.	0 00. 00.	1 .18 .01	0 00. 00	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	1 .18 .01
C-3 (1) (2)	0 .00. .00	0 .00. .00	3 .54 .04	2 .36 .02	0 .00. .00	1 .18 .01	1 .18 .01	1 .18 .01	5 .90 .06	2 .36 .02	5 .90 .06	2 .36 .02	1 .18 .01	2 .36 .02	2 .36 .02	2 .36 .02	0 .00. .00	29 5.23 .35
4-7 (1) (2)	13 2.34 .16	8 1.44 .10	3 .54 .04	5 .90 .06	4 .72 .05	2 .36 .02	4 .72 .05	2 .36 .02	10 1.80 .12	8 1.44 .10	21 3.78 .26	7 1.26 .09	11 1.98 .13	9 1.62 .11	11 1.98 .13	6 1.08 .07	0 .00. .00	124 22.34 1.51
8-12 (1) (2)	14 2.52 .17	6 1.08 .07	5 .90 .06	1 .18 .01	1 .18 .01	1 .18 .01	1 .18 .01	5 .90 .06	12 2.16 .15	17 3.06 .21	17 3.06 .21	38 6.85 .46	46 8.29 .56	46 8.29 .56	35 6.31 .43	25 4.50 .30	0 00. 00.	270 48.65 3.29
13-18 (1) (2)	3 .54 .04	1 .18 .01	0 00. 00.	0 .00.	0 .00.	0 00. 00.	0 00. 00.	1 .18 .01	0 .00. .00.	2 .36 .02	11 1.98 .13	16 2.88 .19	27 4.86 .33	34 6.13 .41	29 5.23 .35	7 1.26 .09	0 .00. .00.	131 23.60 1.59
19-24 (1) (2)	0 00. 00.	0 .00.	0 00.	0 .00.	0 .00.	0 .00.	0 00. 00.	0 00.	0 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 .00.	0 00.	0 00. 00.
GT 24 (1) (2)	0 .00. .00	0 00.	0 00.	0 .00.	0 .00.	0 00.	0 00. 00.	0 00.	0 00. 00.	0 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 00. 00.	0 .00.	0 00. 00.	0 00. 00.	0 00. 00.
ALL SPEEDS (1) (2)	30 5.41 .37	15 2.70 .18	11 1.98 .13	8 1.44 .10	5 .90 .06	4 .72 .05	6 1.08 .07	9 1.62 .11	27 4.86 .33	30 5.41 .37	54 9.73 .66	63 11.35 .77	85 15.32 1.03	91 16.40 1.11	77 13.87 .94	40 7.21	0 00.	555 100.00 6.75

CLASS FREQUENCY (PERCENT) = 6.75

(1)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PAGE
(2)=PERCENT OF ALL GOOD OBSERVATIONS FOR THIS PERIOD
C= CALM (WIND SPEED LESS THAN OR EQUAL TO .95 MPH)

209.0 FT WIND DATA

209.0 E	FT WIN	ND DATA	STABILITY	CLASS G		CLASS	FREQUENCY	(PERCENT)	-	5.85
					WIND	DIRECTION	FROM			

SPEED MPH	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	WNW	NW	NNW	VRBL	TOTAL
CALM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	00.	.00.
(2)	00	00.	00	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	00.	.00
C-3	1	3	4	1	2	0	0	1	3	5	2	3	1	2	4	1	0	33
(1)	.21	.62	.83	.21	.42	00.	00.	.21	.62	1.04	.42	.62	.21	.42	.83	.21	.00	6.86
(2)	.01	.04	.05	.01	.02	00.	00.	.01	.04	.06	.02	.04	.01	.02	.05	.01	.00	.40
4-7	7	15	6	2	2	6	6	2	15	16	15	16	16	12	7	14	0	157
(1)	1.46	3.12	1.25	.42	.42	1.25	1.25	.42	3.12	3.33	3.12	3.33	3.33	2.49	1.46	2.91	00.	32.64
(2)	.09	.18	.07	.02	.02	.07	.07	.02	.18	.19	.18	.19	.19	.15	.09	.17	00.	1.91
8-12	24	5	4	0	0	0	1	6	11	18	17	37	27	30	25	28	0	233
(1)	4.99	1.04	.83	00.	00.	00.	.21	1.25	2.29	3.74	3.53	7.69	5.61	6.24	5.20	5.82	00.	48.44
(2)	.29	.06	.05	00.	00.	00.	.01	.07	.13	.22	.21	.45	.33	.37	.30	.34	00.	2.84
13-18	5	2	1	0	0	0	0	0	0	1	3	5	5	12	15	9	0	58
(1)	1.04	.42	.21	.00.	00.	.00.	00.	00.	00.	.21	.62	1.04	1.04	2.49	3.12	1.87	.00.	12.06
(2)	.06	.02	.01	.00	00.	.00	00.	00.	00.	.01	.04	.06	.06	.15	.18	.11	.00	.71
19-24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	.00	00.	00.	.00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	.00
(2)	.00	00.	00.	.00	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	00.	.00
GT 24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
(1)	.00	00	00.	00.	00.	.00.	.00.	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	.00
(2)	.00	00	00.	00.	00.	.00	.00	00.	00.	00.	00.	00.	00.	00.	00.	00.	.00	.00
ALL SPEEDS (1) (2)	37 7.69 .45	25 5.20 .30	15 3.12 .18	3 .62 .04	4 .83 .05	6 1.25 .07	7 1.46 .09	9 1.87 .11	29 6.03 .35	40 8.32 .49	37 7.69 .45	61 12.68 .74	49 10.19 .60	56 11.64 .68	51 10.60	52 10.81 .63	0 .00.	481 100.00 5.85

	209.0 FT	WIND I	DATA		STABI	LITY C	CLASS A	LL		CLASS	FREQU	IÉNCY	(PERCEI	NT) = (100.00				
								Б	IND DI	RECTIC	N FROM	1							
	SPEED MPH	Ν	NNE	NE	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	W	,wnw	NW	NNW	VRBL	TOTAI
	CALM	0	0	0	0	1	0	0	0	0	1	0	0	0	0	0	0	0	2
	(1)	.00	.00.	00.	00.	.01	.00.	00.	00.	00.	.01	00.	00.	00.	00.	.00	00.	00.	. 02
	(2)	.00	.00	00.	00.	.01	.00	00.	00.	00.	.01	00.	00.	00.	00.	.00	00.	00.	. 02
	C-3	16	12	25	25	11	13	12	13	23	20	22	18	24	23	21	16	0	294
	(1)	.19	.15	.30	.30	.13	.16	.15	.16	.28	.24	.27	.22	.29	.28	.26	.19	.00.	3.58
	(2)	.19	.15	.30	.30	.13	.16	.15	.16	.28	.24	.27	.22	.29	.28	.26	.19	.00	3.58
	4-7	121	100	79	86	85	87	99	57	77	81	113	96	116	126	120	117	0	1560
	(1)	1.47	1.22	.96	1.05	1.03	1.06	1.20	.69	.94	.99	1.38	1.17	1.41	1.53	1.46	1.42	00.	18.98
	(2)	1.47	1.22	.96	1.05	1.03	1.06	1.20	.69	.94	.99	1.38	1.17	1.41	1.53	1.46	1.42	00.	18.98
	8-12	176	92	91	98	127	106	138	102	128	210	269	368	316	387	317	209	0	3134
	(1)	2.14	1.12	1.11	1.19	1.55	1.29	1.68	1.24	1.56	2.56	3.27	4.48	3.85	4.71	3.86	2.54	00.	38.14
	(2)	2.14	1.12	1.11	1.19	1.55	1.29	1.68	1.24	1.56	2.56	3.27	4.48	3.85	4.71	3.86	2.54	00.	38.14
	13-18	60	60	87	55	35	21	32	79	31	86	271	376	312	524	322	53	0	2404
	(1)	.73	.73	1.06	.67	.43	.26	.39	.96	.38	1.05	3.30	4.58	3.80	6.38	3.92	.64	00.	29.29
	(2)	.73	.73	1.06	.67	.43	.26	.39	.96	.38	1.05	3.30	4.58	3.80	6.38	3.92	.64	00.	29.29
	19-24	20	22	28	12	13	22	10	5	3	11	42	19	99	153	141	13	0	613
	(1)	.24	.27	.34	.15	.16	.27	.12	.06	.04	.13	.51	.23	1.20	1.86	1.72	.16	00.	7.40
	(2)	.24	.27	.34	.15	.16	.27	.12	.06	.04	.13	.51	.23	1.20	1.86	1.72	.16	00.	7.40
	GT 24 (1) (2)	0 00. 00.	7 .09 .09	21 .26 .26	14 .17 .17	32 .39 .39	6 .07 .07	0 .00.	0 .00.	1 .01 .01	0 .00.	4 .05 .05	0 00. 00.	24 .29 .29	50 .61 .61	48 .58 .58	4 .05 .05	0 .00. .00.	211 2.57 2.57
ALL	SPEEDS	393	293	331	290	304	255	291	256	263	409	721	877	891	1263	969	412	0	8218
	(1)	4.78	3.57	4.03	3.53	3.70	3.10	3.54	3.12	3.20	4.98	8.77	10.67	10.84	15.37	11.79	5.01	00.	100.00
	.(2)	4.78	3.57	4.03	3.53	3.70	3.10	3.54	3.12	3.20	4.98	8.77	10.67	10.84	15.37	11.79	5.01	00.	100.00

SEABROOK STATION JAN – DEC 2007



S

STABILITY CLASS ALL CALM WINDS 0.02%

NOTE: Frequencies indicate direction from which the wind is blowing.





SEABROOK STATION JAN – DEC 2007



S

STABILITY CLASS ALL

CALM WINDS 0.17%

NOTE: Frequencies indicate direction from which the wind is blowing.



WIND SPEED (MPH)

ENCLOSURE 3 TO SBK-L-08073

Radiation Dose Assessment

Seabrook Station Radiological Effluent Impact Assessment For 2007 (Annual Radioactive Effluent Release Report)

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I. <u>Summary</u>

Seabrook Technical Specification Sections 6.7.6.g.4 & 9 require that limitations be placed on the quarterly and annual doses or dose commitments to Members of the Public from radioactive materials in liquid and gaseous effluents released from the station to Unrestricted Areas at or beyond the site boundary conforming to the dose objectives of Appendix I to 10 CFR Part 50. Technical Specification 6.7.6.g.8 requires that limitations on the quarterly and annual air doses resulting from noble gases released in gaseous effluents to areas beyond the site boundary also conform to Appendix I to 10 CFR Part 50. In a similar fashion, Technical Specification 6.7.6.g.11 requires limitations on the annual dose or dose commitment to any Member of the Public due to radioactivity and radiation from uranium fuel cycle sources conforming to the EPA Radiation Standards in 40 CFR Part 190. The following table details the above referenced effluent dose limits.

EFFLUENT TYPE	DOSE TYPE	QUARTERLY LIMITS	ANNUAL LIMITS		
LIQUIDS (10CFR50,	Total Body	1.5 mrem	3 mrem		
APP. I)	Max. Organ	5 mrem	10 mrem		
NOBLE GAS	Gamma Air	5 mrad	10 mrad		
(10CFR50, APP. I)	Beta Air	10 mrad	20 mrad		
GAS PARTICULATE (10CFR50, APP. I)	Max. Organ	7.5 mrem	15 mrem		
TOTAL DOSE	Total Body & organ		25 mrem		
(40CFR190) [liquids, gas, direct]	Thyroid		75 mrem		

DOSE OBJECTIVE CRITERIA FOR COMPLIANCE

Technical Specification 6.8.1.4 and the Seabrook Offsite Dose Calculation Manual (ODCM) Part A, Section 10.2, provides that the Station's Annual Radioactive Effluent Release Report include a demonstration of compliance with the above off-site dose limitations, as well as the determination of dose impacts to Members of the Public who may be associated with permitted activities inside the site boundary.

Doses resulting from actual liquid and gaseous effluents from Seabrook Station during 2007 were calculated in accordance with Method II as defined in the Station Offsite Dose Calculation Manual. The calculation methods follow the models in Regulatory Guide 1.109 (Reference 1). The assessments included maximum whole body doses and organ doses from all liquid releases, maximum offsite organ doses resulting from airborne iodines, tritium and particulate radionuclides with half-lives greater than eight days, and maximum offsite beta air and gamma air doses from airborne noble gases. Calculated dose impacts from airborne effluents included atmospheric dispersion estimates utilizing concurrent meteorology recorded by the Station's on-site meteorological tower. In addition, the potential direct dose

from fixed radiation sources from plant operations was evaluated as part of the assessment required under 40 CFR Part 190 for doses from the uranium fuel cycle.

Doses were also calculated for the special receptor locations inside the site boundary where the public might be granted access for recreational or educational purposes. The Science and Nature Center is located in the southwest portion of the site and offers educational opportunities on nuclear power and the environment. The "Rocks" is an area northeast of the main plant facilities with access to Brown's Creek and the tidal marsh that borders the site.

All calculated liquid and gaseous pathway doses for the 2007 reporting period are well below the dose criteria of 10CFR50, Appendix I, and the dose limits for effluent releases stated in the ODCM. In addition, the total dose to the most limiting Member of the Public due to the combined exposure to plant-related direct radiation, and liquid and gaseous effluents, was below the dose standards of 40CFR190.

II. Method for Calculating the Total Body and Maximum Organ Doses Resulting from Liquid Releases

Liquid waste generated during plant operations is processed and discharged to the environment via the station's circulating water-cooling system. The cooling system utilizes an offshore-submerged multiport diffuser discharge for rapid dissipation and mixing of liquid effluents in the ocean environment. A 22-port diffuser section of the discharge system is located in approximately 50 to 60 feet of water with each nozzle 7 to 10 feet above the sea floor. Eleven riser shafts, with two diffuser nozzles each for the diffuser, are spaced about 100 feet apart over a distance of about 1000 feet. Water is discharged in a generally eastward direction away from the shoreline through the multiport diffuser, beginning at a location over one mile offshore. During power operations, these high velocity jets passively entrain about ten volumes of fresh water into the near field jet-mixing region before the plume reaches the water surface. This arrangement also effectively prevents the discharge plume (at least to the 1 degree or 40 to 1 dilution isopleth) from impacting the shoreline over the tidal cycle.

During shutdown periods, the high velocity jet mixing created by the normal circulating water flow at the diffuser nozzles is reduced. However, mixing within the discharge tunnel water volume is significantly increased due to the long transit time for batch discharges to travel the three miles from the plant through the 19-foot diameter tunnels to the diffuser nozzles. Additional mixing of the effluent in the near field assures that an equivalent overall 10 to 1 dilution occurs by the time the effluent reaches the ocean surface.

The exposure pathways considered in the calculations of total body and maximum organ doses resulting from liquid discharges from Seabrook Station are limited to ingestion of aquatic foods and exposure to shoreline deposits. The dose calculations do not include the ingestion of potable water or irrigated vegetation as potential exposure pathways because the liquid effluents from the plant are discharged into salt water.

The dose assessment models utilized in the Offsite Dose Calculation Manual (ODCM) (Reference 2) are taken from Regulatory Guide 1.109 (Reference 1). The total body and organ doses are evaluated for each of the four age groups (i.e., infant, child, teen and adult) to determine the maximum total body dose and maximum organ dose via all existing exposure pathways (i.e., fish and aquatic invertebrate ingestion, and shoreline exposure) to an age-dependent individual from all detected radionuclides in plant releases. The values for the various factors considered in the model equations are provided in Regulatory Guide 1.109 and the ODCM (see Table D). The flow rate of the liquid effluent (F) and the radionuclide activities (Q_i) are measured specifically prior to each liquid release. The values for half-lives for radionuclides ($T_{1/2}$) and their radioactive decay constants (λ_i) have been taken from Kocher (Reference 3).

Table A presents the calculated liquid pathway doses for each calendar quarter and total for the year. The calculated annual doses as a percent of the applicable regulatory limits are shown in Table C. The estimated quarterly and annual doses resulting from liquid effluents to members of the public are well below all dose limit criteria.

III. Method for Calculating the Gamma and Beta Air Doses from Noble Gases

Gamma and beta air doses due to noble gases in gaseous effluents are calculated for several receptor locations when noble gases are recorded in effluents. Those locations include the points of estimated highest off-site ground level air concentration of radioactive material, site boundary (or closest point on the opposite shoreline in directions which are bordered by the tidal marsh), nearest resident, nearest vegetable garden, and nearest milk animal within five miles for each of the sixteen principle compass directions. The special on-site receptor locations (Science and Nature Center and the "Rocks") are also included.

Atmospheric dispersion factors (i.e., X/Q factors) calculated from recorded concurrent site meteorological data (i.e., meteorological data measurements taken during the time of the release) are used in the estimation of receptor specific air concentrations due to station effluents. The atmospheric dispersion estimations utilize methodology generally consistent with US NRC Regulatory Guide 1.111 (Reference 4). Beta air doses use undepleted X/Q's and assumes a semi-infinite plume at the point of exposure. Gamma air doses are calculated using the finite cloud model presented in "Meteorology and Atomic Energy – 1968" (Reference 5). That model is implemented through the definition of an effective gamma atmospheric dispersion factor $[X/Q^{\gamma}]$ (Reference 6) and the replacement of the undepleted X/Q in the infinite cloud dose equation by $[X/Q^{\gamma}]$.

The release point of effluents is also considered in the atmospheric dispersion calculation. The primary vent stack is treated as a "mixed-mode" release, as defined in Regulatory Guide 1.111. These effluents are considered to be part-time ground level / part-time elevated releases depending on the ratio of primary vent stack exit velocity relative to the speed of prevailing wind. All other release points (e.g., Turbine Building and Chemistry lab hoods) are considered ground-level releases. The beta air and gamma air dose calculations are consistent with the models presented in Regulatory Guide 1.109 (Reference 1). The values for the dose factors, DF_i^{γ} and DF_i^{β} , have been taken from Table B-1 in Regulatory Guide 1.109.

Table A presents the calculated maximum off-site gamma air and beta air doses for each calendar quarter and year. The calculated annual doses as a percent of the applicable regulatory limit are shown in Table C. The estimated quarterly and annual air doses resulting from noble gas effluents are well below all dose limit criteria.

IV. Method for Calculating the Critical Organ Dose Resulting from Iodines, Tritium and Particulates with T 1/2 Greater than 8 Days in Gaseous Releases

Regulatory Guide 1.109 dose models are applied in the calculation of the critical organ doses from iodines, tritium and particulate radionuclides released into the atmosphere during reporting period. Atmospheric dispersion and deposition factors (i.e., depleted X/Q and D/Q factors) calculated with concurrent meteorological data (i.e., meteorological data measurements taken during the time of the release) are used in the determination of gaseous pathway doses. The dispersion models are described in Section B.7.3.2 & B.7.3.3 of the Seabrook ODCM.

Potential exposure pathways associated with gaseous effluent are (i) external irradiation from radioactivity deposited on the ground surface, (ii) inhalation, and (iii) ingestion of vegetables (both fresh leafy and stored), meat, and milk. Dose estimates were determined for the site boundary and for the locations of the nearest resident, vegetable garden, and milk animal in each of the sixteen principle compass directions. The locations of the nearest resident, vegetable garden and milk animal in each sector were identified by the 2007 Annual Land Use Census as required by ODCM Control C.9.2.1 (see Table F). Additionally, doses were calculated at the point of approximate maximum ground level air concentration of radioactive materials in gaseous effluent. Conservatism in the dose estimates was maintained by assuming that the vegetable garden pathway was active at each milk animal location. Though not required to be part of the land use census, meat animal (cattle) locations are included in the assessment when identified. Meat and milk animals were assumed to receive their entire intake from pasture during the second and third quarters. This is a conservative assumption because most dairy operations utilize supplemental feeding when animals are on pasture, or actually restrict animals to full time silage feeding throughout the entire year. Table E provides the reference sources for dose model parameter assumptions used in the dose assessment.

The maximum organ doses were determined by summing the contributions from all exposure pathways at each location, and sorting in descending order. Doses were calculated for the whole body, GI-LLI, bone, liver, kidney, thyroid, lung, and skin for adults, teenagers, children, and infants. The estimated quarterly and annual organ doses due to iodines, tritium and particulates at the location of the maximally exposed individual are reported in Table A.

The estimated organ doses from iodines, tritium and particulates in gaseous effluents are well below the 10CFR50, Appendix I dose criteria for the reporting period (See Table C for calculated dose as a percentage of annual limits).

V. <u>Total Dose (40 CFR Part 190)</u>

40 CFR 190 states that the annual dose equivalent should not exceed 25 mrem to the whole body, 75 mrem to the Thyroid, or 25 mrem to any other organ of any Member of the Public from all uranium fuel cycle sources. To show compliance with this standard, the maximum doses for both the liquid and gaseous pathways from Seabrook Station are added together with the whole body dose from noble gas releases and any direct radiation component attributed to plant fixed sources to the maximum receptor location. Since there are no other uranium fuel cycle facilities within five miles of Seabrook, no additional impacts from sources beyond Seabrook Station need be considered.

The sum of the maximum annual whole body doses to Members of the Public from all exposure pathways for liquid and gaseous effluents, plus the direct external dose from station fixed sources, was 1.89E-02 mrem to a hypothetical individual at or beyond the site boundary. The maximum organ dose (including the thyroid) to any age group from all exposure pathways including direct radiation was 1.98E-02 mrem.

Table B illustrates the total dose projections from all station sources to the maximum potential offsite individual for the year 2007 and demonstrates compliance with the EPA's environmental radiation standard for the uranium fuel cycle per 40 CFR Part 190 (See Table C for total dose as a percentage of annual limit).

VI. <u>References</u>

- Regulatory Guide 1.109, Revision 1, "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purposes of Evaluating Compliance with 10CFR Part 50, Appendix I", USNRC, October 1977.
- 2. Seabrook Station Offsite Dose Calculation Manual (ODCM), Revision 30, Effective Date 06-05-06.
- 3. Kocher, D.C., Dose-Rate Conversion Factors for Exposure to Photons and Electrons, Health Physics, Vol. 45, No. 3, Sept. 1983.
- 4. Regulatory Guide 1.111, Revision 1, "Method for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water Cooled Reactors", USNRC, July 1977.
- 5. Slade, D.H., "Meteorology and Atomic Energy 1968", USAEC, July 1968.
- Hamawi, J.N., "AEOLUS-2 A computer Code for the Determination of Continuous and Intermittent-Release Atmospheric Dispersion and Deposition of Nuclear Power Plant Effluents in Open-Terrain Sites, Coastal Sites, and Deep-River Valleys for the Assessment of Ensuing Doses and Finite-Cloud Gamma Radiation Exposures", Entech Engineering, Inc., March 1988.

Table A

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Maximum^(a)Off-Site Doses and Dose Commitments to Members of the Public

				Dose (mrem)	(b)		
Release Type		lst Quarter	2nd Quarter	3rd Quarter	4th Quarter	Year ^(c) 2007	
Liquid Effluents:							
Total Body Dose		1.19E-04	8.67E-05	2.75E-05	8.27E-05	3.16E-04	
Organ Dose		(1) 6.33E-04 (3)	(1) 3.45E-04 (3)	(1) 1.40E-04 (3)	(2) 1.36E-04 (4)	1.25E-03	
Airborne Effluents:	Airborne Effluents:						
Organ Dose from Iodines, Tritium, and Particulates		4.30E-03 (5)	9.85E-03 (6)	1.81E-03 (7)	2.56E-03 (8)	1.85E-02	
Noble Gases	Beta Air (mrad)	8.05E-06 (9)	1.10E-06 (10)	1.24E-06 (11)	1.32E-05 (12)	2.36E-05	
	Gamma Air (mrad)	1.42E-05 (9)	2.41E-06 (10)	2.60E-06 (11)	2.31E-05 (12)	4.23E-05	
Direct Dose Offsite From Plant Operation ^(e)						0	
Doses (mrem) at Receptor Loca	ations Inside Site	e Boundary ^(d) :		<u>.</u>	<u> </u>		
Science and Nature Center (SW Organ Dose (mrem)	/, 488m):	1.78E-06 (d1)	7.55E-06 (d1)	6.19E-07 (d1)	2.94E-07 (d1)	1.02E-05	
The "Rocks" (NE/ENE, 244m) Organ Dose (mrem)	:	2.45E-04 (d1)	1.75E-04 (d1)	9.35E-05 (d1)	1.09E-04 (d1)	6.23E-04	

Table A (continued)

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Maximum^(a) Off-Site Doses and Dose Commitments to Members of the Public

NOTES:

- (a) "Maximum means the largest fraction of corresponding 10CFR50, Appendix I, dose design objective.
- (b) The numbered footnotes indicate the age group, organ, and location (compass sector and distance from the primary vent in meters) of the dose receptor, where appropriate.
 - (1) Child
 - (2) Adult
 - (3) Bone of a child.
 - (4) GI-LLI of an adult.
 - (5) Liver, kidney, lung, GI-LLI, thyroid, and whole body of a Child, ENE 2313 m.
 - (6) Liver, kidney, lung, GI-LLI, thyroid, and whole body of a Child, SW 1130 m.
 - (7) Liver, kidney, lung, GI-LLI, thyroid, and whole body of a Child, W 1315 m.
 - (8) Liver, kidney, lung, GI-LLI, thyroid, and whole body of a Child, S 1212 m.
 - (9) ENE 2276 m.
 - (10) W 974 m
 - (11) NW 914 m
 - (12) N 914 m
- (c) "Maximum" dose for the year is the sum of the maximum doses for each quarter. This results in a conservative yearly dose estimate, but still well within the limits of 10CFR50.
- (d) For each special receptor location, the whole body and organ doses calculated for the airborne effluent releases were adjusted by the occupancy factor provided in Seabrook's ODCM (i.e., 0.0014 for the Science and Nature Center and 0.0076 for the "Rocks"). It should also be noted that for 2007 actual occupancy factors were much lower for the "Rocks" (close to zero) since access to the site by the general public has been greatly restricted for security reasons following the terrorist attacks on America on 09/11/01. For conservatism, the previous factors as listed in the ODCM were applied for an estimate of upper bound doses and comparison with calculated impacts for year's pre September 11, 2001. Where appropriate, the numbered footnotes indicate the organ and age group of the dose receptor:

(d1) Liver, kidney, lung, GI-LLI, thyroid, and whole body of a teen.

(e) Only station sources are considered since there are no other facilities within five miles of Seabrook Station. 2007 data for the closest off-site environmental TLD locations in each sector (as listed in Table B.4-1 of Seabrook's ODCM) were compared to preoperation data from 1986-1988 for the same locations. No statistical difference, which could be attributed to station sources, was identified.

Table B

Seabrook Station 2007 Annual Radioactive Effluent Release Report

<u>Total Dose to Maximum Off-Site Individual</u> (40CFR190)

Release Source	Total Body (mrem)	Maximum Organ ^(a) (mrem)
Liquids	3.16E-04	1.25E-03
Noble Gases	2.81E-05	2.81E-05
Gas Iodines, Tritium & Particulates	1.85E-02	1.85E-02
Direct Radiation	0	0
Annual Total	1.89E-02	1.98E-02

(a) Maximum organ includes consideration of the thyroid.

Table C

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Calculated 2007 Maximum Doses Versus Applicable Limits

Receptor	Applicable ODCM Control	ODCM Annual Limit	Calculated Annual (2007) Dose	Percent of Limit
Offsite				
Liquid Effluents				
Whole Body Dose	C.6.2.1	· 3 mrem	3.16E-04 mrem	0.011%
Organ Dose	C.6.2.1	10 mrem	1.25E-03 mrem	0.013%
Airborne Effluents				
Organ Dose (iodines, tritium, and part.)	C.7.3.1	15 mrem	1.85E-02 mrem	0.123%
Gamma Air Dose (noble gases)	C.7.2.1	10 mrad	4.23E-05 mrad	0.0004%
Beta Air Dose (noble gases)	C.7.2.1	20 mrad	2.36E-05 mrad	0.00012%
All Plant Sources ^(a)				
Whole Body Dose	C.8.1.1	25 mrem	1.89E-02 mrem	0.08%
Organ Dose	C.8.1.1	25 mrem	1.98E-02 mrem	0.08%
Onsite (Science and Nature Center, 488m SW)				
Airborne Effluents				
Organ Dose (iodines, tritium, and part.)	C.7.3.1 ^(b)	15 mrem	1.02E-05 mrem	0.00007%
Onsite (The "Rocks" 244m NE/ENE)		· · · · · · · · · · · · · · · · · · ·		
Airborne Effluents				
Organ Dose (indines tritium and part)	C 7 3 1 ^(b)	15 mrem	6.23E-04 mrem	0.0042%
Organ Dose (Tournes, untrum, and part.)	0.7.5.1			0.004270

(a) The "all plant sources" doses are the sum of the whole body doses and maximum organ doses from liquid, noble gas, and iodines/tritium/particulate releases as well as direct radiation from fixed station sources.

(b) ODCM Part A, Section 10.2 states that the annual effluent report shall include an assessment of the radiation doses from radioactive liquids and gaseous effluents to members of the public due to their activities inside the site boundary during the report period. The referenced limit (C.7.3.1) is the acceptable dose from gaseous effluents (no significant liquid pathways) to areas at and beyond the site boundary and is considered to be appropriate for comparison purposes.

Table D

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Sources of the Values of Factors Used in Liquid Dose Equations

Factor	Definition	Source
U _{ap}	Usage factor	Table B.7-1, Station ODCM
M _p	Mixing ratio	Section B.7.1, Station ODCM (value=0.1 for aquatic foods and 0.025 for shoreline)
B _{ip}	Equilibrium bioaccumulation factor	Table A-1, Reg. Guide 1.109
D _{aipj}	Dose factor	Tables E-11 through E-14, R.G. 1.109
t _p	Nuclide transit time	Table E-15, Reg. Guide 1.109
Kc	Transfer coefficient from water to sediment	Reg. Guide 1.109
t _b	Period of activity buildup in sediment or soil	Table B.7-2, Station ODCM
w	Shoreline width factor	Table A-2, Reg. Guide 1.109 (value=0.5)

Table E

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Sources of Values for the Factors Used in Dose Equations for Gaseous Releases

Factor	Definition	Source
t _b	Period of activity buildup in sediment or soil	Table B.7-2, Station ODCM
λι	Nuclide decay constant	Kocher (Reference 3)
DFG _{ij}	Ground plane dose factor	Table E-6, Reg. Guide 1.109
[X/Q] ^D	Atmospheric dispersion factor	Calculated following Reg. Guide 1.111
R _a	Breathing rate	Table B.7-3, Station ODCM
DFA _{ija}	Inhalation dose factor	Tables E-7 through E-10, Reg. Guide 1.109
di	Nuclide deposition rate	Reg. Guide 1.109
Р	Soil surface density	Table B.7-2, Station ODCM
t _e	Crop, leafy vegetable, or pasture grass exposure period	Table B.7-2, Station ODCM
t _h	Average time from crop harvest to consumption	Table B.7-2, Station ODCM
Yv	Agricultural productivity by unit area	Table B.7-2, Station ODCM
r	Fraction of deposited activity retained on crops, leafy vegetables, or pasture grass	Table E-15, Reg. Guide 1.109
B _{iv}	Stable element transfer coefficient from soil to produce, leafy vegetable, or pasture grass	Table E-1, Reg. Guide 1.109
р	Fractional equilibrium ratio	Reg. Guide 1.109
Н	Ambient absolute humidity	Table B.7-2, Station ODCM
F _m	Stable element transfer coefficient from feed to milk	Tables E-1 and E-2, Reg. Guide 1.109

Table E (continued)

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Sources of Values for the Factors Used in Dose Equations for Gaseous Releases

Factor	Definition	Source
t _f	Average time from feed to milk to consumption	Reg. Guide 1.109
fp	Fraction of the year that animals graze on pasture	Table B.7-2, Station ODCM
fs	Fraction daily feed pasture grass	Table B.7-2, Station ODCM
F _f	Stable element transfer coefficient from feed to meat	Table E-1, Reg. Guide 1.109
ts	Average time from meat animal slaughter to consumption	Table E-15, Reg. Guide 1.109
DFI _{ija}	Ingestion dose factor	Tables E-11 through E-14, R.G.1.109
U_a^v	Annual intake of produce	Table B.7-3, Station ODCM
U ^m	Annual intake of milk	Table B.7-3, Station ODCM
U ^F	Annual intake of meat	Table B.7-3, Station ODCM
U ^L a	Annual intake of leafy vegetables	Table B.7-3, Station ODCM
fg	Ingestion rate fractions for garden produce	Reg. Guide 1.109
fl	Ingestion rate fractions for garden leafy vegetables	Reg. Guide 1.109
λ _w	Rate constant for activity removal from plant and leaf surfaces by weathering	Table E-15, Reg. Guide 1.109
Q _F	Animal consumption rate	Table E-3, Reg. Guide 1.109

Table F

Seabrook Station 2007 Annual Radioactive Effluent Release Report

Receptor Locations* for Seabrook Station

	Nearest Resident	Nearest Garden	Milk Animals within 5 Mile Radius
Sector	mile (km)	mile (km)	mile (km)
N	2.20 (3.55)	2.47 (3.97)	
NNE	1.89 (3.04)	1.89 (3.04)	
NE	1.82 (2.92)	2.17 (3.50)	
ENE	1.44 (2.31)		
E	1.60 (2.58)		
ESE	1.70 (2.73)		
SE	1.46 (2.36)	2.60 (4.18)	·
SSE	1.02 (1.65)		
S	0.75 (1.21)	0.76 (1.22)	
SSW	0.69 (1.12)	0.88 (1.42)	
SW	0.70 (1.13)	1.12 (1.80)	
WSW	1.16 (1.87)	1.43 (2.31)	
W	0.82 (1.32)	0.87 (1.40)	
WNW	0.69 (1.11)	0.94 (1.52)	
NW	0.76 (1.22)	0.79 (1.27)	4.30 (6.93)
NNW	0.64 (1.04)	0.64 (1.04)	3.30 (5.32)

* Locations based on 2007 Land Use Census.