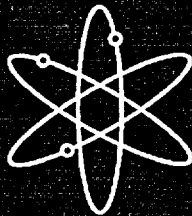
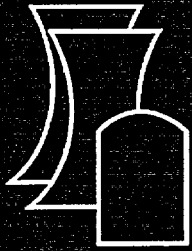


Evaluation of Eddy Current Reliability from Steam Generator Mock-Up Round-Robin



Argonne National Laboratory

**U.S. Nuclear Regulatory Commission
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By

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Abstract

This report presents an independent assessment of steam generator (SG) inspection reliability that was developed through a nondestructive evaluation round-robin on a steam generator mock-up at Argonne National Laboratory (ANL). The report does not establish regulatory position. The purpose of the round-robin was to assess the current state of SG tubing in-service inspection reliability, determine the probability of detection (POD) as function of flaw size or severity, and to assess the capability for sizing of flaws. Eleven teams participated in analyzing bobbin and rotating coil mock-up data collected by qualified industry personnel. The mock-up contains hundreds of cracks and simulations of artifacts such as corrosion deposits and tube support plates that make detection and characterization of cracks more difficult in operating steam generators than in most laboratory situations. An expert Task Group from industry, Argonne National Laboratory, and the NRC have reviewed the signals from the laboratory-grown cracks used in the mock-up to ensure that they provide reasonable simulations of those obtained in the field. The number of tubes inspected and the number of teams participating in the round-robin are intended to provide better statistical data on the POD and characterization accuracy than is currently available EPRI qualification programs.

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Executive Summary

One major outcome of regulatory activity over the past 10 years intended to develop guidance for tube integrity assessments is the development and implementation of two key concepts, condition monitoring and operational assessment. Condition monitoring is an assessment of the current state of the steam generator (SG) relative to the performance criteria for structural integrity. An operational assessment is an attempt to assess the state of the generator relative to the structural integrity performance criteria at the end of the next inspection cycle. Predictions of the operational assessment from the previous cycle can be compared with the results of the condition monitoring assessment to verify the adequacy of the methods and data used to perform the operational assessment.

The reliability of such assessments and projections depends heavily on the reliability of nondestructive evaluation (NDE) techniques used to establish the flaw distribution both in terms of detection and characterization of flaws and the capability to assess their impacts on the structural integrity (i.e., structural and leakage integrity) of SG tubes. An independent assessment of SG inspection reliability has been developed through an NDE round-robin on a steam generator mock-up at Argonne National Laboratory (ANL). The purpose of this exercise was to assess the current state of SG tubing in-service inspection (ISI) reliability, determine the probability of detection (POD) as function of flaw size or severity, and assess flaw sizing capability. This report presents the results for detection probabilities but does not establish regulatory position. Eleven teams have participated in analyzing bobbin and rotating probe data from the mock-up that was collected by qualified industry personnel. The mock-up contains hundreds of cracks and simulations of artifacts such as corrosion deposits, support structures, and tube geometry variations that in general make the detection and characterization of cracks more difficult. An expert NDE Task Group from ISI vendors, utilities, EPRI, ANL, and the NRC have reviewed the eddy current signals from laboratory-grown cracks used in the mock-up to ensure that they provide a realistic simulation of those obtained in the field. The number of tubes inspected and the number of teams participating in the round-robin are expected to provide better statistical data on the probability of detection (POD) and characterization accuracy than is currently available from industry performance demonstration programs.

The mock-up tube bundle consists of 400 Alloy 600 tubes made up of nine test sections, each 0.3 m (1 ft) long. The test sections are arranged in nine levels, each having 400 tube sections. The lowest level, level A, simulates the tube sheet, while the 4th, 7th, and 9th levels simulate tube support plate intersections. The other five levels are free-span regions. To simulate the tube sheet geometry, tubes were rolled into thick ferritic steel collars. Thus, both the roll transition geometry and the effect of the ferritic tube sheet are simulated. Axial and circumferential cracks are present in the roll transition region. In the tube support plate (TSP) crevice, the presence of magnetite was simulated by filling the crevice with magnetic tape or a ferromagnetic fluid. A mixture of magnetite and copper powder in an epoxy binder simulated sludge deposits. Axial outer diameter stress corrosion cracks (ODSCC), both planar and segmented, and cracks in dents with varying morphologies, are present at TSP locations. Cracks in the five-free span levels are primarily LODSCC, both planar and segmented. Other types of flaws such as (IGA) and wear are found in the tube bundle but in small numbers.

Bobbin coil (BC) data were collected on all 3600 test sections of the mock-up by using magnetically biased (mag-biased) probes. A mag-biased rotating three-coil probe that incorporates a midrange +Point, a 2.9-mm (0.115-in.)-diameter pancake, and a 2-mm (0.080-in.)-diameter high-frequency shielded pancake coil was used to collect data from all 400 tube sheet and special-interest test sections. Eddy current data was collected by a qualified industry team and stored on optical disks. Round-robin (RR) teams later analyzed the data with an ANL proctor present to monitor the analysis

process. The intent was to make the analysis as close a simulation of an actual inspection as possible. The procedures and training sets were developed in cooperation with the NDE Task Group so that the inspection protocols and training would mimic those in current practice.

The locations of flaws in the mock-up are known, because they were created by laboratory methods at ANL and Westinghouse and then the test sections containing flaws were carefully assembled into the mock-up. The reference state for each flaw in the mock-up, i.e., crack geometry and size, was established by using a multiparameter eddy current (EC) data analysis algorithm developed at ANL. Both pre- and post-assembly inspection results were used for this purpose. Throughout the development stage of the algorithm, comparisons were made between the NDE predictions and results obtained by destructive analyses for dozens of flaws. A final validation was performed by comparing the NDE results to destructive analyses in a blind test on a set of 23 flawed specimens. The results from this comparison were used to estimate the uncertainties associated with the depth estimates from the multiparameter algorithm. These results will be further validated by destructive examination of selected tubes from the mock-up.

Eleven teams participated in the analysis round-robin. Each team provided nine reports; a primary, a secondary, and a resolution analysts' report for each of the three optical data disks containing the inspection results. The first disk had the bobbin coil data from all 3600 test sections. The second had motorized rotating pancake coil (MRPC) data from selected test sections (special interest calls). The third optical disk contained MRPC data from all 400 tube sheet test sections. Results were analyzed for all teams with team-to-team variation in the POD presented, along with the population average. Analysis of the data for LODSCC at the tube support plate and in the free span showed that BC false call rates are about 2% for TSP and 0.1% for free span. The MRPC false call rate for the tube sheet is about 6% of all the test sections involved.

The detection results for the 11 teams were used to develop POD curves as a function of maximum depth and the parameter m_p , which can be interpreted as a stress multiplier that relates the stress in the ligament ahead of the crack to the stress in an unflawed tube under the same loading. Because m_p incorporates the effect of both crack depth and length, it better characterizes the effect of a flaw on the (i.e., structural and leakage integrity) of a tube than do traditional indicators such as maximum depth. The POD curves were represented as linear logistic curves, and the curve parameters were determined by the method of Maximum Likelihood. The effect of both statistical uncertainties inherent in sampling from distributions and the uncertainties due to errors in the estimates of maximum depth and m_p were estimated. The 95% one-sided confidence limits (OSL), which include errors in maximum depth estimates, are presented along with the POD curves.

The BC POD for TSP IDSCC is higher than for ODSCC (99% with 98% OSL at 60% TW vs. 75% with 65% OSL at 60% TW). The BC POD for freespan LODSCC (95% at 60% TW) is higher than the POD for TSP LODSCC and lower than the POD for TSP LIDSCC. The TS POD for IDSCC is about 90% with an OSL of about 75%. The highest TS MRPC POD curve is for LIDSCC where the POD at 60% TW is 95%. A review of MRPC results for BC voltage from 2.0 to 5.6 was carried out. Such calls are normally reviewed to confirm or dismiss the BC flaw call. The result, for LODSCC >74% TW, is an average correct call of 98%. All teams missed, with MRPC data, an LODSCC at the TSP with an estimated maximum depth of 28% TW. There is a possibility of having a strong BC signal and a weak MRPC signal that would not be called a crack by analysts. The example presented had an estimated maximum depth of 99% TW with only a few tenths of a volt generated by the +Point coil at 300 kHz.

When the PODs are considered as a function of m_p , it is found that in the TSP and FS regions the POD for cracks that would fail or leak under $3\Delta p$ internal pressure (corresponding to $m_p \approx 2.3$) is $>95\%$, even when uncertainties are accounted for.

The results were analyzed by team to determine whether there was a strong team-to-team variations in the POD. The performances of most of the teams cluster rather tightly, although in some cases there is a significant variation between best and worst. The probability that team-to-team variations in logistic fits to data are due to chance can be estimated. For LIDSCC at the TSP, the variation from best to worst is very significant statistically. There is $<0.1\%$ probability that the difference is due to chance (DTC). For FS OD, the variation from best to worst is probably significant (DTC is $<20\%$). For TSP OD, the probability that the variation from best to worst is DTC is $>60\%$ and thus the variation is probably not significant.

The BC voltages reported for LODSCC indications at TSP regions were also analyzed. In most cases, variations in reported voltages by the teams were fairly small. This in part is attributed to the fact that all teams analyzed the same set of data, i.e., identical data acquisition and calibration setups. For each longitudinal OD indication, an average BC voltage and a corresponding standard deviation were computed for all teams. For almost 85% of all indications, the normalized standard deviation in the reported voltage is <0.1 . Indications with larger variations are not associated with particularly high or low voltage values (i.e., approximately half the signals with standard deviations of >0.1 V have voltages of >2 V), but rather are associated with the complexity of the signal and the difficulty of identifying the peak voltage and the associated null position.

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Acronyms and Abbreviations

ABB-CE	ASEA Brown-Boveri-Combustion Engineering
AECL	Atomic Energy of Canada, Ltd.
ANL	Argonne National Laboratory
ASME	American Society of Mechanical Engineers
BC	bobbin coil
CIDSCC	circumferential inner diameter stress corrosion crack/cracking
CODSCC	circumferential outer diameter stress corrosion crack/cracking
DE&S	Duke Engineering and Services
EC	eddy current
ECT	eddy current testing
EDM	electro-discharge machining
EPRI	Electric Power Research Institute
FS	free span
FTI	Framatome Technology
ID	inner diameter
IGA	intergranular attack
INEEL	Idaho National Engineering and Environmental Laboratory
ISI	inservice inspection
LIDSCC	longitudinal inner-diameter stress corrosion crack/cracking
LODSCC	longitudinal outer diameter stress corrosion crack/cracking
MRPC	motorized rotating pancake coil
NDE	nondestructive evaluation
NDD	nondetectable degradation
NRC	U.S. Nuclear Regulatory Commission
OD	outer diameter
ODSCC	outer diameter stress corrosion crack/cracking
OPG	Ontario Power Generation
OSL	One-sided 95% confidence limits
PNNL	Pacific Northwest National Laboratory
POD	probability of detection
PWR	pressurized water reactor
PWSCC	primary-water stress corrosion crack/cracking
RPC	rotating pancake coil
RR	round-robin
RTZ	roll transition zone
SCC	stress corrosion crack/cracking
SG	steam generator
TS	tube sheet
TSP	tube support plate
TW	throughwall
UT	ultrasonic testing
W	Westinghouse



1 Introduction

One major outcome of regulatory activity over the past 10 years intended to develop guidance for tube integrity assessments is the development and implementation of two key concepts, condition monitoring and operational assessment. Condition monitoring is an assessment of the current state of the steam generator (SG) relative to the performance criteria of structural integrity. An operational assessment is an attempt to assess what will be the state of generator relative to the structural integrity performance criteria at the end of the next inspection cycle. The predictions of the operational assessment from the previous cycle can be compared with the results of the condition monitoring assessment to verify the adequacy of the methods and data used to perform the operational assessment. The reliability of the in-service inspection (ISI) is critical to the effectiveness of the assessment processes. Quantitative information on probability of detection (POD) and sizing accuracy of current-day flaws for techniques used for SG tubes is needed to determine if tube integrity performance criteria was met during the last operating cycle and if performance criteria for SG tube integrity will continue to be met until the next scheduled ISI. Information on inspection reliability will permit estimation of the true state of SG tubes after an ISI by including the flaws that were missed because of imperfect POD. Similarly, knowledge of sizing accuracy will permit corrections to be made to flaw sizes obtained from ISI.

Eddy-current (EC) inspection techniques are the primary means of ISI for assessing the condition of SG tubes in current use. Detection of flaws by EC depends on detecting the changes in impedance produced by the flaw. Although the impedance changes are small ($\approx 10^{-6}$), they are readily detected by modern electronic instrumentation. However, many other variables, including tube material properties, tube geometry, and degradation morphology, can produce impedance changes, and the accuracy of distinguishing between the changes produced by such artifacts and those produced by flaws is strongly influenced by EC data analysis and acquisition practices (including human factors). Similarly, although it can be shown that there is a relationship between the depth of a defect into the tube wall and the EC signal phase response, in practice, those things that affect detection also affect sizing capability.

The most desirable approach to establishing the reliability of current ISI methods could be to carry out round-robin (RR) exercises in the field on either operating SGs or those removed from service. However, access to such facilities for this purpose is difficult, and validation of the results would be difficult. Such work would also be prohibitively expensive. In addition, obtaining data on all morphologies of interest would require tubes from many different plants.

The approach chosen for this program was to develop an SG tube bundle mock-up that simulates the key features of an operating SG so that the inspection results from the mock-up would be representative of those for operating SGs. Considerable effort was expended in preparing realistic flaws and verifying that their EC signals and morphologies are representative of those from operating SGs. The mock-up includes stress corrosion cracks of different orientations and morphologies at various locations in the mock-up and simulates the artifacts and support structures that may affect the EC signals. Factors that influence detection of flaws include probe wear, eddy current signal noise, signal-to-noise ratio, analyst fatigue and the subjective nature of interpreting complex eddy current signals. In this exercise all analysts examine the same data provided on copies of optical disks that contain the data to be analyzed. The team-to-team variation in detection capability is the result of analyst variability in interpretation of eddy current signals. The fits to the POD data and the subsequent lower 95% confidence limits are influenced by the uncertainty in crack depth determined by a multiparameter algorithm and the number of cracks in the sample set. The mock-up will also be used as a test bed for evaluating emerging technologies for the ISI of SG tubes.

In this report, while the probabilities of detecting flaws of various types and at various locations are presented as logistic fit curves to the raw data, along with lower 95% confidence limits, the results do not establish regulatory position.

2 Program Description

The overall objective of the steam generator tube integrity program [1] is to provide the experimental data and predictive correlations and models needed to permit the NRC to independently evaluate the integrity of SG tubes as plants age and degradation proceeds, new forms of degradation appear, and new defect-specific management schemes are implemented. The objective of the inspection task is to evaluate and quantify the reliability of current and emerging inspection technology for current-day flaws, i.e., establish the probability of detection (POD) and sizing accuracy for different size cracks. Both EC and ultrasonic testing (UT) techniques are being evaluated, although only EC testing organizations have participated in the round-robin up to now.

The procedures and processes for the round-robin (RR) studies mimic those currently practiced by commercial teams in actual inspections. Teams participating in the RR exercise report their data analysis results on flaw types, sizes, and locations, as well as other commonly used parameters such as signal amplitude (voltage) and phase.

An important part of the round-robin RR exercise was the NDE Task Group, an expert group from ISI vendors, utilities, EPRI, ANL, and the NRC. They have reviewed the signals from the laboratory-grown cracks used in the mock-up to ensure that they provide reasonable simulations of those obtained from real cracks. The Task Group participated in the development of the RR and provided input on the quality of the mock-up data, the nature of flaws, and procedures for data acquisition, analysis, and documentation. To the extent possible, the intent was to mimic current industry practices.

Because the destructive examination of all the flaws in the mock-up would be extremely expensive and time-consuming, several laboratory NDE methods (including various EC and UT procedures) were evaluated as way to characterize the defects in the mock-up tubes so that the reference state can be estimated without destructive examinations. Based on these evaluations, multiparameter analysis of rotating probe data that was implemented at ANL was used to determine the reference state of the mock-up test sections [2]. This effort has provided sizing estimates for the tube bundle defects. The multiparameter algorithm has been validated by using 23 test sections with SCCs like those in the mock-up. The depth profiles generated by the multiparameter algorithm were compared to profiles of test sections destructively analyzed with cracks mapped by fractography techniques. These results will be further validated by the destructive examination of selected tubes from the mock-up before the final report on the work is completed.

2.1 Steam Generator Mock-Up Facility

The mock-up tube bundle consists of 400 22.2-mm (0.875-in.)-diameter, Alloy 600 tubes consisting of 9 test sections, each 0.3 m (1 ft) long. Test sections are arranged in nine levels with 400 test sections at any elevation. The center of the tubes are separated by 3.25 cm (1.28 in.). Tie rods hold the test sections together. The ends of each test section are pressed into 19-mm (0.75-in.)-thick high-density polyethylene plates that hold the test sections in alignment. One end of each tube is spring-loaded. The lowest level (A) has a roll transition zone (RTZ), and simulates the tube sheet, while the 4th, 7th, and 9th levels simulate drilled hole tube support plate (TSP) intersections. The other five levels are freespan regions. Above the 9th level is a 0.91-m (3-ft)-long probe run-out section (see Fig. 2.1 for the tube bundle diagram and Fig. 2.2 for photograph of the mock-up). Debris generated during assembly (e.g., shavings from the polyethylene plates) was cleared to assure the eddy current probes could travel unobstructed through all test sections.

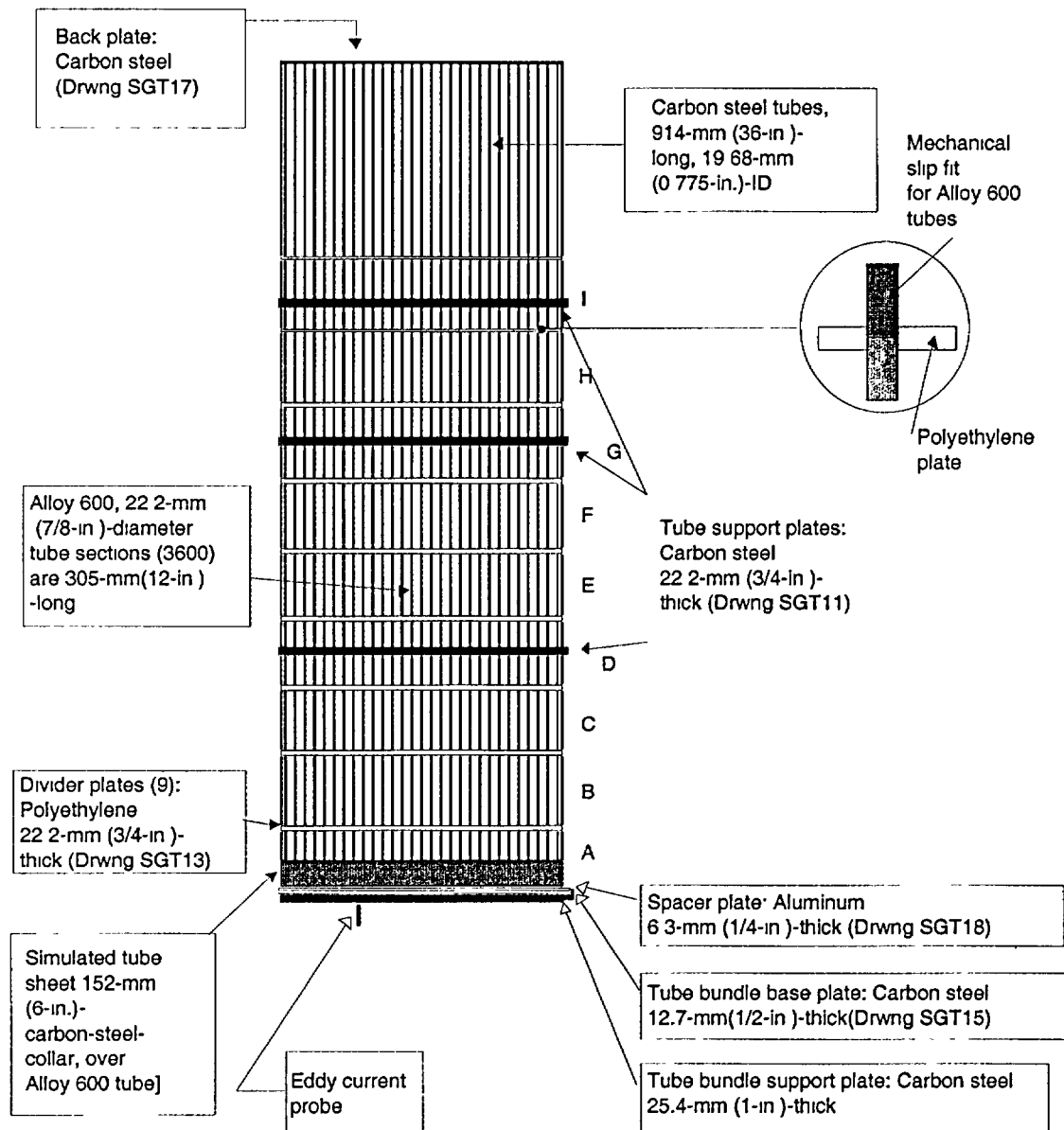


Figure 2.1 Schematic representation of steam generator mock-up tube bundle.

Most of the degraded test sections were produced at ANL, although some were produced by Pacific Northwest National Laboratory (PNNL), Westinghouse, Equipos Nucleares, SA (ENSA), and the Program for the Inspection of Steel Components (PISC).

The test sections in the tube sheet level are all mechanically expanded onto a 30.5-cm (6-in.)-long carbon steel collar, leaving a RTZ halfway from the tube end. In order to produce cracks in and near the RTZ, the steel collar was split and removed from the expanded tube. Exposing the expanded test specimen to a chemical solution then induced cracks. Axial and circumferential outer diameter (OD) and inner diameter (ID) stress corrosion cracks (SCC) were produced in the roll transition zones. New steel collars that were expanded by heating were slipped over the cracked tubes. This process produced flawed test sections with realistic EC signals.

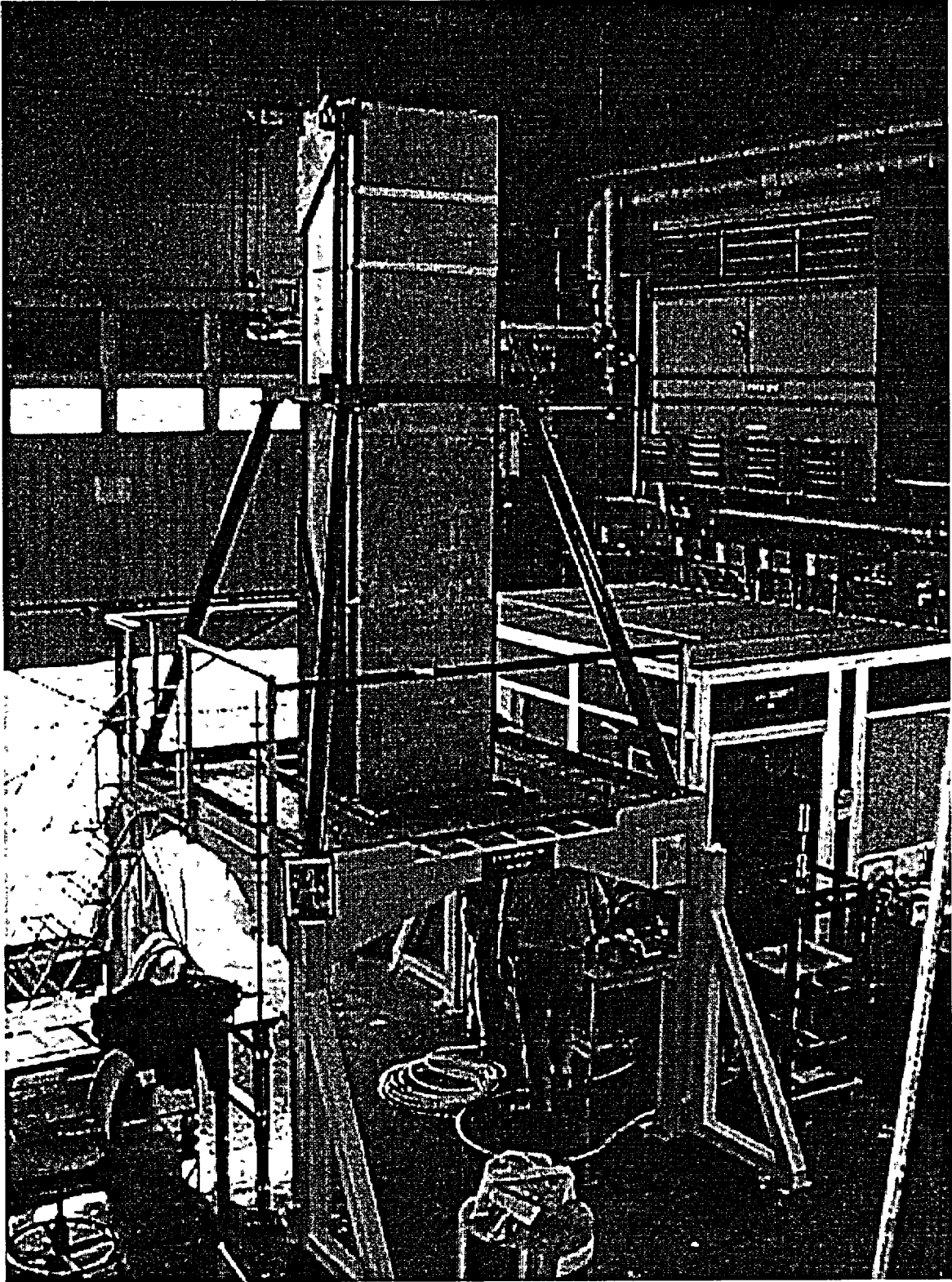


Figure 2.2 Photograph of mock-up during acquisition of eddy current data.

In the tube support plate TSP regions, filling the crevice with magnetic tape or a ferromagnetic fluid simulated magnetite in the crevices. A mixture of magnetite and copper bonded with epoxy simulated sludge deposits. Sludge was placed above the RTZ and at TSP intersections in some cases (see Figure 2.3 for photograph of sludge on a tube sheet test section). Many test sections had sludge or magnetite but no flaws. LODSCC and LIDSCC, both planar and segmented, and cracks with varying morphologies are present at TSP locations with and without denting (see Figure 2.4 for a photograph of a dent). Some flaw free test sections were dented. Cracks in the remaining five freespan levels are primarily LODSCC, both planar and segmented. Axial and circumferential cracks of ID and OD origin are found in the RTZ. A small number of other flaw types such as IGA and wear are placed in the tube bundle. The mock-up also contains test sections with electric-discharge-machined (EDM) notches and laser-cut slots. Table 2.1 summarizes the degradation types and their locations in the mock-up.

Magnetite-filled epoxy markers were placed at the ends of all test sections to provide a reference for the angular location of flaws when collecting data with a rotating or array probe. Figure 2.5 shows an isometric plot (c-scan) indicating the EC response from a 400- μm (0.016-in.)-wide by 250- μm (0.010-in.)-thick by 25-mm (1-in.)-long, axially oriented magnetite-filled epoxy marker located on the ID side, at the end of a test section. The data were acquired at 400 kHz with a 0.080-in. high-frequency shielded pancake coil. This test section also contains an outer-diameter stress corrosion crack (ODSCC) at the TSP intersection region. The analysts were instructed to ignore the region 1 in. from each test section end when carrying out their analysis.

Prior to assembly, flawed test sections in the tube bundle were examined with both bobbin coil (BC) and a three-coil rotating probe that incorporates a +Point coil, a 2.9-mm (0.115-in.) pancake coil, and a 2-mm (0.080-in.) shielded pancake coil. In addition to a full EC examination, many cracked test sections were examined by the dye-penetrant method before being incorporated into the mock-up tube bundle. If EC data, dye penetrant results or crack growth parameters indicated that a crack must be present, the test section was included in the mock-up. Because primary interest is with deep flaws, the majority of cracks selected for the mock-up had a +Point phase angle consistent with deep (>60% TW) cracks. Note that since the importance of obtaining POD data from deep flaws is greater than that for shallow ones, as expected, high voltage signals are more common in the mock-up than in operating steam generators. This is the result of the need for a large number of flaws when establishing a high POD (deep cracks) compared to the smaller number of flaws needed for a low POD (shallow cracks).

BC data from the mock-up were analyzed to show the distribution of voltages. The histograms (Figures 2.6 and 2.7) show a reasonable distribution of BC voltages (up to 20 V) for cracks and conditions, and cracks alone. Figure 2.6 shows the distribution for all signals called in the mock-up (cracks, dents, dings, wastage, and all overcall signals associated with artifacts). Figure 2.7 shows the distribution without the signals from artifacts or geometry. There are some cracks and conditions with voltages greater than 20 that are not shown in the histogram. Voltage and phase for mock-up cracks are similar in nature to field data such as from McGuire (Duke Power). Figure 2.8 shows a comparison of representative data from mock-up flaws and McGuire field data. The general scattering in the voltage-phase representation is similar. Although the McGuire tubes are 19-mm (0.75-in.) rather than the mock-up 22.2-mm (0.875-in.), they can be compared because the voltages from notches of the same %TW are set the same.

There are differences between the mock-up and an operating steam generator. The mock-up has short sections, not continuous tubes, and there are clear EC signals at the test section ends, which look like a throughwall 360° circumferential notch or crack. The short lengths were necessary to allow realistic flaws to be made and to allow the mock-up to be reconfigured. There are no U-bends in the

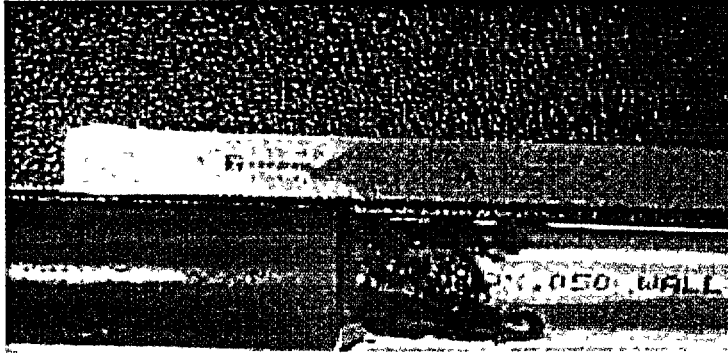


Figure 2.3
 Photograph of sludge on a tube sheet test section; many test sections with and without flaws had sludge deposits.

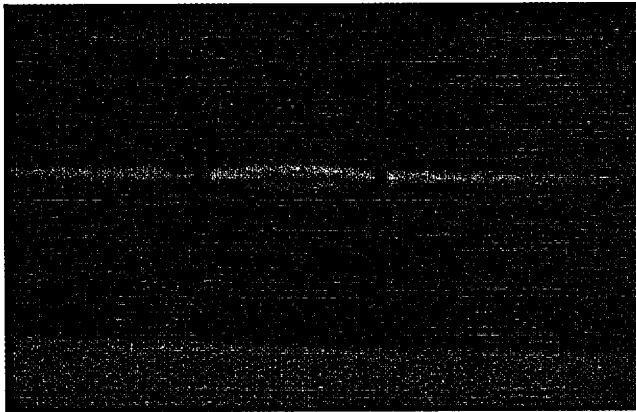


Figure 2.4
 Photograph of dent in a test section. Such dents were produced by a device provided by FTI. The dent is between the black bars, which are 25 mm apart. Test sections with and without cracks had dents.

Table 2.1 Flaw types and quantity

Location	EDM & Laser Cut Slots	IGA	ODSCC	PWSCC	Wear/Wastage	Fatigue
Top of Tube sheet	-		21	47	-	-
Freespan	14	8	90	4	3	-
TSPs	7	5	69	31	9	3

mock-up. The simulated tube sheet is only 15.2-cm (6-in.)-thick with individual ferritic steel collars into which the tube sheet test sections are expanded. For all practical purposes, the EC signals at the inner edge of the collars and at the roll transition areas are the same as found in the field.

2.1.1 Equivalencies

Mock-up data were collected with magnetically (“mag”) biased bobbin and MRPC probes. Data have been collected to show equivalency of mag- and non-mag-biased probes. This is necessary because of the use of non-mag biased probes in the field. Magnetically biased probes were used for the mock-up so those signals from sensitized and nonsensitized test sections have similar EC responses. Data from several mock-up flaws have been analyzed by using all frequencies employed in the mock-up data acquisition exercise. Data from a mag-biased +Point coil and data from the same flaw obtained with a

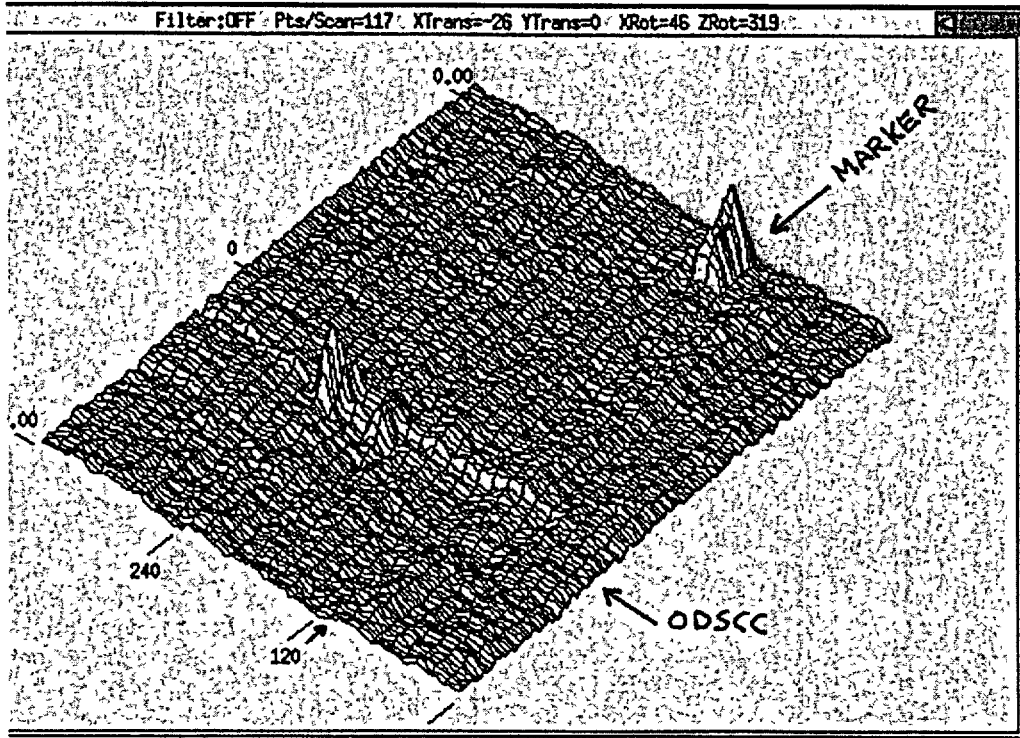


Figure 2.5 Isometric plot (c-scan) showing eddy current response from 400- μm -wide by 250- μm -thick by 25-mm-long, axially oriented magnetite filled epoxy marker located on ID side at end of 22.2 mm (0.875-in.) Inconel 600 tube.

non-mag-biased coil are virtually the same [1]. Mock-up MRPC data were taken at 900 rpm. Data have been analyzed to show equivalency between an MRPC at 900 rpm [12.7 mm/s (0.5 in./s)] and an MRPC at 300 rpm 2.54 mm/s (0.1 in./s) because the lower rpm can be found in field inspections. A Lissajous figure from a mock-up flaw at 2.54 mm/s (300 rpm) using a +Point coil and a Lissajous figure from a mock-up flaw at 12.7 mm/s (900 rpm) using the same +Point coil are almost indistinguishable. Similar results have also been seen for other frequencies and coils.

2.1.2 Standards

An ASME standard and an 18-notch standard were used during all test section inspections. The ASME standard has 100, 80, 60, 40 and 20%TW holes, a TSP simulation ring, and ID and OD circumferential grooves. The notch standard (fabricated by Zetec Inc.) has 20, 40, 60, 80, and 100%TW, 6-mm-long ID and OD, axial and circumferential EDM notches. Before installation in the mock-up, a test section was scanned in tandem with the two standards. Figure 2.9. shows the stand and tube arrangement for inspections of degraded test sections. A Zetec 4-D pusher-puller, Zetec MIZ30 data acquisition system, and Zetec EddyNet 98 software were employed for data collection and analysis. During collection of data from the mock-up, whether with BC or MRPC, both standards were used before and after each tube, or section of tube, was scanned. Figure 2.10 shows schematic drawings of both standards.

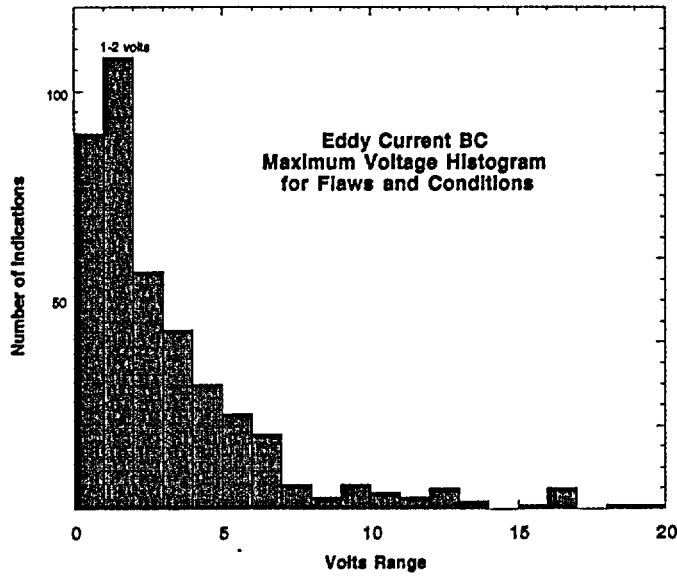


Figure 2.6
Bobbin coil voltage histogram for mock-up flaws and conditions

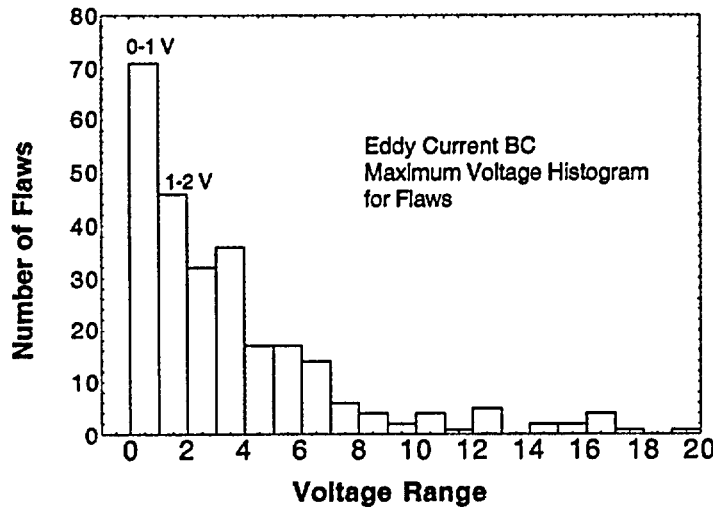


Figure 2.7
Bobbin coil voltage histogram for mock-up flaws

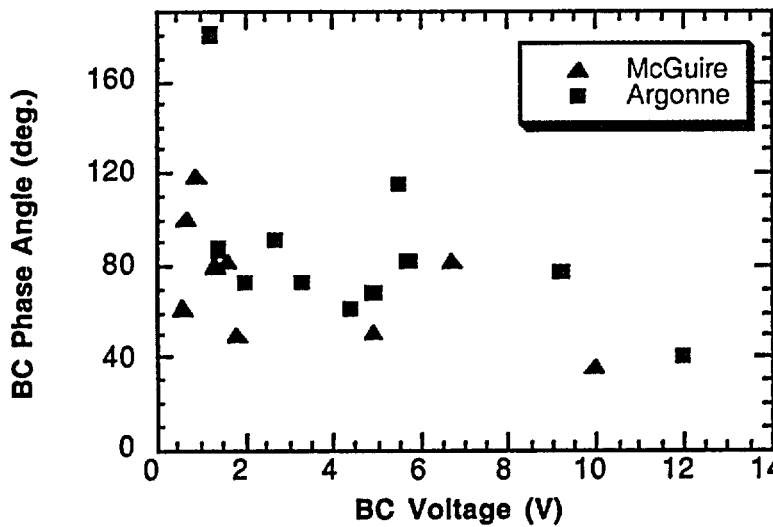


Figure 2.8
Comparison of bobbin coil voltage and phase for representative cracks in mock-up and McGuire field data. Phase/voltage relationships are similar.

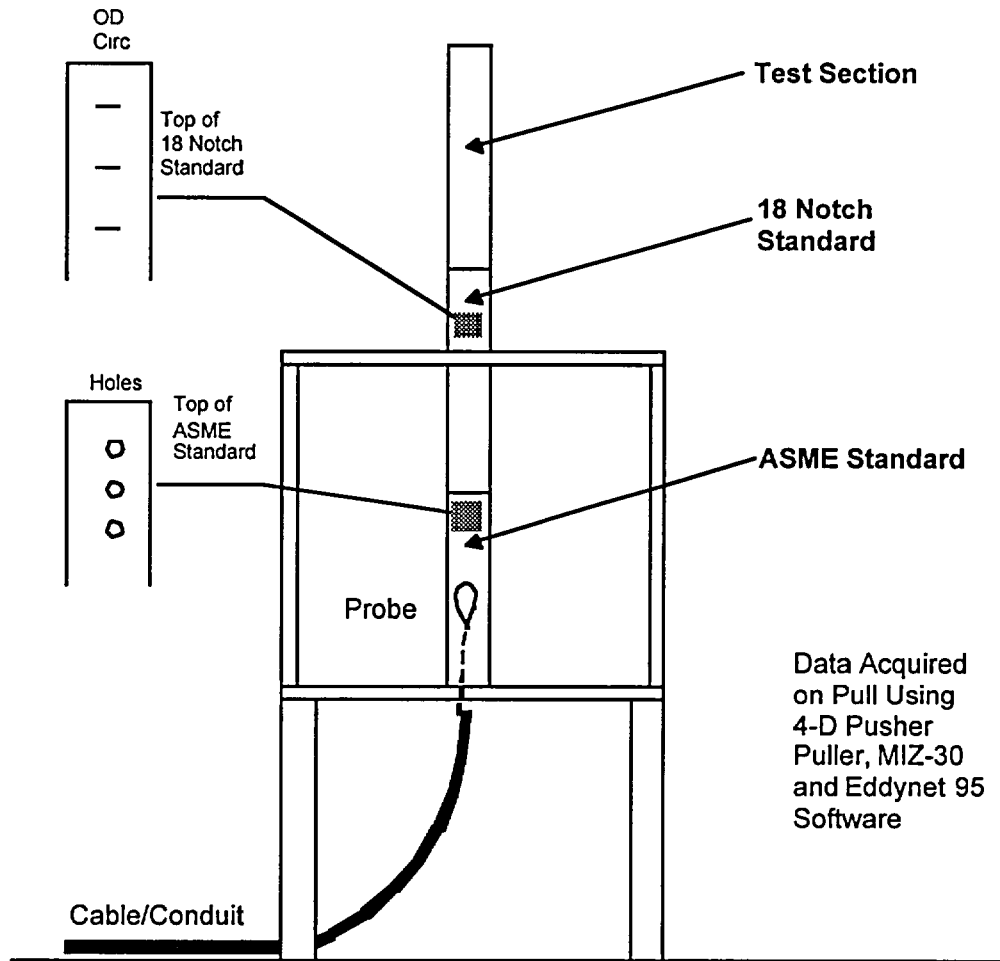


Figure 2.9 Schematic drawing showing configuration of stand, standards, and degraded test section during an eddy current inspection of a single test section

2.1.3 Flaw Fabrication and Morphology

2.1.3.1 Justification for Selection of Flaw Types

The flaw types selected for the mock-up are those currently found in operating steam generators. Since about 1980, steam generator tube degradation has been dominated by stress corrosion cracking (SCC), which can occur on either the primary or secondary side, unlike the wastage and denting that occur exclusively on the secondary side (OD) of the tubes. Primary water stress corrosion cracking (PWSCC) is most likely to occur at regions of high residual stress, such as the tube expansion transition and immediately above the tubesheet, at U-bends (particularly the small-radius U-bends), and in tube regions deformed by secondary-side denting. As a result, the mock-up consists primarily of ID and OD SCC at the TSP (with and without dents), at and above the roll transitions, as well as in the freespan. Outer-diameter intergranular attack (IGA) commonly occurs in crevices or under corrosion product scales. Such locations include the TSP crevice, the region near the top of the tube sheet, freespan areas under corrosion products or deposits, and regions under sludge buildup. As a result, some outer-diameter IGA is present in the mock-up. In addition, there are some fatigue cracks, some test sections with wastage, and some with wear.

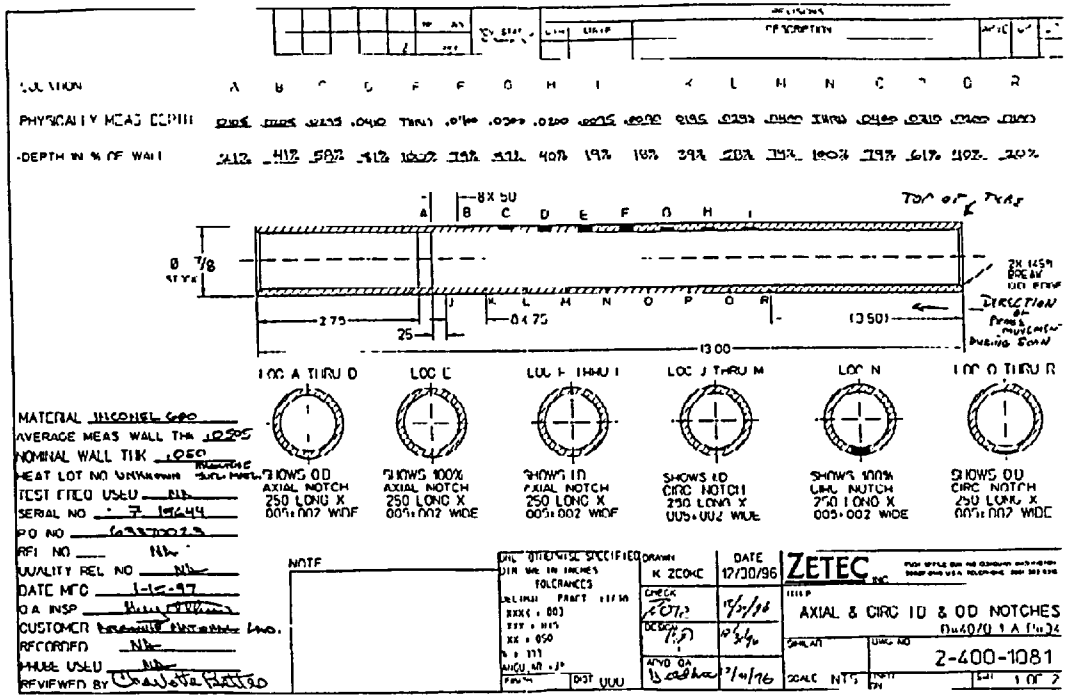
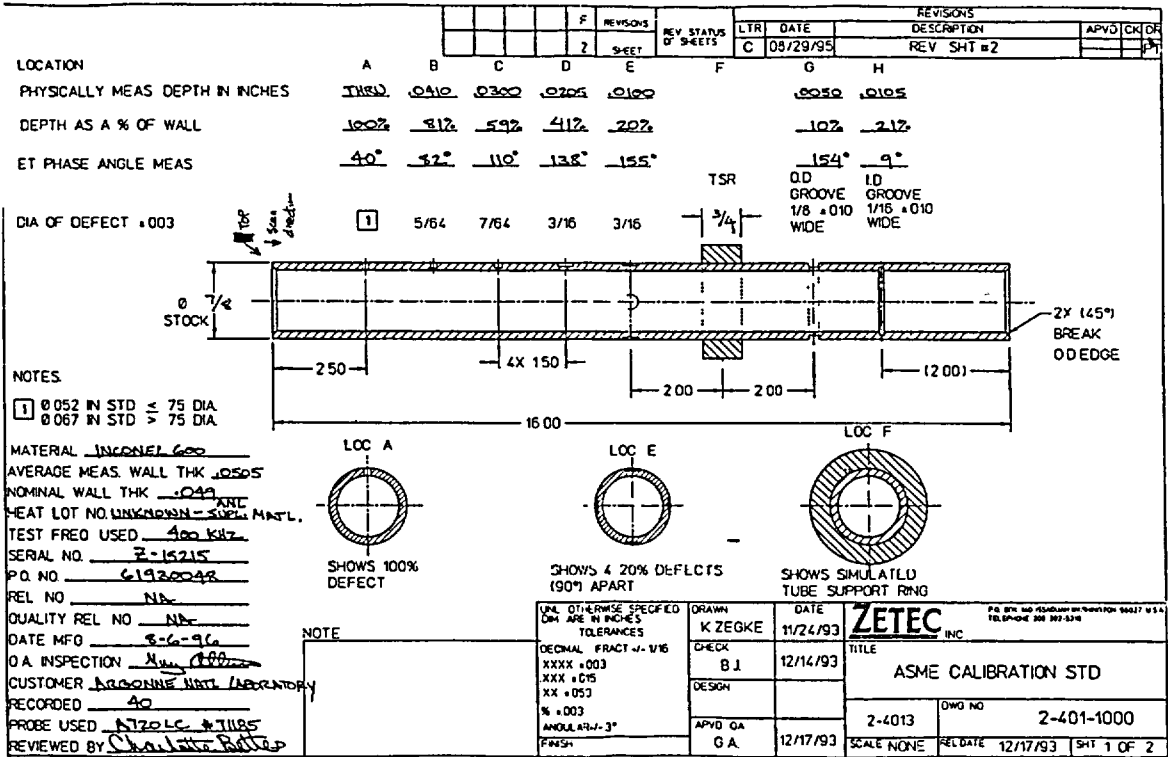


Figure 2.10 Schematic drawing of ASME (top) and 18-notch standard (bottom) used when scanning degraded test sections and mock-up tubes.

2.1.3.2 Process for Fabricating Cracks

Alloy 600 test sections at ANL were cracked by using a 1M aqueous solution of sodium tetrathionate at room temperature and atmospheric pressure. Techniques of localized environmental exposure, low applied load, and electrochemical potential were utilized to produce various crack geometries. Masking by coating areas of the tubes with lacquer was used to limit or localize the cracking area. The tubes were internally pressurized to generate hoop stresses to produce axial cracks and axially loaded to produce circumferential cracks. The times to produce cracking ranged from 20–1000 h, depending on the type of crack being produced. A variety of OD and ID crack geometries were produced; axial, circumferential, skewed, or combinations of these. Many of the specimens contained multiple cracks separated by short axial or circumferential ligaments. Prior to exposure to the sodium tetrathionate solution, specimens were sensitized by heat-treating at 600°C (1112°F) for 48 h to produce a microstructure that is susceptible to cracking. Protective sleeves were used to prevent scratching or other mechanical damage to the test sections. An identification alphanumeric (ID) was permanently inscribed on the OD at both ends of each test section (Figure 2.11). All documentation is referenced to the test section ID. The mock-up was seeded with sensitized flaw-free test sections with and without artifacts so that the possibility of distinguishing sensitized from unsensitized test sections would not be an indicator that a flaw was present in that test section. In addition, many cracks were grown without sensitizing the test sections from Westinghouse.

Dye penetrant examinations were carried out for degradation on the OD. After completion of the degradation process, test sections were ultrasonically cleaned in high-purity water and dried. Dye penetrant examinations (PT) were performed in the vicinity of degradation for many test sections. The PT was carried out with Magnaflux Spotcheck SKL-SP Penetrant and SKC-S Cleaner/Remover. If SKL-SP Penetrant provided an unsatisfactory result, Zyglo 2L-27A Penetrant was used with Magnaflux Zyglo 2P-9f Developer as an alternate process.

The results of dye penetrant examination were documented by photography at 0.5–5X magnification. The photograph includes a calibrated scale so that magnification factor may be measured directly from the photograph (Figure 2.12).

Cross-sectional microscopy was performed on metallographically polished surfaces of many samples to provide documentation of the mock-up crack morphology. Figure 2.13 shows examples of LODSCC. The specimens were sometimes etched to delineate grain boundaries and other microstructural features, by electrolytic etching in 5% nitric acid–alcohol solution at 0.1 mA/mm² for 5-30 seconds. The etching may also enhance contrast of the image, but the tip of a tight intergranular crack could be confused with a grain boundary. Photographic images were recorded at 10–500x magnifications. Cracks in the mock-up provided by PNNL (about 50) were produced by Westinghouse with a doped steam method that is proprietary and will not be discussed here. Axial and circumferential cracks both ID and OD were produced for the freespan, TSP, and roll transitions. Several IGA specimens, as well as fatigue and wastage samples, were also provided by PNNL. Figure 2.14 shows sketches of some dye penetrant images of ODS/SCC provided by PNNL for the mock-up.

2.1.3.3 Matrix of Flaws

Table 2.2 shows the distribution of flaw types. In this section, the flaw types and their depths are presented. The flaw depths are distributed into three ranges, 0-40%TW, 41%-80%TW, and 81-100%TW. The distribution is skewed toward deeper cracks. This is necessary to obtain high confidence in the high

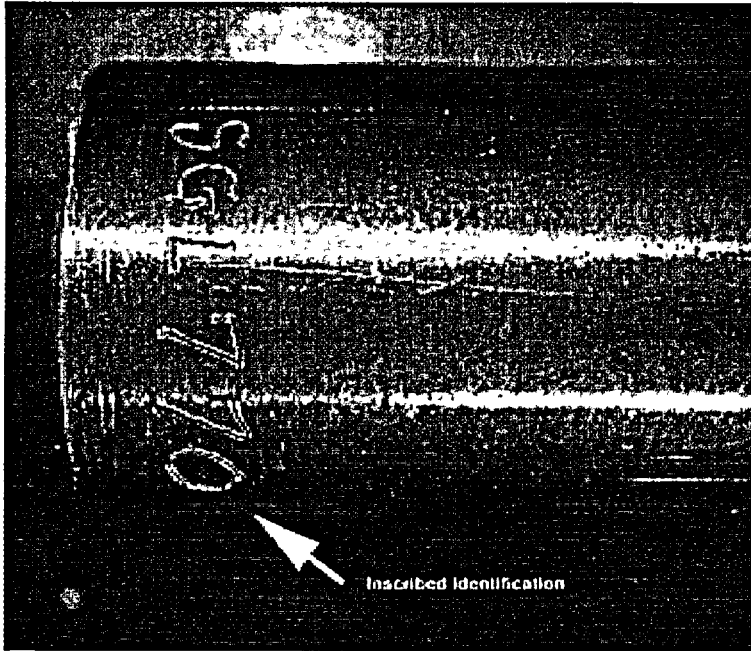


Figure 2.11
Inscribed identification of tube specimen

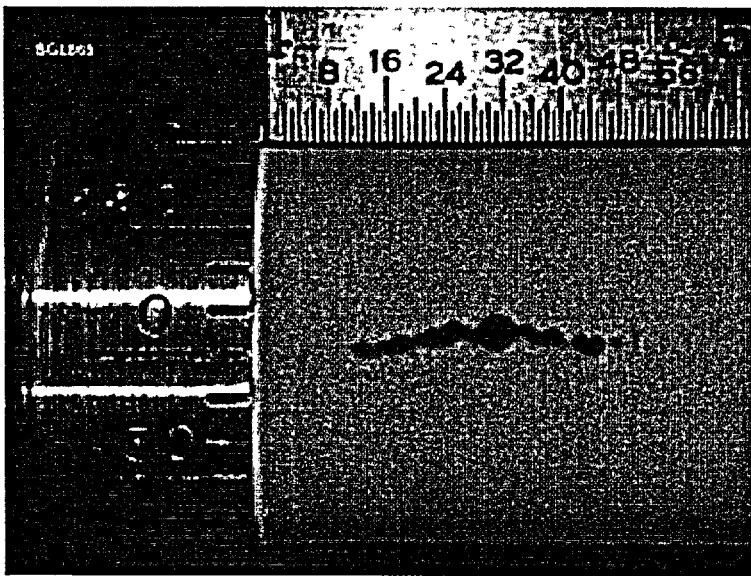


Figure 2.12
Dye penetration examination of tube specimen SGL865 showing an LODSCC.

POD for the deeper cracks. Draft Regulatory Guide 1074 (Steam Generator Tube Integrity) describes criteria for performance demonstrations to quantify defect detection performance (POD for a given defect). While the distribution of flaw sizes for the round-robin is not as uniform as required in DG 1074, other requirements involving extraneous signals, signals from fabricated defects, detection and false calls, have, for the most part, been met.

2.1.3.4 Crack Profiles by Advanced Multiparameter Algorithm and Comparison to Fractography

As part of the development of the multiparameter algorithm, results have been compared to fractographic results on a wide variety of SCC cracks and EDM and laser notches. To provide an

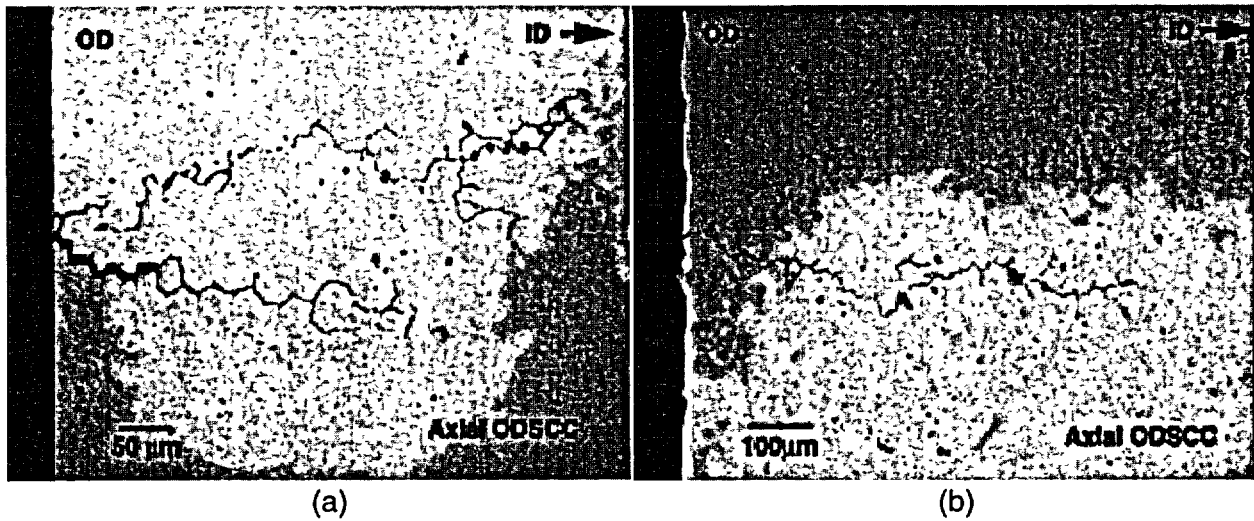


Figure 2.13 Cross-sectional optical metallography: (a) branched LODSCC, (b) LODSCC.

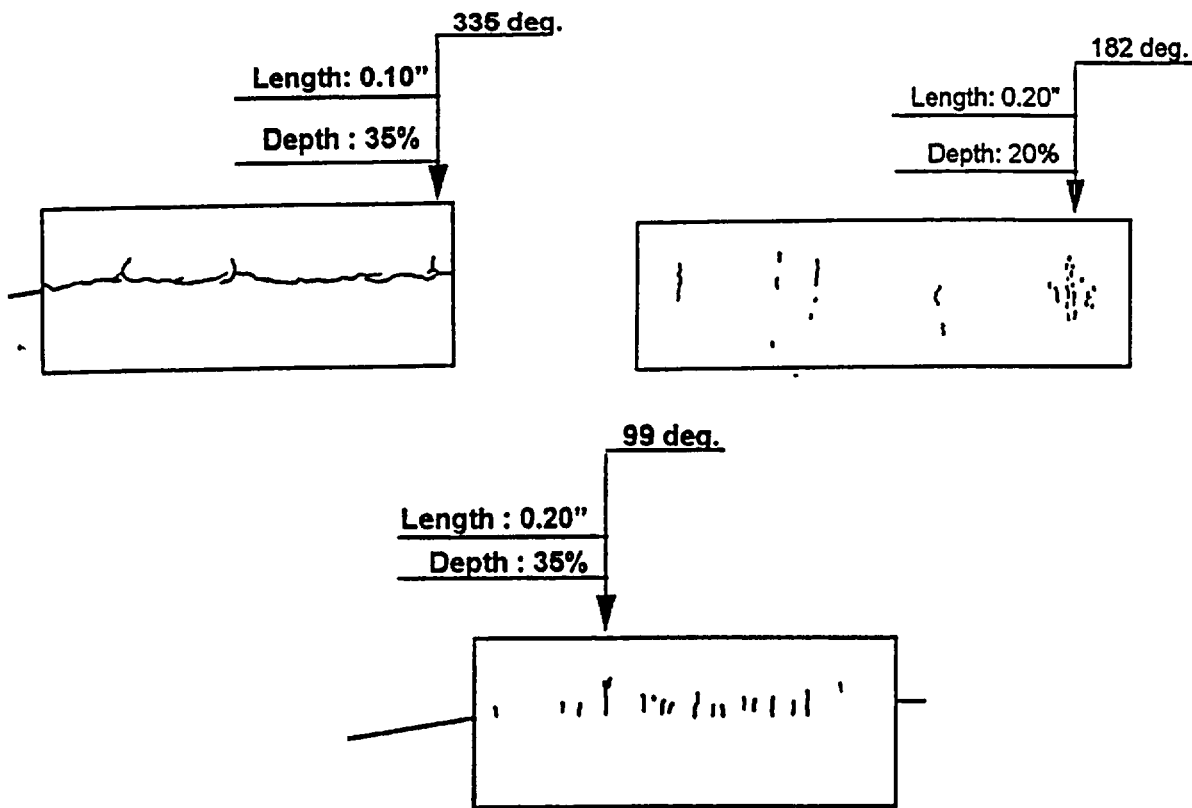


Figure 2.14 Sketch of dye penetrant images of three ODSCCs in mock-up. Test section axis is vertical. Top-left SCC is circumferential; top-right and bottom sketches show numerous LODSCCs distributed around the circumference. Bottom sketch shows a series of LODSCCs at the roll transition.

Table 2.2 Distribution of Flaw Types

Maximum Depth Range	EDM & Laser-Cut Slots	IGA	ODSCC TS	ODSCC TSP	ODSCC Freespan	PWSCC TS	PWSCC TSP	PWSCC Freespan	Wear/Wastage	Fatigue
0-40%TW	7	2	3	14	15	4	8	1	6	0
41-80%TW	13	9	2	14	26	8	16	0	6	0
81-100 %TW	1	2	16	41	49	35	7	3	0	3

objective benchmark, however, an additional set of 29 SCC cracks was produced and used in a blind test of the predictions of the algorithm against fractographic measurements of the crack geometry. Six of the benchmark samples have not yet been destructively analyzed because they will also be used for leak and ligament rupture tests that have not yet been performed.

The stress corrosion cracks for the blind test were produced by the same technique in 1M aqueous solutions of sodium tetrathionate described in the previous page. A variety of OD and ID crack geometries were produced; axial, circumferential, skewed, or combination of these. Many of the specimens contained multiple cracks separated by short axial or circumferential ligaments. Cracked tubes were examined by dye penetrant techniques, conventional eddy current NDE, the multiparameter algorithm, and by destructive methods.

2.1.3.4.1 Procedures for Collecting Data for Multiparameter Analysis

A description of data collection procedures for multifrequency inspection of the mock-up tubes is provided in Section 2.2.2.1.2. These guidelines define the instrumentation setup (coil excitation frequencies, gain setting, cable length, sampling rate, probe speed, etc.) and calibration procedures for a given probe (e.g., bobbin, rotating, and array probes). Although the quality of data affects both detection and sizing, this issue is of particular concern when quantitative estimates of flaw size are to be determined. The multiparameter algorithm used to obtain flaw size estimates for the mock-up requires data at three frequencies and the minimum sampling rate recommended in the ETSS for MRPC probes. The multiple-frequency EC data were acquired with a standard three-coil rotating probe that incorporates a 2.92-mm (0.115-in.) mid-range primary pancake coil, a mid-range +Point™, and 2.03-mm (0.080-in.)

high-frequency pancake coil. Initial amplitude profiles are obtained from the +Point coil at a single channel. The final estimated depth profiles are obtained by using multichannel information from the mid-range primary pancake coil for multiparameter data analysis. A detailed description of the algorithm and the data quality issue is given in Ref. 2, which also describes the conversion of EddyNet formatted data to a standard format for off-line analysis.

2.1.3.4.2 Fractography Procedures

For the destructive examination, the samples were heat-tinted before fracture to permit differentiation of the SCC and fracture opening surfaces. The specimens were then chilled in liquid nitrogen and cracks were opened by fracture. The fracture surfaces were examined macroscopically and with optical and scanning electron microscopy. The fractography and NDE data were digitized to obtain tabular and graphical comparisons of the depths as a function of axial or circumferential position. Well-defined markers on the test sections provided a means to accurately overlap the profiles.

Individual pieces of the specimen resulting from fracture are clearly identified, marked with new IDs, and documented.

The fractured surfaces are recorded by digital photography at a 0.2–10X magnification (Figure 2.15). Methods of illuminating the fracture surface play an important role in obtaining the optimal image quality of the degradation. Optimal illumination may be found by a trial-and-error method. For a large crack, photographs may be taken for partial areas, and then a whole composite photograph may be constructed later. All digital photographs have been identified with a unique and proper file name that is traceable to particular degradation and tube.

2.1.3.4.3 Procedure for Comparing Multiparameter Results to Fractography

Crack profiles were obtained by digitizing the photographs of the fracture surfaces and drawing lines through the points. The sampling distance depends on the complexity of the crack geometry. Short sampling distances were used for complicated geometries over a small scale, while longer distances were used for simpler geometries, e.g., straight-line or smooth contours. Fractography and NDE results were plotted in a same figure for comparative purpose. (e.g., see Figure 2.16). Drawing lines through the EC data points generates the NDE profiles (nominally 30 per inch around the

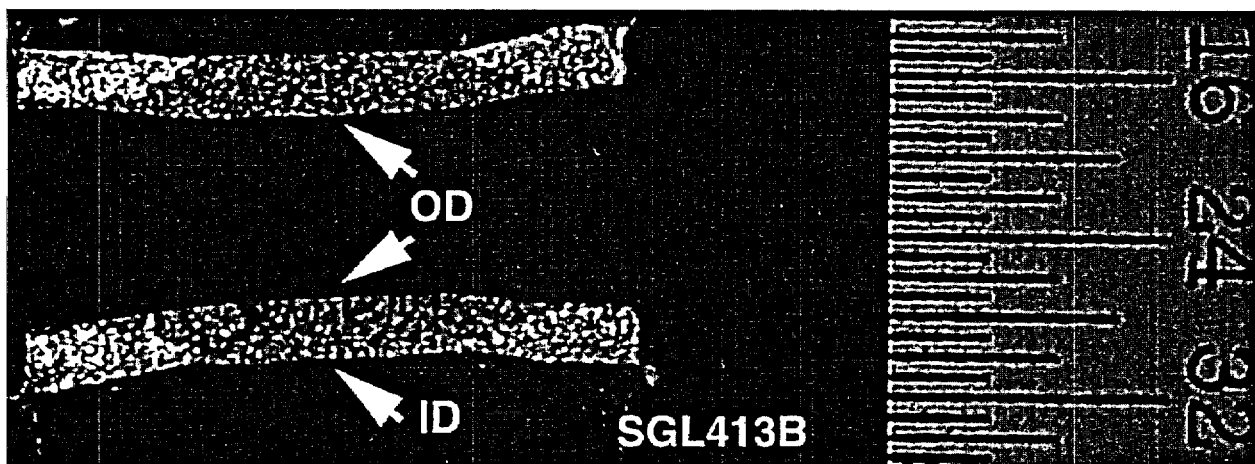


Figure 2.15 Fractography of tube specimen SGL413

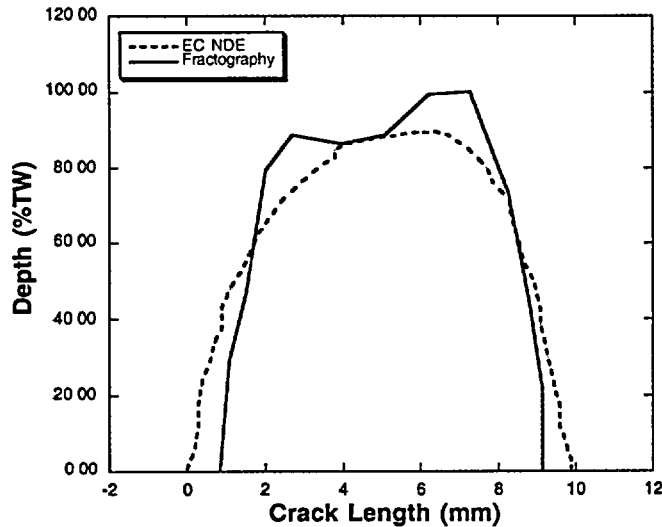


Figure 2.16
 Sizes and shapes of LODSCCs in tube specimen AGL 536 determined by EC NDE using the multiparameter algorithm (dotted curve) and fractography (smooth curve).

circumference and 30 per inch axially). The NDE and fractography profiles were then compared at many axial and circumferential positions, and the differences were used to establish the NDE uncertainty as a function of depth. The NDE uncertainties were then used in generating the lower 95% confidence limits for the POD curves presented in the report.

2.1.3.4.4 Multiparameter Profiles vs. Fractography for Laboratory Samples

In the development of the multiparameter algorithm, the results from the algorithm have been compared to fractographic results on a wide variety of SCC cracks and EDM and laser-cut notches. To provide an objective benchmark, however, additional SCC were produced and used for a blind test of the predictions of the algorithm against fractographic measurements of the crack geometry. Crack profiles from the destructive analyses are compared with those obtained from multiparameter algorithm in Figs. 2.17-2.39. Figure 2.40 shows maximum depths as determined by fractography to maximum depths determined by the multiparameter algorithm. A linear regression fit and 95% confidence bounds for the observed data as a function of the multiparameter estimates are shown in the figure. The overall root mean square error (RMSE) in the predicted maximum depths is 13.7%. If the comparison is limited to deeper cracks, the RMSE is smaller, 9.7% for depths 30–100%, and 8.2% for ODSKC of depths 50–100%. The data are too few, however, to determine whether the apparent variation of the RMSE with depth is statistically significant.

Because the field of view of the rotating pancake probe is limited, the depth measurements at points ≥ 5 mm apart along the crack profile are essentially independent and additional comparisons of the estimated depth with that determined by fractography were made at various points along the crack profile. To avoid observer bias in the selection of the data for comparison, the intersections of the crack profiles with the major grid lines in the graphs of the superimposed profiles were chosen as the points for the comparison. This corresponds in most cases to a spacing of 5 to 10 mm between points. Figures 2.41 and 2.42 show the results for 89 points from 20 different cracks, axial and circumferential, ID and OD. A linear regression curve and 95% confidence bounds for the observed data as a function of the multiparameter estimates is shown. The intercept is 13.8 in this case, somewhat less than that generated from the maximum depth data, but the slope of 0.79 is almost identical to the linear regression line slope for the maximum depth data.

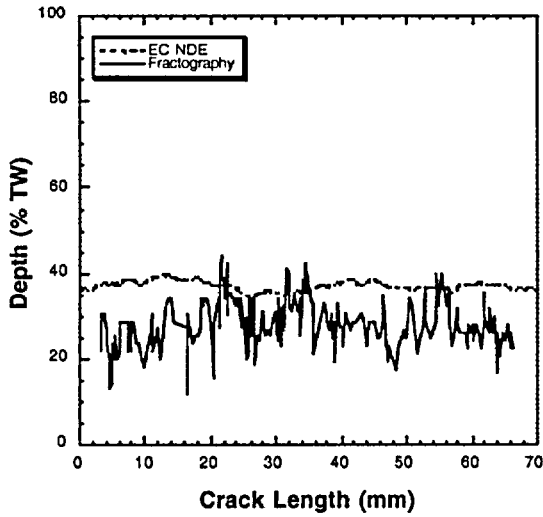


Figure 2.17
 AGL 2241 CODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

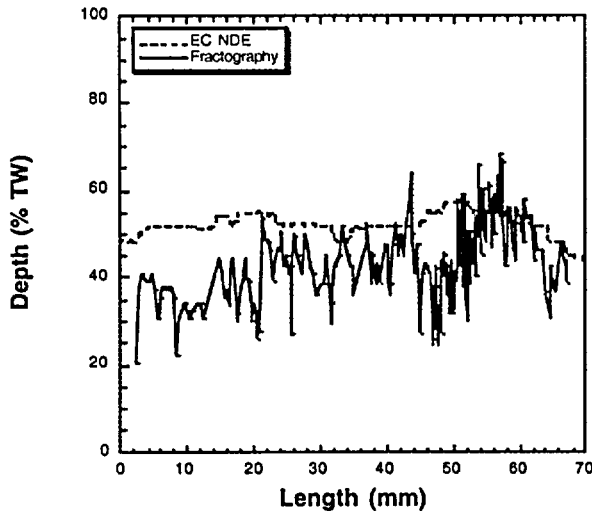


Figure 2.18
 AGL 2242 CIDSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

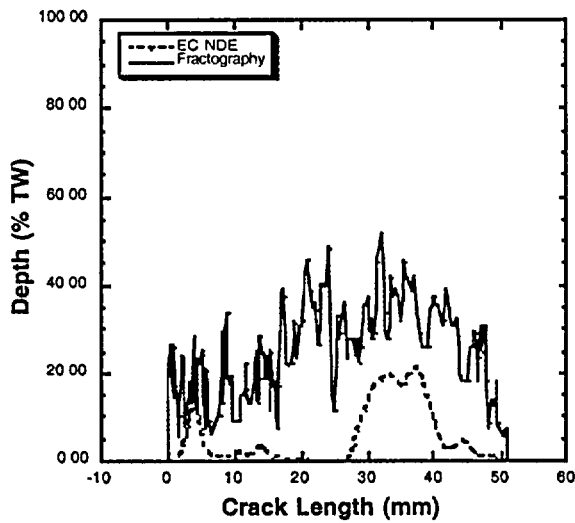


Figure 2.19
 AGL 288 LIDSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

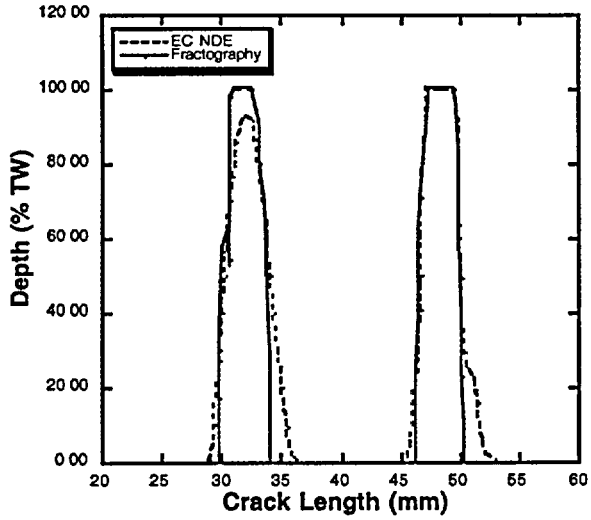


Figure 2.20
 AGL 394 CODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

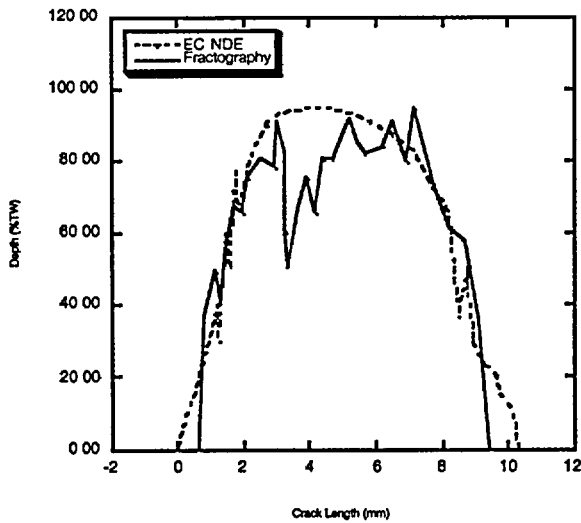


Figure 2.21
 AGL 533 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

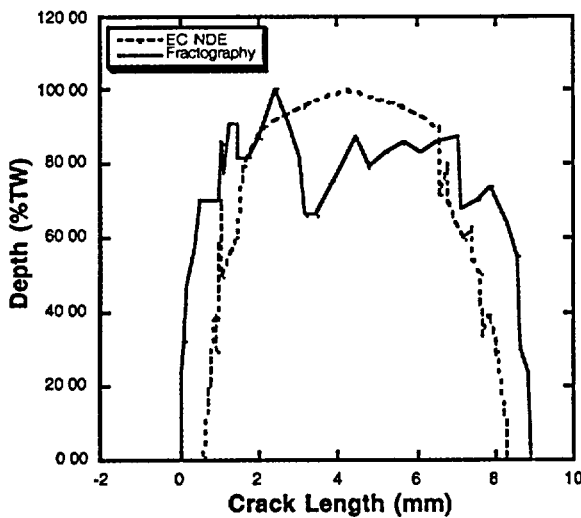


Figure 2.22
 AGL 535 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

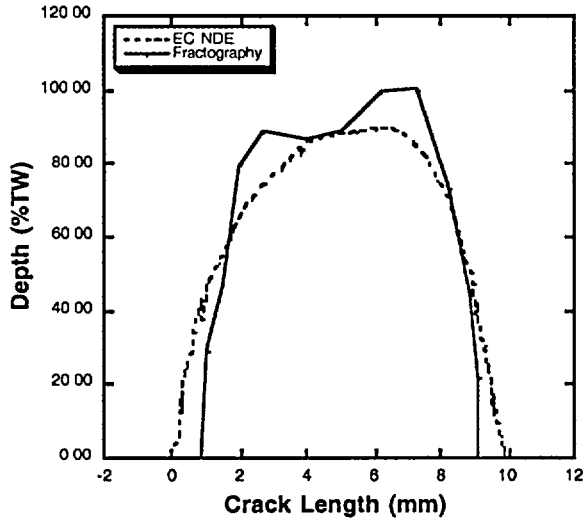


Figure 2.23
 AGL 536 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

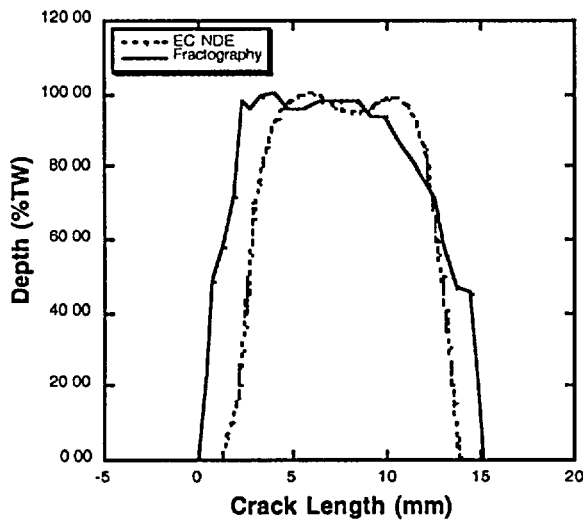


Figure 2.24
 AGL 503 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

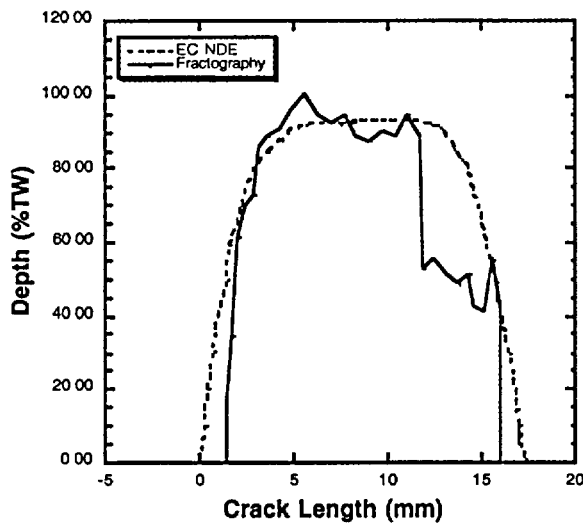


Figure 2.25
 AGL 516 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

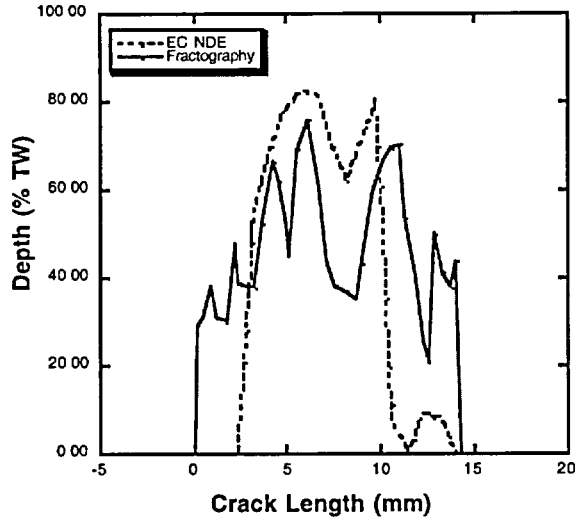


Figure 2.26
 AGL 517 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

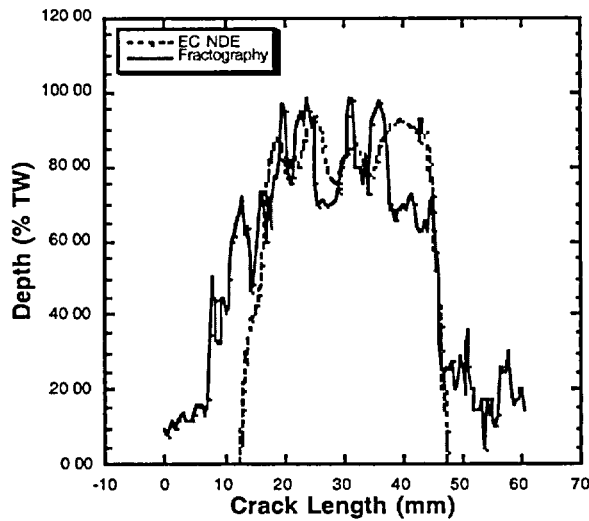


Figure 2.27
 AGL 824 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

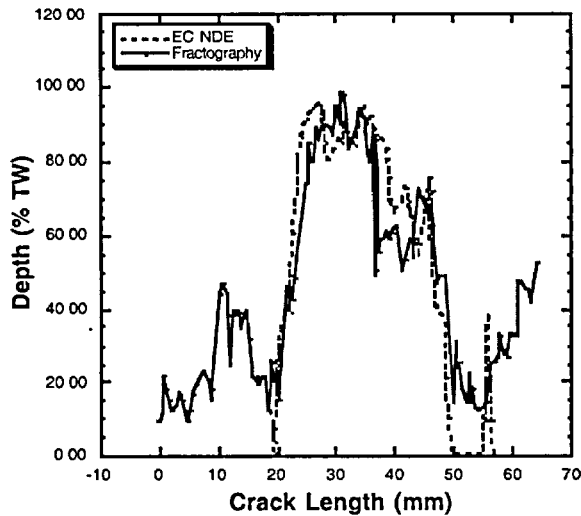


Figure 2.28
 AGL 826 CODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

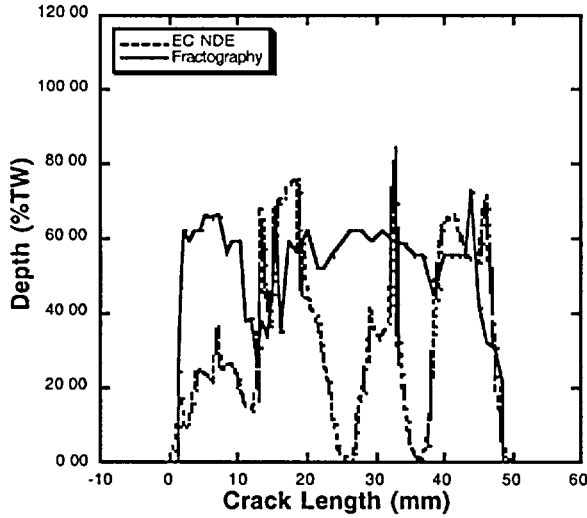


Figure 2.29
AGL 835 LODSCC:
EC NDE depth versus position using the
multiparameter algorithm (dotted curve)
and fractography depth versus position
(smooth curve).

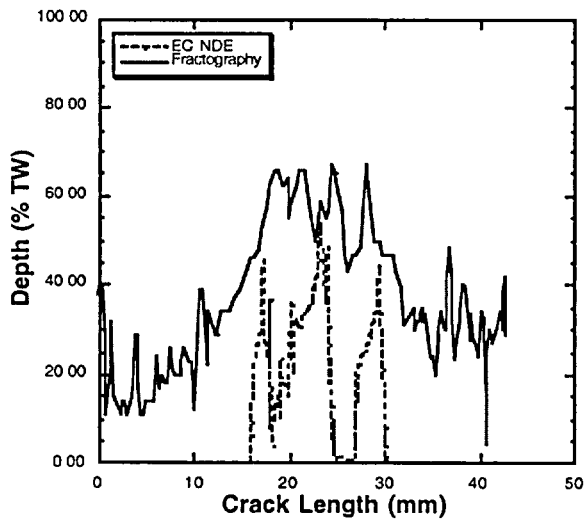


Figure 2.30
AGL 838 CODSCC:
EC NDE depth versus position using the
multiparameter algorithm (dotted curve)
and fractography depth versus position
(smooth curve).

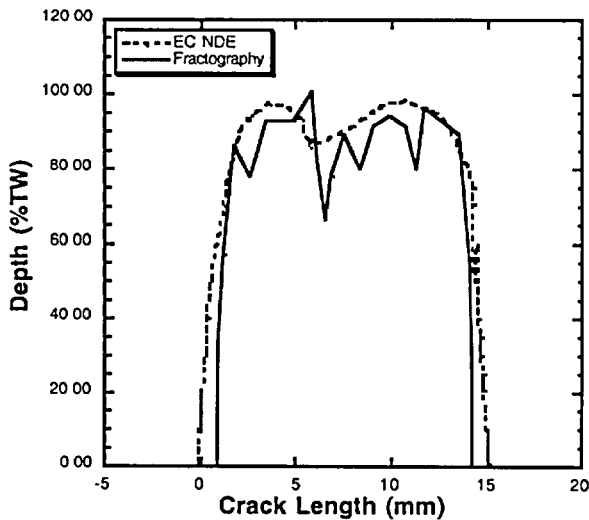


Figure 2.31
AGL 854 LODSCC:
EC NDE depth versus position using the
multiparameter algorithm (dotted curve)
and fractography depth versus position
(smooth curve).

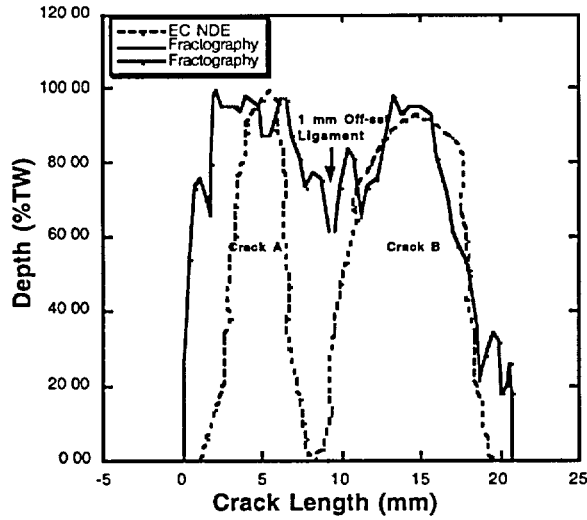


Figure 2.32
 AGL 855 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

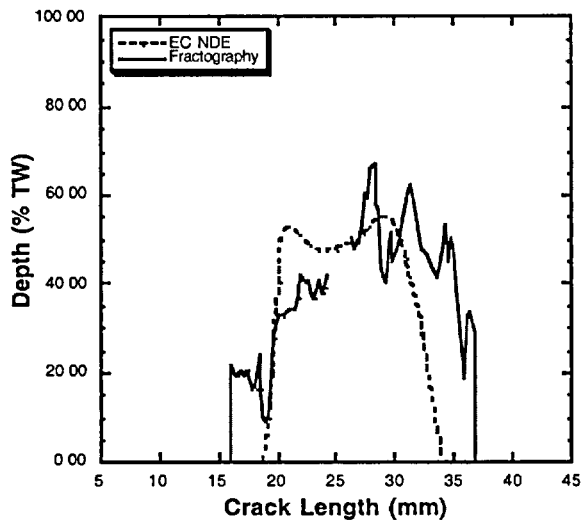


Figure 2.33
 AGL 861 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

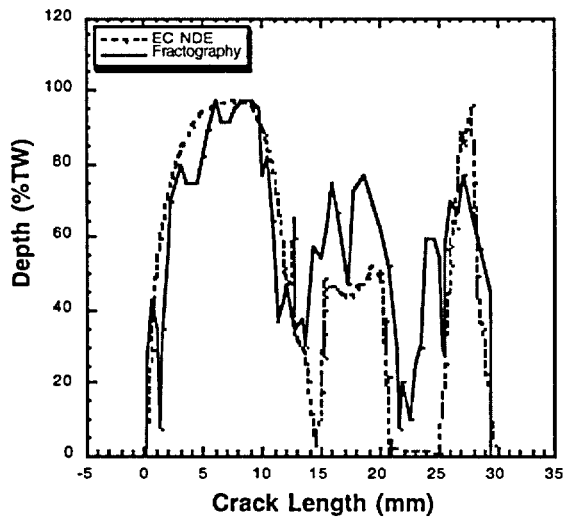


Figure 2.34
 AGL 874 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

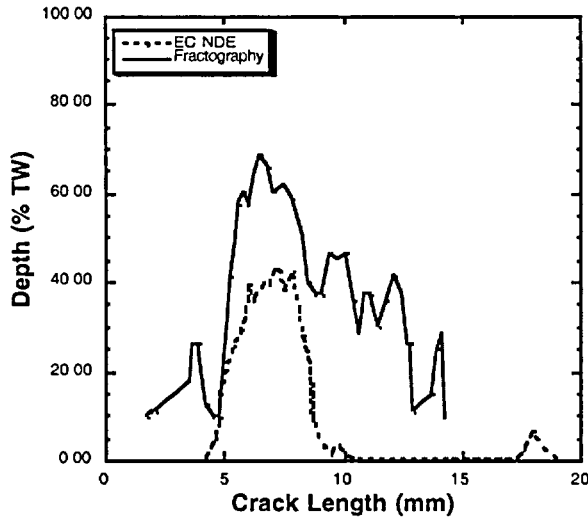


Figure 2.35
 AGL 876 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

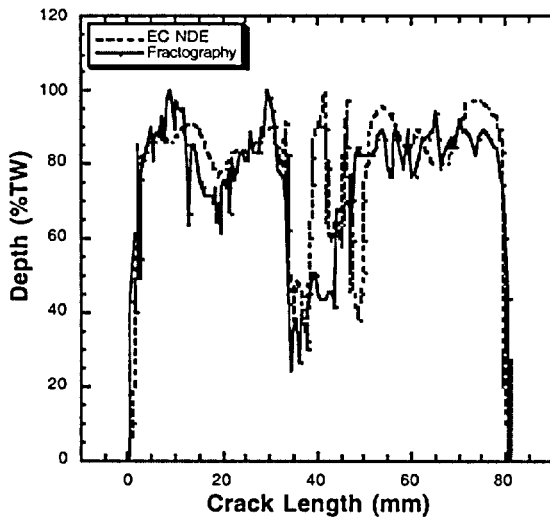


Figure 2.36
 AGL 883 LODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

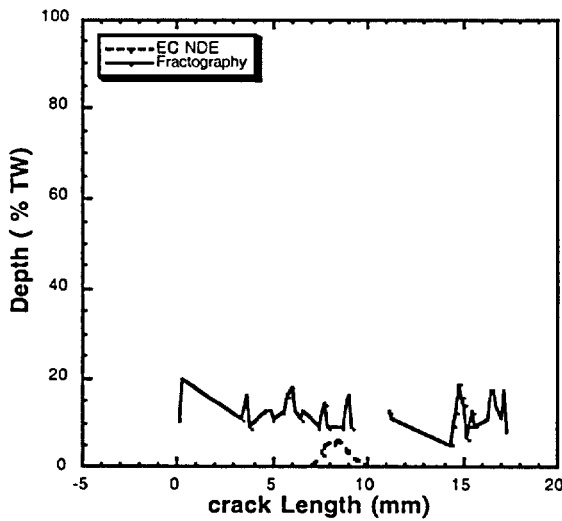


Figure 2.37
 AGL 893 CODSCC:
 EC NDE depth versus position using the
 multiparameter algorithm (dotted curve)
 and fractography depth versus position
 (smooth curve).

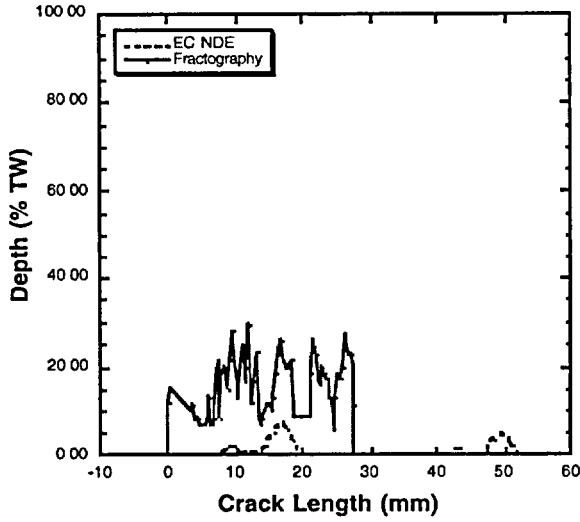


Figure 2.38
AGL 8161 LIDSCC:
EC NDE depth versus position using the
multiparameter algorithm (dotted curve)
and fractography depth versus position
(smooth curve).

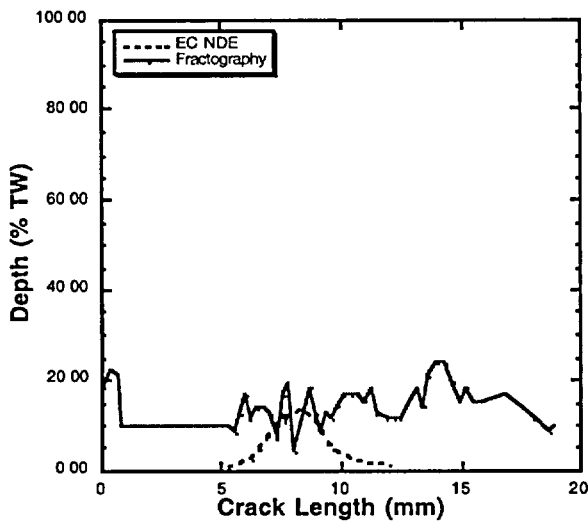


Figure 2.39
AGL 8162 LIDSCC:
EC NDE depth versus position using the
multiparameter algorithm (dotted curve)
and fractography depth versus position
(smooth curve).

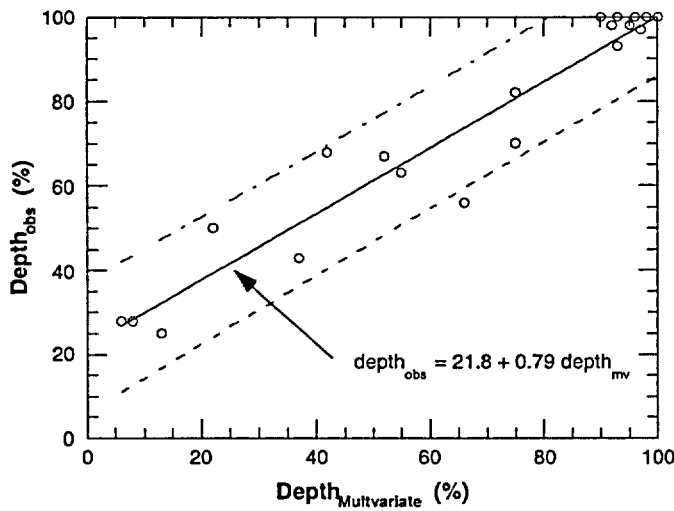


Figure 2.40
Comparison of maximum depth
determined by the multiparameter
algorithm with that determined by
fractography

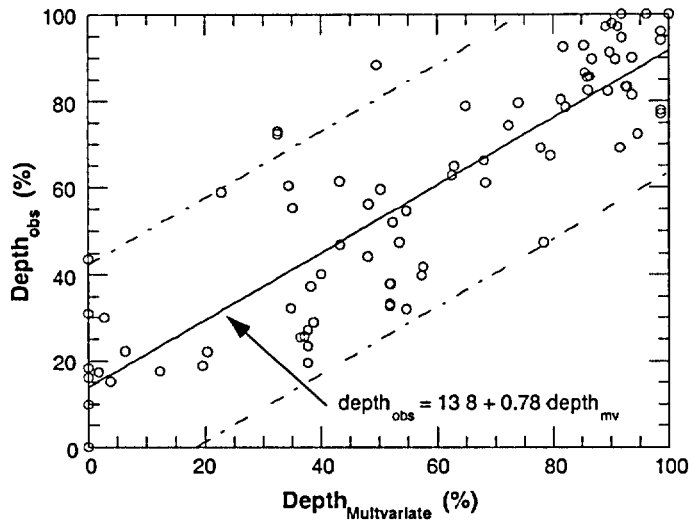


Figure 2.41
Comparison of depths (%TW) determined by the multiparameter algorithm with those by fractography and regression fit and estimated 95% bounds of the observed depth as a function of the multiparameter depth estimate.

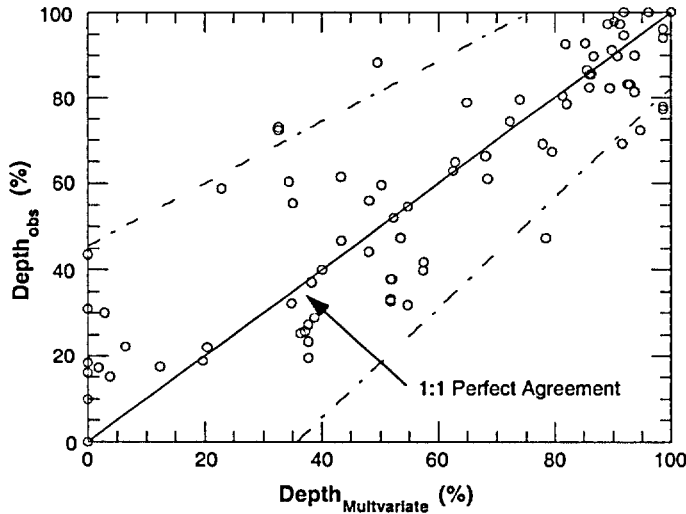


Figure 2.42
Comparison of depths (%TW) determined by the multiparameter algorithm with those by fractography. In this case, the observed and predicted results are shown in terms of the "perfect agreement" 1:1 line and estimated 95% bounds that account for the variation in the uncertainty with depth.

A set of 20 test sections analyzed with the multiparameter algorithm was destructively analyzed by PNNL in an exercise carried out before the 23 test section set was evaluated. While these 20 test sections, prepared by doped-steam techniques, represented a small subset of the mock-up test sections, the NDE results from this set provided the guidance for selecting the multiparameter approach. Many NDE techniques were evaluated before selecting the multiparameter algorithm for establishing the reference state of the mock-up flaws. The evaluated techniques include phase analysis of EC +Point data, multivariate regression analysis of EC data, multiparameter analysis of EC data with neural networks, high-frequency ultrasonics (UT) from the OD, Lamb waves, acoustic microscopy and a combination of UT and EC data (from the ID). The multiparameter algorithm provided the best accuracy for sizing the cracks. The capability of the multiparameter algorithm for characterizing cracks from the 20-test-section set is shown in Fig. 2.43. Here, the EC depth estimates for the 10 OD LODSCC and CODSCC are compared with actual depths from metallographic destructive analysis. In general, estimates of flaw depth are accurate to within about 10% TW. Note that this approach to sizing would have to be reviewed if used by industry for an alternate repair criteria. The current approach to carrying out a performance demonstration is to metallographically section the specimens used. Qualifications are based on sectioning.

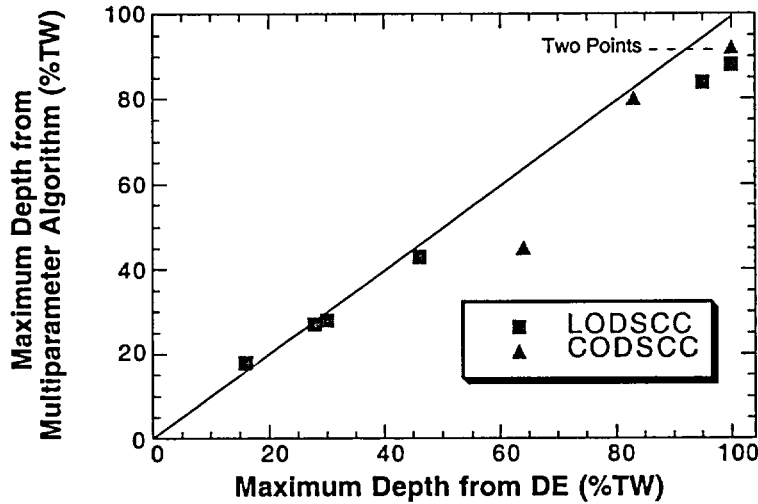


Figure 2.43
Maximum eddy current depth as percent throughwall (%TW) using a pancake coil and multiparameter algorithm for 10 LODSCC and CODSCC from a 20-test-section set vs. destructive analysis result. Destructive analysis was carried out using metallographic sectioning techniques.

In Figure 2.44, estimates of crack depths by the multiparameter algorithm are compared with estimates of maximum crack depth using +Point phase analysis at 300 kHz. Significant differences in maximum depth estimates can be seen. The comparison was made by using test sections from the 23-tube set that was destructively analyzed and profiled by fractography.

In addition to comparing crack depths as determined by the multiparameter algorithm with those estimated by +Point phase analysis, comparisons have also been made to depth estimates from amplitude and phase of bobbin coil signals. Figure 2.45 compares depth as determined by the multiparameter algorithm to the maximum voltage in the bobbin coil EC signal for mock-up cracks. The correlation between bobbin coil signal amplitude and depth of mock-up cracks is poor for either freespan or TSP cracks. The correlation between bobbin coil phase angle and depth of mock-up TSP cracks is also poor, as can be seen in Figure 2.46 for LODSCC and in Figure 2.47 for LIDSCC. The use of bobbin coil voltage or phase angle can result in very large errors in predicting crack depths. For example, a 3-V bobbin coil signal could be generated by cracks ranging in depth from 25-100% TW. Predicting depth from bobbin coil phase angle is just as uncertain.

2.1.3.4.5 Characterization of Cracks in Terms of m_p

Although the probability of detection is normally expressed in terms of the maximum depth of the crack, it is also useful to express POD in terms of a parameter that better characterizes the structural integrity (i.e., ligament rupture) of the tube. A useful parameter for this purpose is m_p , which is defined as:

$$m_p = \frac{p_b}{p_{sc}}, \quad (1)$$

where p_b is the bursting pressure of an unflawed tube and p_{sc} is the ligament failure pressure of a part-throughwall crack. The parameter m_p can be interpreted as a stress multiplier that relates the stress in the ligament ahead of the crack to stress in an unflawed tube under the same loading. Because it incorporates

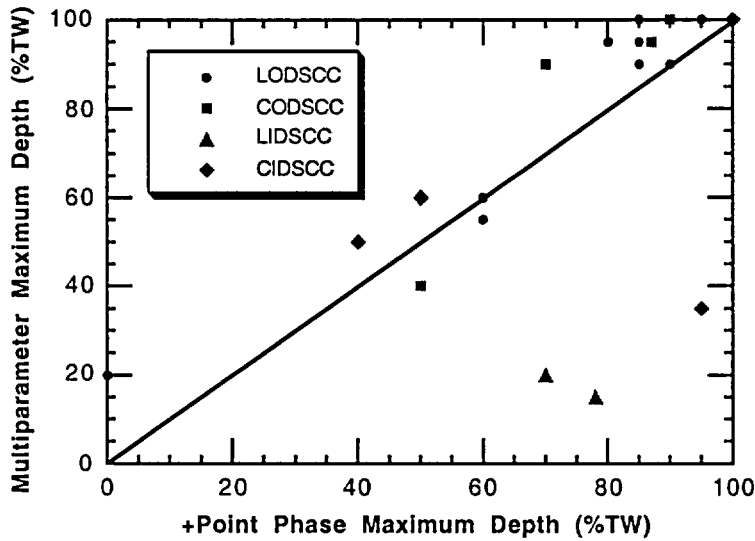


Figure 2.44
Estimates of crack depths by the multiparameter algorithm compared with estimates of maximum crack depth using +Point phase analysis at 300 kHz.

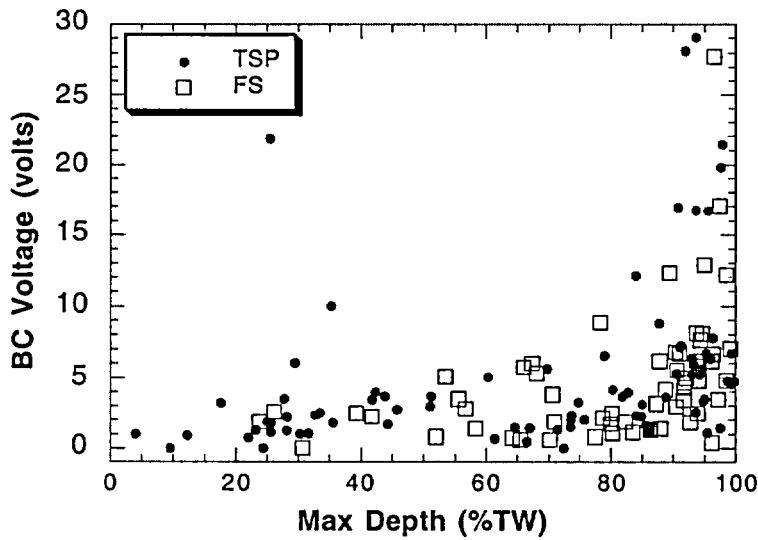


Figure 2.45
Maximum bobbin coil voltage as a function of maximum crack depth for mock-up FS and TSP SCC. The eddy current multiparameter algorithm was used to profile the crack and determine the maximum depth.

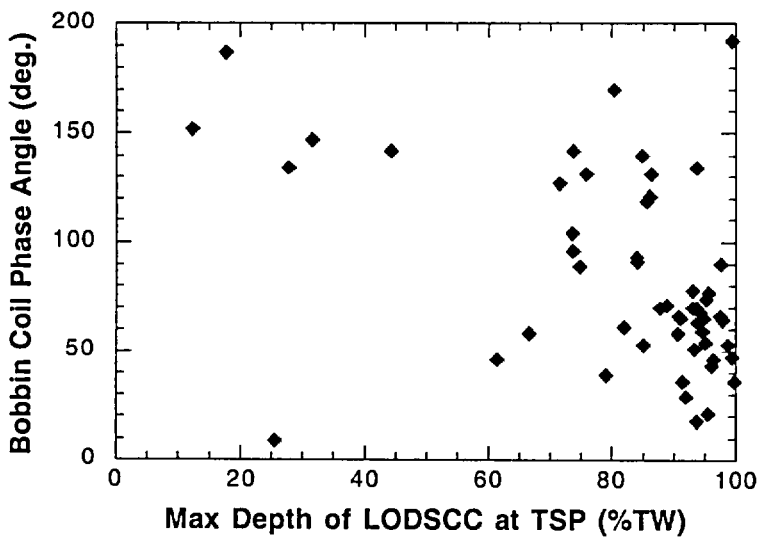


Figure 2.46
Bobbin coil phase angle as a function of maximum crack depth for mock-up TSP LODSCC. The eddy current multiparameter algorithm was used to profile the crack and determine the maximum depth.

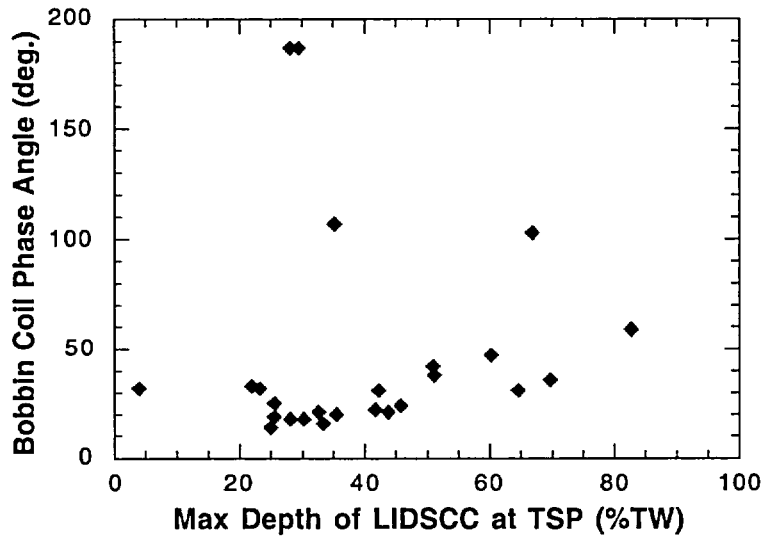


Figure 2.47
Bobbin coil phase angle as a function of maximum crack depth for mock-up TSP LIDSCC. The eddy current multiparameter algorithm was used to profile the crack and determine the maximum depth.

the effect of both crack depth and length, it better characterizes the effect of a flaw on the integrity of a tube than does maximum depth. For short cracks, the ligament may not correspond to tube bursting pressure. The crack may just “pop” through without increasing in length. For rectangular cracks, m_p can be expressed as a function of the crack and tube geometries by using the correlation [3]:

$$m_p = \frac{1 - \alpha \frac{a}{mh}}{1 - \frac{a}{h}}, \quad (2a)$$

$$\alpha = 1 + 0.9 \left(\frac{a}{h} \right)^2 \left(1 - \frac{1}{m} \right), \quad (2b)$$

where a = crack depth, h = wall thickness of tube, and m = bulging parameter [3].

Although Eqs. 1 and 2a-b can be used to estimate the crack tip ligament rupture pressure of rectangular part-throughwall cracks, they are not directly applicable to laboratory-grown SCC cracks, which are irregular in shape and have variable depths along their lengths. Instead of being a single planar crack, they are composed of a family of crack segments in different planes.

Currently, there are no widely accepted models available for predicting the ligament failure pressure of cracks with such complex geometries. From a limit analysis viewpoint, it can be argued that the collapse behavior of a crack tip ligament with an irregular point-by-point variation of crack depth should be similar to a crack with a smoothed-out “average” crack depth profile. For the present, we assume that the average profile measured by the EC method is the one that is relevant for limit analysis. With this assumption, although the real crack may have short throughwall segments at a number of locations, from the standpoint of plastic collapse of the ligament, the tube behaves as if it has a smoothly varying average ligament thickness (or crack depth) profile.

Because the measured crack depth profile by ANL's EC algorithm is generally not rectangular (e.g., see Fig. 2.48), the following procedure was used to establish the length and depth of an equivalent rectangular crack: [3]

(a) Choose a crack depth d_o and assume that any crack segment with depth $d < d_o$ does not adversely affect the crack tip ligament rupture pressure of the tube (Fig. 2.48a). In other words, replace the original crack depth profile by a new crack depth profile in which any crack segment with depth $d < d_o$ is replaced by $d = 0$ (Fig. 2.48b). The choice of d_o fixes the candidate equivalent rectangular crack length (L_o).

(b) The depth of the candidate equivalent rectangular crack is determined by equating its area to the area under the crack depth profile defined in step 1 (Fig. 2.48b). For example, in Figs. 2.48 a-b, the choice of $d_o = 50\%$ fixes the length and depth of the candidate equivalent rectangular crack at 9 mm and 70%, respectively.

(c) Generate a series of candidate equivalent rectangular cracks by parametrically varying d_o and calculate the ligament rupture pressures for all the candidates (Fig 2.49).

(d) The equivalent rectangular crack corresponds to the lowest ligament rupture pressure (Figure 2.49).

This procedure has been automated by systematically choosing various candidate equivalent crack lengths L_o (instead of d_o), determining the corresponding candidate equivalent crack depths, and selecting the equivalent crack length, depth, and value of m_p that correspond to the minimum ligament rupture pressure.

2.1.3.5 Summary of Sizing Accuracy

The RMSE values from the data of Figs. 2.17 to 2.39, for various binned depth ranges, are presented in Tables 2.3 and 2.4. In Table 2.3, the depth ranges are given in terms of the metallographic depths. This is useful when assessing the capability of the multiparameter algorithm for cracks of a certain depth. In Table 2.3, the depth ranges are given in terms of the predicted depths. This is more useful when assessing the uncertainty in predicted depths. In Figure 2.50, the standard deviation in depth (in %TW) is plotted against the maximum depth. The largest uncertainty is in the 50-70%TW range. While the deviation is small for the shallow cracks, it represents a relatively large error. For example, the standard deviation for 20%TW is 12%TW.

The overall RMSE for all cracks of all depths is 15.1%, but it is somewhat misleading to look at this overall value because there is a significant variation in the RMSE with depth. The RMSE value is significantly better for the 80–100%TW bin than for the other depth bins.

In Table 2.4, two sets of RMSE values are given; one is based on the values obtained directly from the multiparameter algorithm and the other on "corrected" values obtained from the regression fit shown in Fig. 2.41. For the shallowest cracks, the "corrected" values give a significantly lower RMSE value, but when all the data are considered, the differences in the RMSE for corrected and uncorrected predictions are small. This indicates that there is little systematic bias in the predictions of the multiparameter algorithm, i.e., the errors are random.

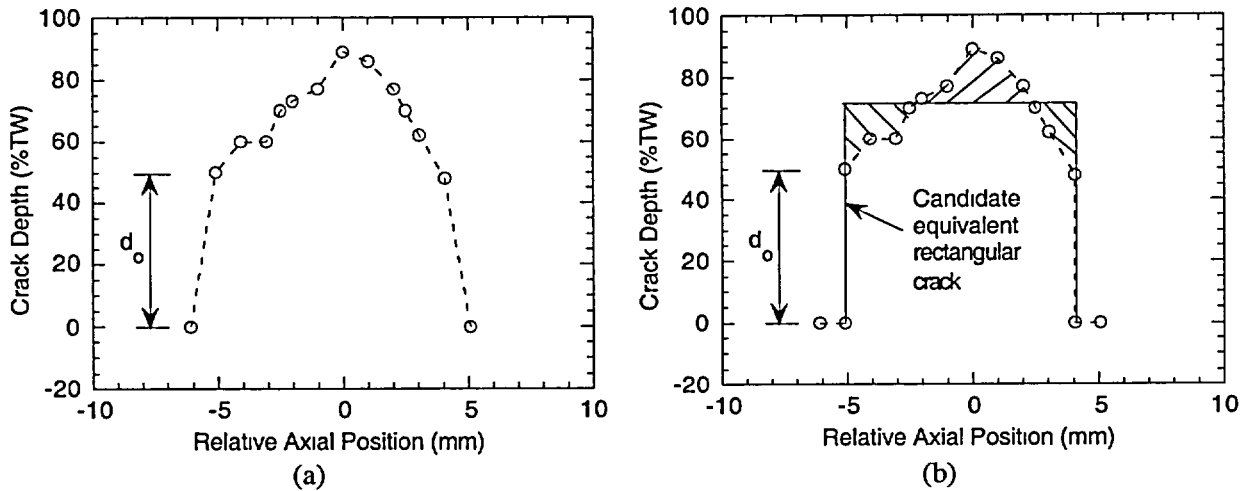


Figure 2.48 (a) Crack depth profile measured by eddy current and (b) a candidate equivalent rectangular crack corresponding to depth $d_0 = 50\%$ and $L_0 = 10$ mm.

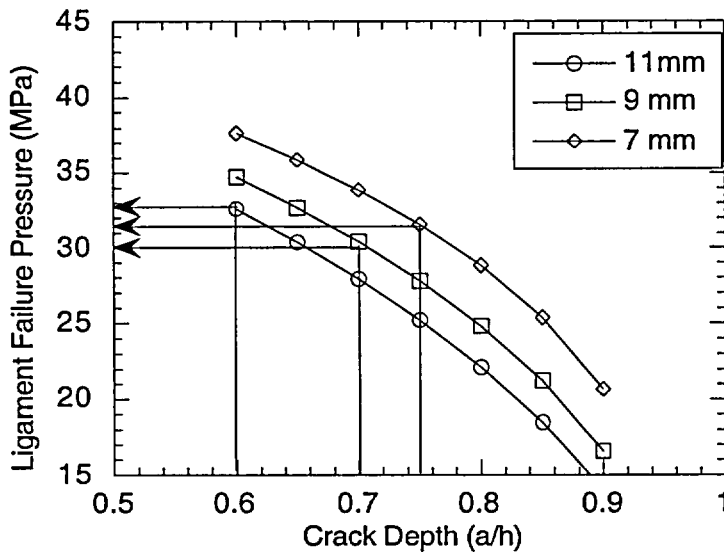


Figure 2.49 Ligament rupture pressures corresponding to three candidate equivalent rectangular cracks, 11 mm by 60%, 9 mm by 70%, and 7 mm by 75%. The equivalent rectangular crack is 9 mm by 70% because it corresponds to the lowest ligament rupture pressure (30 MPa).

The regression fit is very sensitive to the values at zero depth. However, these primarily reflect a problem of detection: the errors are not really sizing errors, but rather represent the cracks that were just not detected. Thus, direct comparison of the multiparameter and observed values may be a better measure of the sizing capability of the algorithm. This comparison is shown in Fig. 2.42, where the direct multiparameter predictions are used as the best estimate of the crack depth, and the 95% confidence bounds in the figure account for the variation of the RMSE with crack depth.

These results can be used to estimate the uncertainty in POD curves if the multiparameter algorithm is used to determine the “true” state of the mock-up for the NDE round-robin. Instead of characterizing the error in the depths in terms of the overall average for all depths ($\approx 15\%$), the error will be taken as a function of depth. Analytically, the values of RMSE given in Table 2.4 are assumed to apply at the midpoint of the depth range for each bin. The error at other depths is then estimated by linear interpolation of these values.

Table 2.3 Comparison of RMSE for depth estimates by multiparameter algorithm as a function of metallographic crack depth

Depth range (%TW)	RMSE Maximum crack depth (%TW)
0-100	13.7
30-100	9.7
50-100 (ODSCC only)	8.2

Depth range (%TW)	RMSE Crack depth (%TW)
0-100	15.5
0-20	11.9
20-40	15.9
40-60	20.5
60-80	18.7
80-100	9.8

Table 2.4 Comparison of RMSE for depth estimates by multiparameter algorithm (MV) and by regression fit in Figure 2.41 as a function of predicted crack depth

Depth range (%TW)	RMSE Crack depth MV (%TW)	RMSE Crack depth regression (%TW)
0-20	19.5	12.8
20-40	21.0	23.0
40-60	16.3	16.1
60-80	12.2	10.6
80-100	9.8	9.5

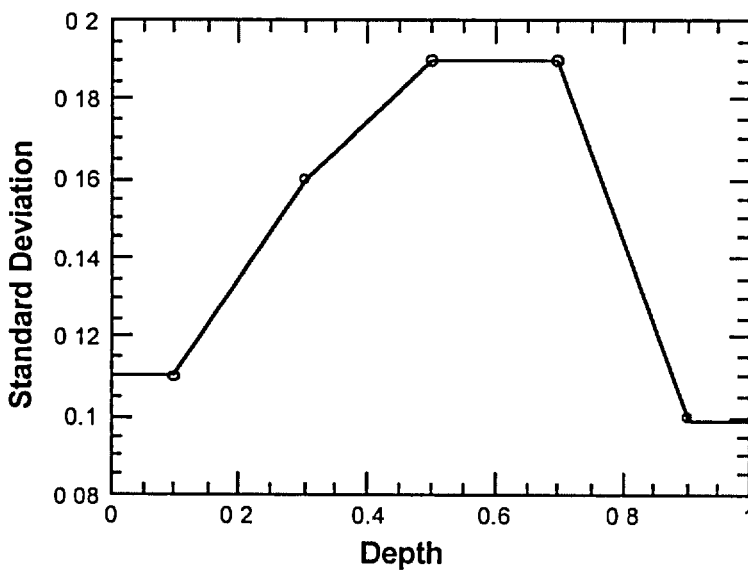


Figure 2.50 Standard deviation in percent throughwall as a function of maximum depth.

2.1.3.6 Reference State Table Summary for Mock-up

The reference state table for the mock-up provides all the relevant information for analyzing the round-robin analysts' results. Tables 2.5 and 2.6 highlight the primary information for a flaw in the table. The flaw type, BC volts, BC phase, whether ID or OD, three-letter code for the flaw, maximum depth as determined by multiparameter algorithm, flaw length, average depth, and m_p are all included in the flaw table. Not shown are flaw location in the mock-up (row, column, and level) and beginning and end points of the flaw, in BC data points. The test sections included in the table data are those for which m_p was determined. As a result, these tables present data from the flaws that have relatively large EC signals, permitting the profiling to be carried out accurately and leading to an accurate value of m_p . Table 2.5 shows the values for TSP SCC, while Table 2.6 shows the values for freespan SCC.

2.2 Design and Organization of Round-Robin

A very important aspect of developing the round-robin (RR) exercise was input from an NDE Task Group. The Task Group helped define the parameters found in a field inspection and provided input on how to ensure that the RR mimicked an in-service (ISI) inspection. Members of the Task Group are from utilities, vendors, EPRI, NRC, and ANL. The industry members are G. Henry and J. Benson (EPRI), T. Richards and R. Miranda (FTI), D. Adamonis and R. Maurer (Westinghouse), D. Mayes (Duke), S. Redner (Northern States Power), and B. Vollmer and N. Farenbaugh (Zetec).

The Task Group provided input related to the make-up of the mock-up, the quality of the data collected for the RR, the nature of the flaws, procedures for analyzing data, and documentation. The Task Group helped meet the goal of providing an RR exercise that represents, as closely as possible, a true field inspection. The Task Group provided input on the analysis guidelines, data acquisition, degradation assessment, training manual, and examination technique specification sheets (ETSSs). The RR began only after the Task Group approved the documentation used for the RR and concluded that flaws in the mock-up had EC signals similar to signals observed under field conditions. In addition, opinions were expressed on how to handle spin calls, how to handle the logistics of distributing EC data to the various teams, content of the training documentation, make-up of the analysis team, and what equivalency demonstrations needed to be carried out. As a result of the input on the analysis team, a decision was made to use a five-member team that would include a primary, a secondary, and two equally qualified resolution analysts to analyze the EC data. The fifth member, the independent qualified data analyst (QDA), should be from a utility. The primary and secondary analysts reported their observations independently of each other. The resolution analysts reviewed calls when the primary and secondary analysts' calls differed. The independent QDA monitored the effort looking for, in his opinion, excess overcalls and sampled 40 test sections to ascertain, in his opinion, if flaws were being missed.

2.2.1 The Mock-Up as ANL's Steam Generator

The mock-up was treated as a steam generator owned by a utility. The role of the utility in this case was taken by ANL. The ISI followed the process and procedures used by industry. ANL was responsible for documentation preparation, monitoring data collection, monitoring data analysis, and carrying out statistical analysis.

Table 2.5

Reference table showing data for axial SCC and EDM notches at TSP for test sections that had m_p determined.

Flaw Type	BC Volts	BC Phase		Ref State	Max Depth (%TW)	Length (mm)	Avg Depth (%TW)	Length x	
		(deg.)	ID/OD					Ave Depth (mm ²)	m_p
LIDSCC	9.97	107	ID	MAI	35.2	10.7	26.4	3.5	1.2
LODSCC	3.57	71	OD	SAI	88.8	27.1	67.6	22.9	2.6
LODSCC	8.78	70	OD	SAI	87.8	20.0	78.8	19.7	3.6
LIDSCC	2.7	24	ID	MMI	45.7	34.2	19.2	8.2	1.2
LODSCC	2.28	91	OD	SAI	84.1	7.8	62.7	6.1	1.5
LODSCC	5.56	59	OD	MAI	94.5	30.2	68.5	25.8	4.5
LODEDM	0	0	OD	SAI	24.4	9.2	16.4	1.9	1.1
LODSCC	5.18	68	OD	MAI	94.2	29.7	81.4	30.2	5.4
LODSCC	6.69	74	OD	MAI	95.2	13.6	72.1	12.2	3.4
LODEDM	4.7	36	OD	SAI	99.8	7.0	82.4	7.2	34.2
LIDSCC	2.19	187	ID	SAI	28.1	9.5	17.3	2.1	1.1
LODSCC	5.56	63	OD	MAI	93.8	21.0	69.8	18.3	3.2
LODSCC	6.49	39	OD	MAI	78.9	21.9	66.0	18.1	2.3
LODSCC	4.76	53	OD	SAI	98.7	40.7	58.1	29.5	3.3
LODSCC	0.63	46	OD	MAI	61.3	40.5	41.5	21.0	1.6
LODSCC	3.46	54	OD	MAI	95.0	32.5	72.4	29.4	5.2
LIDSCC	6.02	187	ID	SAI	29.5	12.0	25.5	3.8	1.2
LODSCC	29.07	18	OD	MAI	93.7	14.2	57.3	10.2	2.2
LODEDM	1.47	104	OD	SAI	73.5	21.6	63.9	17.3	2.2
LODSCC	2.52	134	OD	SAI	93.7	18.5	53.8	12.4	2.4
LIDSCC	0.97	32	ID	SAI	4.0	2.6	1.9	0.1	1.0
LODSCC	0.47	58	OD	MAI	66.5	35.0	31.2	13.7	1.6
LODSCC	21.42	64	OD	MAI	97.8	30.1	86.6	32.6	12.0
LODSCC	16.74	77	OD	MAI	95.6	21.6	57.5	15.5	3.7
LODSCC	1.5	131	OD	MAI	86.4	41.7	29.6	15.4	2.3
LODSCC	5.89	51	OD	SAI	93.4	15.0	68.4	12.8	2.3
LODSCC	1.41	66	OD	SAI	97.4	15.8	50.8	10.0	3.5
LODSCC	3.11	53	OD	SAI	85.0	21.1	40.0	10.5	1.8
LIDSCC	1.09	25	ID	SAI	25.5	8.0	15.5	1.5	1.1
LODSCC	0	0	OD	SAI	9.5	59.8	2.8	2.1	1.0
LIDSCC	1.41	103	ID	SAI	66.9	10.7	48.2	6.5	1.4
LODSCC	4.53	192	OD	MAI	99.4	16.8	57.5	12.1	4.8
LODEDM	3.2	89	OD	SAI	74.7	21.9	64.0	17.5	2.2
LODSCC	19.84	90	OD	MMI	97.5	283.7	80.0	283.6	7.7
LIDSCC	1.72	19	ID	SAI	25.6	10.0	19.2	2.4	1.1
LODSCC	7.2	36	OD	MAI	91.4	26.3	72.1	23.7	3.5
LODSCC	12.1	93	OD	MAI	84.0	29.5	45.6	16.8	2.0
LODSCC	2.28	142	OD	SAI	73.7	15.7	24.4	4.8	1.3
LODSCC	1.69	142	OD	MAI	44.2	11.9	30.2	4.5	1.2
LODEDM	0	0	OD	SAI	72.4	25.1	56.4	17.7	2.0

Flaw Type	BC Volts	BC Phase		Ref. State	Max Depth (%TW)	Length (mm)	Avg. Depth (%TW)	Length x	
		(deg.)	ID/OD					Call	Ave Depth (mm ²)
LIDSCC	1.17	18	ID	SAI	28.1	24.8	11.4	3.5	1.1
LODSCC	3.64	61	OD	SAI	81.9	21.1	46.5	12.3	1.8
LODSCC	0.87	152	OD	SAI	12.3	11.6	4.9	0.7	1.0
LODEDM	1.06	121	OD	SAI	86.1	24.4	70.9	21.7	2.7
LIDSCC	3.64	38	ID	MMI	51.2	54.5	18.8	12.8	1.2
LIDSCC	0.73	33	ID	SAI	22.0	14.7	10.7	2.0	1.1
LIDSCC	1.23	32	ID	MMI	23.2	57.0	9.9	7.1	1.1
LODSCC	7.75	46	OD	MAI	96.4	25.9	84.6	27.4	7.6
LIDSCC	4.98	47	ID	MAI	60.3	10.3	43.0	5.5	1.3
LIDSCC	2.48	16	ID	MMI	33.4	25.7	18.8	6.0	1.2
LODSCC	5.19	70	OD	SAI	93.0	22.2	68.3	18.9	3.1
LIDSCC	3.4	22	ID	MMI	41.7	146.8	25.3	46.5	1.5
LODSCC	1.26	127	OD	SAI	71.4	7.1	42.5	3.8	1.1
LODSCC	2.02	131	OD	SAI	75.8	26.4	38.5	12.7	1.6
LIDSCC	1.42	31	ID	MMI	64.6	41.9	20.6	10.8	1.3
LODSCC	1.06	21	OD	SAI	95.5	15.6	69.6	13.6	2.3
LODSCC	6.26	43	OD	MAI	96.0	24.2	70.7	21.3	5.5
LODSCC	2.21	140	OD	SAI	84.8	12.8	61.1	9.8	1.9
LODSCC	6.36	78	OD	MAI	93.0	22.0	67.0	18.4	3.1
LODSCC	6.69	47	OD	MAI	99.4	41.4	78.3	40.5	13.2
LODEDM	1.97	96	OD	SAI	73.6	22.1	64.3	17.8	2.2
LIDSCC	5.56	36	ID	SAI	69.7	23.0	40.5	11.7	1.6
LIDSCC	2.93	42	ID	MMI	51.0	61.5	26.1	20.0	1.6
LODSCC	7.12	65	OD	SAI	91.1	23.3	58.1	16.9	2.3
LODSCC	16.92	66	OD	MAI	90.8	73.6	23.8	21.9	2.3
LIDSCC	3.9	59	ID	MAI	82.7	17.0	66.6	14.1	2.4
LIDSCC	3.93	31	ID	MMI	42.3	38.9	14.8	7.2	1.2
LODSCC	28.13	29	OD	MAI	91.9	18.9	78.0	18.4	3.6
LODSCC	16.79	70	OD	MAI	93.7	20.5	64.9	16.6	3.5
LODSCC	5.25	58	OD	SAI	90.6	24.4	71.3	21.7	3.0
LODSCC	3.3	65	OD	MAI	94.8	36.2	50.2	22.7	4.4
LODSCC	21.84	9	OD	MAI	25.5	16.2	8.9	1.8	1.1
LODSCC	1.58	119	OD	SAI	85.6	10.8	66.4	9.0	1.9
LODSCC	3.17	187	OD	MAI	17.6	7.8	5.9	0.6	1.0

Table 2.6 Reference table showing data for axial SCC and EDM notches in the freespan for test sections that m_p had determined.

Flaw Type	B C Volts	BC Phase (deg.)	ID/OD	Ref State	Depth (%TW)	Length (mm)	Avg Depth (%TW)	Area(mm ²)	m_p
LODSCC	4.61	70	OD	SAI	91.8	12.2	77.2	11.8	2.8
LODSCC	3.38	61	OD	SAI	91.7	20.1	57.2	14.3	2.0
LODSCC	1.29	51	OD	SAI	86.4	20.5	48.6	12.5	1.9
LODSCC	3.79	186	OD	SAI	70.7	17.7	54.0	11.9	1.8
LIDEDM	5.04	30	ID	SAI	53.5	12.8	41.7	4.0	1.4
LODSCC	3.13	50	OD	SAI	87.3	17.8	67.4	15.0	2.6
LODEDM	1.84	102	OD	SAI	71.0	13.5	59.8	9.3	1.8
LODSCC	1.83	68	OD	MAI	82.4	20.9	46.0	12.0	1.7
LODEDM	0.8	120	OD	SAI	52.0	13.6	41.3	7.0	1.4
LODSCC	12.9	82	OD	MAI	95.0	16.6	73.6	15.3	6.3
LODSCC	12.9	82	OD	MAI	95.0	16.6	73.6	15.3	6.3
LODSCC	17.06	74	OD	MAI	97.4	13.1	86.9	14.3	5.0
LODSCC	8.03	84	OD	MAI	94.7	25.7	80.5	25.9	5.3
LODSCC	7.6	48	OD	MAI	94.3	23.9	81.4	24.3	5.3
LODSCC	6.68	68	OD	MAI	91.1	17.8	72.4	16.1	3.1
LIDEDM	5.7	34	ID	SAI	66.1	13.9	55.2	9.6	1.6
LODSCC	4.12	57	OD	MAI	88.8	10.5	73.7	8.8	2.4
LODSCC	0.8	141	OD	SAI	77.4	19.7	19.7	10.6	1.8
LODSCC	1.81	74	OD	SAI	92.8	12.0	76.2	11.4	2.5
LODSCC	0.59	133	OD	MAI	70.2	13.6	49.6	8.5	1.6
LIDEDM	2.22	25	ID	SAI	41.7	12.8	28.1	4.5	1.2
LIDSCC	3.47	8	ID	MAI	55.6	14.1	33.5	4.5	1.3
LODSCC	8.06	95	OD	MAI	93.7	26.5	61.6	20.4	2.7
LODSCC	2.44	79	OD	MAI	93.9	21.8	71.0	19.3	3.3
LODSCC	4.95	75	OD	MAI	92.1	13.1	69.8	8.1	1.9
LODSCC	12.19	60	OD	MAI	98.5	24.0	80.6	24.2	8.7
LODSCC	0	0	OD	SAI	30.6	12.4	13.7	2.1	1.1
LODSCC	1.37	95	OD	MAI	88.0	14.9	61.5	11.5	2.0
LODSCC	2.74	124	OD	MAI	56.7	7.5	39.3	3.7	1.2
LODSCC	2.56	137	OD	SAI	26.1	13.3	11.7	1.9	1.1
LODSCC	2.12	107	OD	MAI	78.7	16.8	63.9	13.4	2.1
LODSCC	5.5	53	OD	MAI	90.6	25.3	67.4	21.3	3.7
LODSCC	1.12	113	OD	SAI	83.5	25.2	32.9	10.4	1.8
LODSCC	6.62	78	OD	SAI	96.3	29.1	85.0	31.0	9.3
LODSCC	2.46	107	OD	SAI	80.2	11.4	64.6	9.2	1.8
LODSCC	4.74	50	OD	MAI	98.5	22.1	76.1	21.0	4.1
LODSCC	3.4	89	OD	MAI	97.2	23.6	50.0	14.7	3.2
LODSCC	2.92	73	OD	MAI	90.5	13.9	64.4	11.2	2.1
LODSCC	6.12	81	OD	MAI	87.8	20.9	57.8	15.1	2.5
LODSCC	7	65	OD	MAI	99.2	37.4	42.0	19.7	7.5
LODSCC	4.28	70	OD	SAI	91.8	28.6	39.7	14.2	2.4
LIDSCC	0.68	110	ID	SAI	64.1	20.3	48.8	12.4	1.7

Flaw Type	B C Volts	BC Phase (deg)	ID/OD	Ref State	Depth (%TW)	Length (mm)	Avg Depth (%TW)	Area(mm ²)	m _p
LODSCC	0.57	45	OD	SAI	65.5	30.3	28.3	10.7	1.4
LIDSCC	5.27	37	ID	SAI	68.1	26.1	54.1	17.7	2.0
LODSCC	1.68	76	OD	SAI	80.0	25.3	39.8	12.6	1.7
LODSCC	0.36	144	OD	MAI	96.1	24.8	64.4	20.0	3.2
LODSCC	6.15	68	OD	MAI	96.1	24.8	64.4	20.0	3.2
LODSCC	1.01	81	OD	MAI	80.4	28.1	48.0	16.9	2.2
LODSCC	1.37	148	OD	SAI	58.3	12.4	27.4	4.3	1.2
LODSCC	6.77	129	OD	MAI	90.4	28.7	66.0	23.7	3.1
LODSCC	8.81	169	OD	SAI	78.2	17.8	55.5	11.5	1.9
LODSCC	5.76	72	OD	SAI	94.1	18.6	68.2	15.9	3.3
LIDEDM	5.99	39	ID	SAI	67.3	25.8	55.8	18.0	2.0

2.2.1.1 Responsibilities

2.2.1.1.1 Data Collection

Data were collected by a qualified (according to EPRI guidelines) team from Zetec in June and again in August 1999. A qualified observer from Westinghouse was also present. The data acquisition team included a qualified data analyst (QDA) Level II and a QDA Level IIIa.

2.2.1.1.2 NDE Task Group

The NDE Task Group provided input during the development of the documentation. They provided input on data collection, how to carry out the Degradation Assessment, how to select the Examination Technique Specification Sheets (ETSS), how to carry out the site-specific examinations, and how to prepare the training manual. The role of the Task Group, in general, was to help ANL mimic a field inspection.

2.2.1.1.3 Analysis of Round-Robin

Analysts' RR reports on optical disks were collected from RR teams by ANL proctors and converted to Excel files so they could be analyzed in a convenient manner. Proctors (ANL staff) were present during all analysts' activities to ensure that procedures developed for the analysis of data were followed correctly.

2.2.1.1.4 Statistical Analysis

Data were analyzed at ANL. Logistical fits to data for POD as a function of crack depth and m_p with confidence limits that include errors in reference state were developed. Assistance from P. Heasler and R. Kurtz of PNNL was provided to ensure that the statistical analysis was carried out correctly. Decisions regarding the grading unit for the statistical analysis were arrived at through discussions with P. Heasler.

2.2.1.1.5 Documentation

The documentation prepared included the degradation assessment, the appropriated Examination Technique Specification Sheets (ETSS), data collection procedures, analysis guidelines, and the training

manual. Detailed documentation was prepared on how the RR exercise was carried out, the sequence of events, and the role of the ANL proctors, including administration of site-specific exams.

2.2.2 Round-Robin Documentation

Four documents were prepared for conduct of the mock-up testing and for the RR data analysis. They are ANL001 Rev. 2 "Argonne Analysis Guideline," ANL002 Rev. 3 "Multifrequency EC Examination of Tubing within the ANL SG Mock-up," ANL003 Rev. 3 "SG Mock-up Tubing Degradation Assessment and Technique Qualification," and ANL004 Rev. 3 "Training Manual." These documents are discussed below.

2.2.2.1 Degradation Assessment (ANL003 Rev. 3)

A Steam Generator Tube Degradation Assessment for flaws was prepared, per the requirements specified in NEI-97-06 and Revision 5 of the EPRI PWR Steam Generator Examination Guidelines. In accordance with Rev. 5 of the EPRI PWR Steam Generator Examination Guidelines, a review of EPRI-qualified techniques was performed to ensure that application of these techniques was pertinent to site-specific conditions of the mock-up.

This document identified the degradation mechanisms in the tubing of the steam generator mock-up. This assessment also identified the inspection methods to be used to ensure that the inspection techniques and personnel used for the detection and sizing of tube flaws is appropriate for all degradation mechanisms. The training document for the RR addressed the handling of anomalous signals.

The degradation assessment reviewed all types of degradation in the mock-up, including the following:

- (a) Intergranular attack (IGA) characterized by a uniform or relatively uniform attack of the grain boundaries over the surface of the tubing. When the occurrence is over a relatively large extent exhibiting three-dimensional features, the IGA is referred to as volumetric IGA. IGA is associated with the outside diameter of the tubing material. The IGA present in the mock-up is not mixed with SCC, a combination that can be found in the field and is easier to detect than pure IGA. However, the IGA in the mock-up is similar to that found in several operating plants. The mock-up IGA is representative of IGA at Cook, Point Beach, and San Onofre, simulating IGA found in the tube sheet crevice.
- (b) Primary water stress corrosion cracking (PWSCC), defined as cracking that occurs on the tube's primary side (the inside diameter) when a source of stress is present in susceptible material. Locations of PWSCC in the mock-up include expansion transitions and dents.
- (c) Wear, the volumetric removal of material caused by the mechanical action of one material in contact with another.
- (d) Corrosive fatigue, which is a result of alternating stress cycles produced by tube vibration that may be accelerated by a corrosion process occurring during stress cycling. A few fatigue cracks can be found in the mock-up.
- (e) Wastage that is corrosive wear to the outer wall of the tubing.
- (f) Stress corrosion cracking initiating at the outer diameter (ODSCC) of Alloy 600 steam generator tubes is present at the TSP, in the freespan and in the tubesheet. ODSCC refers to a range of stress

corrosion cracking morphologies observed to occur along the OD of Alloy 600 steam generator tubing. Inspection requirements for this damage mechanism include 100% of the tube sheet transitions in Level A of the mock-up.

2.2.2.2 Data Acquisition Documentation (ANL002 Rev. 3)

The document "Multifrequency EC Examination of Tubing within the ANL SG Mock-up" provides all information necessary to collect the RR data. The procedures mimic those of an actual ISI. The basis of the data acquisition is the Examination Technique Specification Sheet (ETSS). The document defines the frequencies, axial and rotational speeds, and calibration procedures. Two ETSSs were developed for the ANL mock-up. These ETSSs are the result of reviewing EPRI ETSSs for the various degradation mechanisms in the mock-up and combining them into the two used.

One hundred percent of the tubes were inspected full-length with a bobbin coil. EPRI site-qualified technique ETSS 96008, covered by ANL's ETSS#1 (described later), was used. This technique has an EPRI-reported probability of detection of 85% at >40% TW at a confidence level of 90% in those areas not associated with the roll transition.

In addition, 100% of the tubes were inspected with a three-coil MRPC probe (Plus-Point™, standard pancake and shielded high-frequency coil) at the top of tube sheet region. EPRI site-qualified technique ETSS 96403, covered by ANL's ETSS#2 (described later), was used for the detection of tube sheet flaws. This technique has an EPRI-reported probability of detection of 81% @ >50% TW at a 90% confidence level for both axial and circumferential indications.

Bobbin coil indications at TSPs were investigated with a rotating coil (Plus-Point™). The site-qualified bobbin technique for nondented TSPs is EPRI ETSS 96007, covered by mock-up ETSS#1. The EPRI-reported probability of detection is 89% @ >60% TW at a 90% level of confidence. For all rotating coil inspections, site-qualified technique EPRI ETSS 96403, covered by mock-up ETSS#2, was used. This technique has an EPRI-reported probability of detection of 81% @ > 50% TW at a 90% confidence level for axial and circumferential indications.

The tubing in the mock-up steam generator was mechanically-expanded (rolled) in the shop. The transition zone is the region of the tube where the tube transitions from the expanded tube diameter to the nominal tube. Axial and circumferential indications are found in this region. A 100% rotating coil examination of top of the tube sheet was performed to detect PWSCC. EPRI site-qualified technique ETSS 96508, covered by mock-up ETSS#2, was used for detection of this degradation mechanism. This technique has an EPRI-reported probability of detection of 84% @ > 50% TW @ 90% confidence level for both axial and circumferential indications.

Corrosion of the TSPs causes the tubing to become dented, resulting in high localized stresses that lead to stress corrosion cracking. EPRI site-qualified Technique ETSS 96012 (covered by mock-up ETSS#1) was used for bobbin detection of axial PWSCC at TSP intersections (dent <2V). This technique has an EPRI-reported probability of detection of 89% @ >34% TW at a confidence level of 90%.

Site-qualified technique EPRI ETSS 96508 (covered by mock-up ETSS#2) was used for rotating coil detection of axial and circumferential PWSCC at dented locations and has an EPRI-reported probability of detection of 84% @ >50% TW at a confidence level of 90%.

Degradation due to wear is adequately identified by a bobbin coil examination. The technique used for detection of tube wear was EPRI ETSS 96004 (covered by mock-up ETSS#1) with an EPRI-reported probability of detection of 82% for >50% TW and a 90% confidence level.

No special examination requirements are listed in the EPRI PWR Steam Generator Examination Guidelines for fatigue degradation due to rapid growth rates.

Note that the EPRI-reported PODs may be determined from small sample sets, with the lower confidence limit the stated POD. As an example, if all cracks in a set of 11 test sections were detected (100% detection), the lower 90% confidence limit is 82% and the stated POD would be 0.82. EPRI-stated PODs are adjusted to sample size.

2.2.2.3 ANL Analysis Guideline (ANL001 Rev. 3)

This procedure provided the technical direction for the performance of EC examinations of the ANL SG mock-up. This procedure was applicable to all examination personnel and generally mimics industry ISI guidelines. Flaws were located by data point. Percent throughwall was entered into the PERCENT column, with the exception of dents and dings. The three-letter analysis codes were entered into the UTIL1 column of the appropriate "Cal" record. Data were reviewed for the presence of undesirable noise with the following criteria: (a) Undesirable system noise was determined by identifying electrical interference or spiking associated with faulty probes, cabling and equipment. Studies have shown probe wear can generate undesirable horizontal noise resulting in poor signal-to-noise ratios. (b) Undesirable tube noise was determined by identifying signals caused by excessive permeability, pilgering, chatter, variations in tube geometry, tube cleanliness, and secondary-side sludge and deposits. These conditions were reported by the analyst so that a review could be performed to disposition these locations.

The primary and secondary analysts generated data used in the final analyst report and were responsible for reporting all indications. The resolution team (consisting of two resolution analysts and an independent QDA) performed the task of comparing and resolving discrepancies between the primary and secondary analyses. All identified differences in data interpretation were reviewed by resolution analysts to arrive at the final interpretation. The following procedures were used:

- (a) If the primary and secondary analysts agreed that an indication is a flaw, it was reviewed by two resolution analysts. The independent QDA has the final say if there is no consensus on the call.
- (b) If the primary and secondary analysts both give the "no detectable degradation" (NDD) call for a test section, there was no further analysis.
- (c) If the primary and secondary analysts disagreed, the disagreement was resolved by the two resolution analysts. If the resolution analysts were not in agreement, the independent QDA made the final call.

Table 2.7 shows how the data from the analysts were recorded. The row and column of the test section was entered along with the voltage, phase angle, %TW, location by data point, three-letter code, and whether ID or OD.

Table 2.7 Example format for entering data

SG	ROW	COL	VOLTS	DEG	%TW	CH	LOC (Data Point)	UTIL 1	UTIL 2
11	F	19	4.23	174	0	P1	+2383	DNT	OD
11	B	20	3.67	110	50	P 1	+2578	DSI	OD
11	B	15	1.31	13	33	P 1	+3789	NQI	ID
11	C	14	0.32	109	52	P 1	+3299	NQI	OD
11	D	3	3.1	180	0	P 1	+2678	DNT	
11	E	8	1.51	125	30	P 1	+2276	NQI	OD
11	F	6	2.36	88	68	6	+6578	ADI	OD
11	E	7	2.98	181	0	P 1	+2386	DNG	
11	G	13	4.56	125	30	P 1	+2768	DTI	OD
11	E	8	2.61	89	66	6	+3287	VOL	OD
11	A	15	1.76	76	80	P2	+2367	SCI	ID
11	I	17	2.67	89	66	6	+987	SAI	OD
11	G	11	4.7	105	50	6/P	+1224	MVI	OD
11	A	5	3.8	98	40	P2	+3398	MCI	OD
11	D	3	1.6	15	40	P1	+2688	DNI	ID
11	B	22	3.45	76	80	6	+3267	MAI	OD

2.2.2.4 Training Manual (ANL004 Rev. 3)

A training manual was developed for review by all analysts before the RR exercise was carried out. The manual provided information on the mock-up design, including a schematic diagram, type of artifacts present, a discussion regarding the presence of the circumferential markers, discussion of how the data for the RR were acquired, and a table showing format for entering data. Examples of mock-up bobbin coil data (Eddyner 98 line traces and Lissajous figures), followed by MRPC data (isometric plots) for the various types of flaws present, were provided. The examples included LODSCC and CODSCC at top of the tube sheet (TTS) with and without sludge, LODSCC at TSP and at a freespan location, CODSCC at a freespan location, PWSCC at dented TSP and at top of the tube sheet with and without sludge, freespan ding with and without an LIDSCC, fatigue crack, and degradation resulting from IGA.

2.2.2.5 Examination Technique Specification Sheet (ETSS)

Before development of the mock-up ETSSs a review of the essential variables for all EPRI-qualified techniques was performed. This ensured that the applications of the EPRI techniques are pertinent to site-specific mock-up steam generator conditions.

The EPRI Appendix H EC techniques used during the examination of the steam generator mock-up were reviewed to determine their applicability to the site-specific mock-up conditions. An investigation of the tube bundle degradation was performed to support the Appendix H technique qualifications.

There are three classifications of EC techniques available: "site-qualified," "qualified," and "nonqualified."

"Site-qualified techniques" have an EPRI Examination Technique Specification Sheet (ETSS) for detection and/or sizing. The ETSSs have been reviewed for similarity and applicability to the mock-up conditions. For degradation previously "detected" in the mock-up, EC signals have been compared to the EPRI signals to classify the technique as site-qualified. Damage mechanisms in the mock-up have site-qualified techniques for detection.

2.2.3 Acquisition of Eddy Current Mock-Up Data and Description of Data Acquisition Documentation

The qualified Level II Operator was responsible for acquiring examination data and for the quality of that data. This Operator reviewed all calibrations performed, for acceptance. The Level III Examiner was responsible for all aspects of the examination task, to include establishing the essential variables for the examination, approving the procedures to be used and making changes when required, recommending the appropriate examination technique(s) to be used, providing judgment on data quality issues, resolving analysis discrepancies, and evaluating data.

The equipment used for data acquisition was the Zetec MIZ-30(A) Digital Multi-frequency Eddy Current Instrument used with Zetec Eddynet Software for data acquisition and analysis. The electronic instrumentation of the EC system was certified. A Hewlett Packard computer, compatibly configured to operate the EC instrument and associated controllers and fixtures, was used for data acquisition.

Removable-media data storage devices, such as optical disk drives and disks, of a type compatible with the EC system and operating software were used.

The EC probes were specified on the appropriate technique sheets. For each examination, the manufacturer, description or part number, type, size and length of probe used were provided on the summary form recorded with each calibration group.

The calibration tube standards were manufactured from a length of tubing of the same nominal size and material type as that of the tubing examined. The tubing size and material type are listed on each technique sheet.

The inside surfaces of all tubes to be examined were as clean as practical and free of obstructions or other extraneous matter. For bobbin probe examination, the scan included the full length of each tube scheduled for examination, unless specified differently in the inspection plan. For rotating-probe examination, the scan was as specified in the inspection plan bobbin coil examination data was acquired during probe retraction (pull). The scan direction for rotating examination may be during probe insertion or retraction (push or pull).

During June and August of 1999, a qualified three-man team from Zetec collected data from the mock-up (Fig. 2.51); an observer from Westinghouse was also present. The data acquisition team included a QDA Level IIa and a QDA Level IIIa. Data were acquired with a 10-D pusher-puller, MIZ30 with 36-pin cables, and Eddynet software. BC data from a mag-biased probe was collected from all 3600 test sections of the mock-up. The BC data were calibrated before and after the 4-h interval required to collect the data. No change in voltage from the standard was detectable during this time period. A

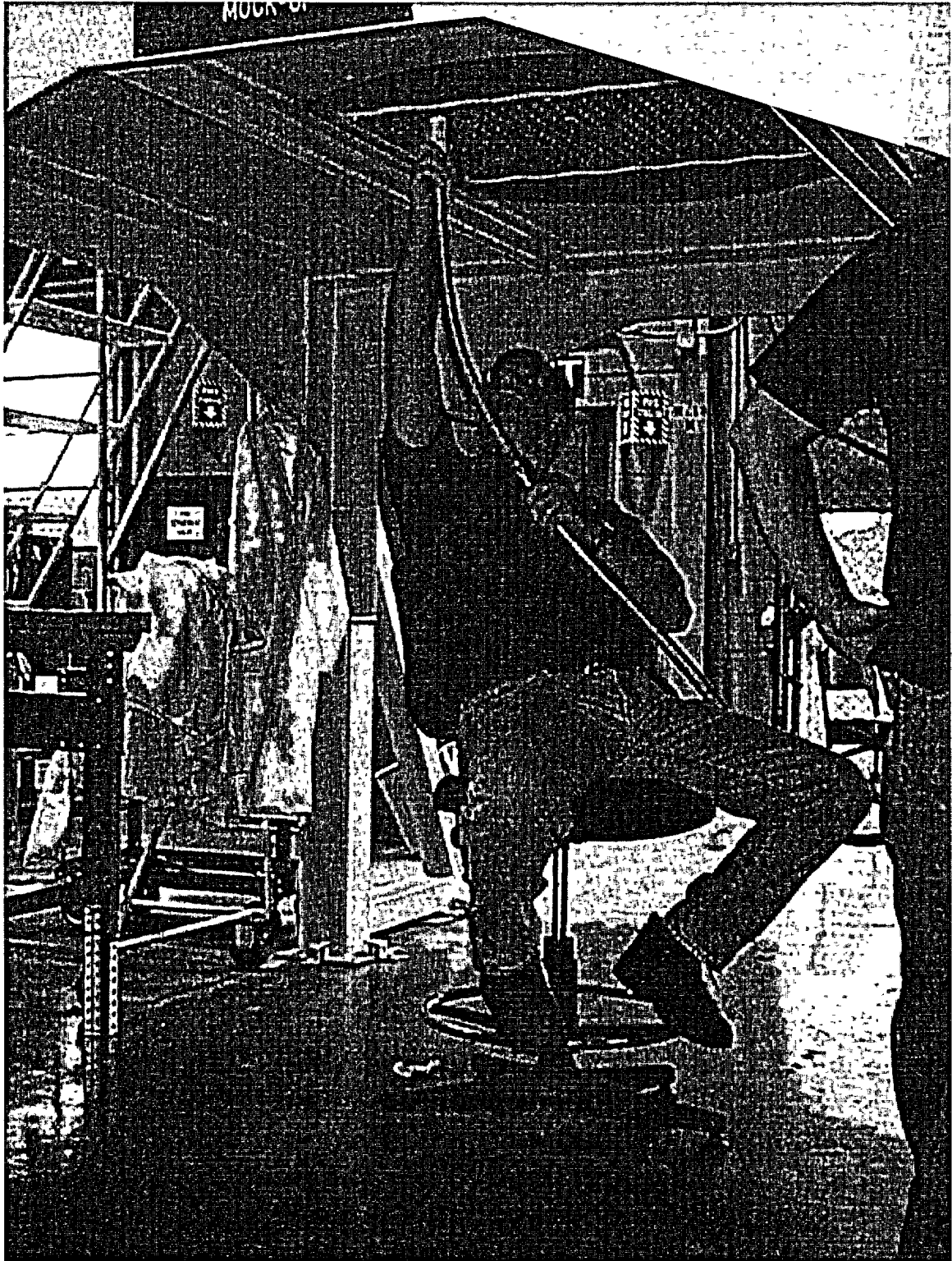


Figure 2.51 Photograph of underside of tube bundle. Conduit carrying the EC probe is shown being positioned under a tube.

magnetically biased rotating three-coil probe that includes a +Point, 2.9-mm (0.115-in.)-diameter pancake and high-frequency shielded coil was used to collect data from all 400 tube sheet test sections and all special-interest (spin call) test sections. A comparison of magnetically biased and unbiased coils shows that the biasing eliminates the voltage shift and noise in the +Point EC signal resulting from tube sensitization.

The BC data were taken at 21 in./s, maintaining a digitization rate of 37 samples per inch. Bobbin coil data were taken at 400, 200, 100, and 20 kHz (differential and absolute). MRPC data was taken from all degraded test sections in addition to hundreds of clean test sections and test sections with artifacts. An ASME standard and a standard with 18 ID and OD axial and circumferential EDM notches (20, 40, 60, 80, and 100% throughwall) were used for calibration. MRPC data were taken at 900 rpm and an axial speed of 0.5 in./s (12.7 mm/s) to maintain a digitization rate of 30 samples per inch (12 samples/cm) in the circumferential direction and 30 in the axial direction. Data were taken at 600, 400, 300, 200, and 100 kHz. A total of nine +Point probes were used during this exercise because of probe wear. MRPC probes were replaced when one of the channels could not be nulled. This inability to null appears on the computer screen as an alert "flag."

All data were recorded on 2.6-GB magneto-optical disks. Two copies of the master disk were made, and all the data were copied to an ANL archive computer backup system. The setup for the bobbin coil and +Point probe matches or exceeds the specifications of the examination technique specification sheets (ETSSs) qualified for the flaws in the tube bundle.

The mock-up data collected by Zetec were analyzed at ANL (by ANL personnel) with EddyNet98 software. The locations of the flaw signals were checked against the location data of the flaw map. Locations of possible dings due to assembly that could lead to significant EC signals were noted. These dings could be created if a test section were inadvertently pressed against the simulated TSP during assembly.

During summer 1999, a recognized industry expert reviewed the ANL steam generator mock-up bobbin coil data and some of the MRPC data acquired by Zetec. The overall quality of the data was judged to be good, generally representative of field data and meeting or exceeding requirements for qualified techniques. For IGA, the examples in the mock-up are pure IGA, and not mixed with other cracks. The mock-up IGA is representative of IGA at Cook, Point Beach, and San Onofre, simulating IGA found in the tube sheet crevice. As a result of this data review, important knowledge on how to prepare the site-training document was acquired.

2.2.4 Examination Technique Specification Sheets

The Examination Technique Specification Sheets (ETSSs) developed for the RR are shown below. There are two ETSSs, one for the bobbin coil and one for the three-coil MRPC, which includes a mid-range +Point coil. The ETSSs provide the parameters for collecting and analyzing the RR data.

2.2.5 Participating Companies and Organization of Team Members

Companies participating in the RR provided a list of analysts who would be available to participate. For those companies who supplied more names than would be needed, ANL selected the team members by random picks from the list provided. The team members were expected to be available during the entire exercise, generally seven to eight working days. Analysts were generally QDA Level II-a or III.

Examination Technique Specification Sheet for Bobbin Coil

ETSS #1 BOBBIN PROBE ACQUISITION				Revision 6	
Site: Argonne SG Mock-up			Page 1 of 5		
Examination Scope					
Applicability. Standard ASME Code examination for tubing Detection of IGA/ODSCC in freespan with and without sludge, at non-dented drilled TSP's, and above the TS sludge pile region, Detection of axial PWSCC at dented drilled tube support plate intersections, wastage and wear. This technique meets the requirements of App. H ETSSs 96001, 96004 (except sizing), 96007 and 96008 and 96012.					
Instrument			Tubing		
Manufacturer/Model: Zetec MIZ-30, Tecrad TC6700			Material Type: Inconel 600		
Data Recording Equipment			OD X Wall (inch): 0.875 X 0.050		
Manuf./Media: HP Hard Drive, 2.6 Gb Optical or Equiv.			Calibration Standard		
Software			Type: ASME Rev. 5 requirements		
Manufacturer: Zetec or Westinghouse latest approved version			Analog Signal Path		
			Probe Extension Manuf.: Zetec		
Examination Procedure			Extension Type & Length. Universal 940-1760, 50 ft		
Number/Revision: ANL002/Rev. 3			Slip Ring Model Number: 508-2052 or equivalent		
Scan Parameters					
Scan Direction: Pull					
Digitization Rate, Samples Per Inch (minimum):		Axial Direction	37	Circ. Direction	N/A
Nominal Probe Speed	Sample Rate	RPM Set	RPM Recommended Min	RPM Recommended	
21"/sec.	800	N/A	N/A	N/A	
Probe/Motor Unit					
Description (Model/Diameter/Coil Dimensions)			Manufacturer/Part Number		Length
A-720-M/UJC (720UL)			Zetec 760-1192-000		110 ft
Data Acquisition					
Calibration Coil 1 Channels					
Frequency Channel	400 kHz Ch.1	200 kHz Ch. 3	100 kHz Ch. 5	20 kHz Ch. 7	
Phase Rotation	100% TWH 40 degrees	100% TWH 40 degrees	100% TWH 40 degrees	TSP 270 Degrees	
Span Setting	100% TWH 5 divisions	100% TWH 5 divisions	100% TWH 5 divisions	TSP 5 divisions	
Calibration Coil 5 Channels					
Frequency Channel	400 kHz Ch. 2	200 kHz Ch. 4	100 kHz Ch. 6	20 kHz Ch. 8	
Phase Rotation	100% TWH 40 degrees	100% TWH 40 degrees	100% TWH 40 degrees	TSP 270 Degrees	
Span Setting	100% TWH 3 divisions	100% TWH 3 divisions	100% TWH 3 divisions	TSP 5 divisions	

ETSS#1 BOBBIN PROBE ACQUISITION										Revision 6		
Site:Argonne SG Mock-up										Page 2 of 5		
Configuration Board Settings												
trig: off		down		configuration# 0			name Bobbin			samples/sec see pg1		rec.medra = HD
tester=		board#1		board#2			board#3			board#4		board#5
#of channels= 8		probe#1		probe#1			probe#2			probe#2		probe#1
		DRIVE		DRIVE			DRIVE			DRIVE		DRIVE
		A D B C		A D B C			A D B C			A D B C		A D B C
Drive Polarity		N N										
Group Number		1 1										
Coil Number		1 5										
freq#1	Time slot #1											
400kHz	G:x2	12 0V	D A									
freq#2	Time slot#2											
200kHz	G.x2	12 0V	D A									
freq#3	Time slot#3											
100kHz	G x2	12 0V	D A									
freq#4	Time slot#4											
20kHz	G x2	12 0V	D A									
freq#5	Time slot#5											
End loc ch	1	1	driveA: D=A1-A2, P=dr A1 pu A2, DP= dr: D1&D2 pu A1&A2									
Threshold	off	off	driveB D=B1-B2, A=A1-A2									
(P) Gain	x6		P=dr B1 pu B2, DP = dr C1&C2 pu B1&B2									
Active Probes		1	drive C D=C1- C2, A=D1-C2									
	(see note 1)		drive D D= D1-D2									
Special Instructions												
<ol style="list-style-type: none"> 1. The 720MULC probe is the primary use probe for the bobbin examination 2. Examine each tube full length or to the extent possible. 3. Three recordings of the calibration standard should be performed at the beginning and end of each calibration group or every four hours, whichever comes first. 4. Periodically monitor all channels for data quality and acceptability. 												

Examination Technique Specification Sheet

ETSS#1- BOBBIN PROBE ANALYSIS

Revision 6

Page: 3 of 5

Data Analysis

Calibration Differential Channels

Channels & Frequency	Ch 1 400 kHz	Ch 3 200 kHz	Ch 5 100 kHz	Ch 7 20 kHz
Phase Rotation	100% TWH 40±1°	100% TWH 40±1°	100% TWH 40±1°	TSP 270±3°
Span Setting Minimum	4x20FBH @ 4 Div	4x20FBH @ 4 Div	4x20FBH @ 4 Div	TSP 5 divisions

Calibration Absolute Channels

Channel & Frequency	Ch 2 400 kHz	Ch 4 200 kHz	Ch 6 100 kHz	Ch 8 20 kHz
Phase Rotation	Probe Motion Horiz. Flaws Up	Probe Motion Horiz Flaws Up	Probe Motion Horiz. Flaws Up	TSP 270±3°
Span Setting Minimum	100% TWH 2 divisions	100% TWH 2 divisions	100% TWH 2 divisions	TSP 5 divisions

Calibration Process and Other Channels

Channels & Frequency	P1(Ch 1/5) 400/100 kHz Diff	P2(Ch 2/6) 400/100 kHz ABS	P3(Ch 3/1/5) 200/400/100 kHz Diff	
Configure & Adjust Parameters	Suppress Drilled TSP	Suppress Drilled TSP	Save 100,60,20 Suppress Drilled TSP, Expansion	
Phase Rotation	100% TWH ~35°, noise horiz	100% TWH ~35°, noise horiz.	100% TWH @40±3°	
Span Setting Minimum	4x20 FBH @ 4 divisions	100% TWH 2 divisions	100% TWH 5 divisions	

Voltage Normalization

Calibration Curves

CH	Signal	Set	Normalize	Type	CH	Set Points
1	4X20% FBH	4.0 volts	All	Phase Curve	1,3,5,P1 Max Rate 2,4,6,P2 Vpp	100,60,20,FBH (use as-built dims)

Data Screening

Left Strip Chart	Right Strip Chart	Lissajous
P1	Ch 6	P1

Reporting Requirements

Condition/Region	Report	Ch	Comment
Freespan	NQI	P1	All indications
Absolute Drift	ADI	6	Gradual indications that lack a differential response
Drilled TSP	DSI	P1	All indications within TSP
Tubesheet Interface	DTI	P1	Distorted Top of Tubesheet
Dent(Structure)	DNT	P1(Vpp)	Report all Dents > 2.0 volts at TSP's or TS interface
Ding(Freespan)	DNG	P1(Vpp)	Report all Dings in freespan > 2.00 volts
Dent/Ding with ind	DNI	P1	Distorted dent/ding with possib indication of degrad
ID Chatter or Pilger.	IDC	P1	Any indication which you believe could mask an indic.
Permeability Variat	PVN	P1	Any indication which you believe could mask an indic.

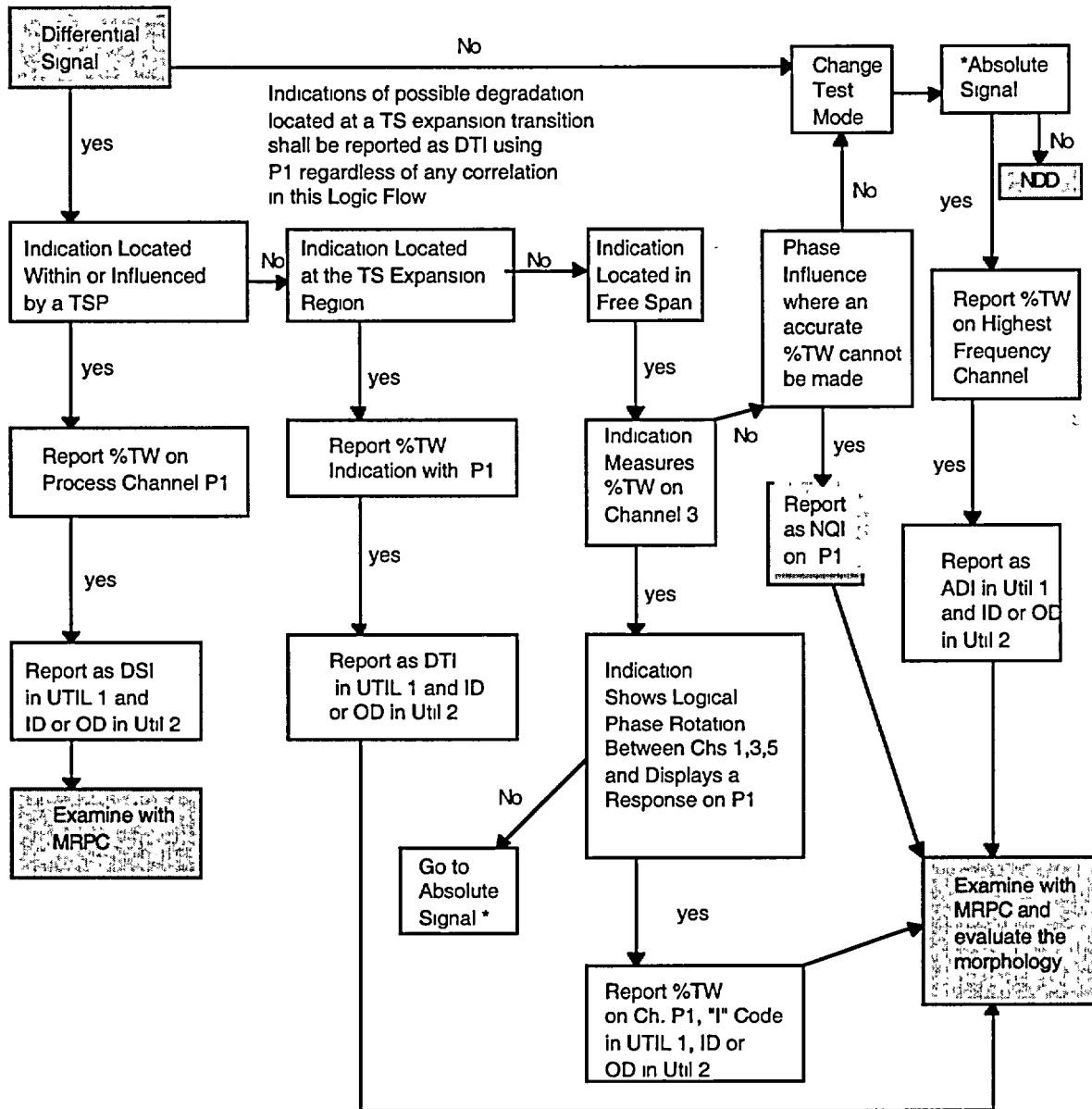
Examination Technique Specification Sheet

ETSS# 1- Bobbin Probe Analysis Revision 6 Page 4 of 5

Special Instructions

1. Provide a best estimate of %TW on all bobbin indications based on ASME calibration curve. Place appropriate "I-Code" in the Utility 1 field. Place flaw origin in Util 2 (ID or OD).
2. Zoom the strip charts to 3 (or equivalent setting based on window size) for increased visibility of small amplitude indications.
3. Scroll each freespan region with channel 3.
4. Scroll each top of tubesheet region and expansion transition with channel P1 and P3.
5. Review each drilled TSP with channel P1 and Channel 3.
6. Monitor the 100 kHz absolute strip chart for positive drift.
7. Refer to the flow chart on the following page for additional information on evaluation of indications.
8. When distorted indications within dents or dings are identified, record the dent voltage as well as the indication.
9. All data should be analyzed unless voided by the operator. There are no retest codes necessary for the mock-up. Use BDA for bad data.
10. Landmarking is not necessary. All elevations will be recorded by data point.
11. Graphics are not required.
12. Do not report signals within one inch of test section ends.

Bobbin Probe Flow Chart



Examination Technique Specification Sheet for MRPC

ETSS #2 3-Coil RPC (115/+PT/080 HF) ACQUISITION				Revision 6		
Site Argonne SG Mock-up			Page 1 of 7			
Examination Scope						
Applicability: Detection of PWSCC at TS Expansion Transitions and TSPs or Freespan Regions with or without dents Detection of ODSCC at or above TS Expansion Transitions and TSPs with or without dents Sizing of crack-like indications as applicable Satisfies requirements of ETSSs, 96403, 96508, 96702, 96703						
Instrument		Tubing				
Manufacturer/Model Zetec MIZ-30, Tecrad TC6700		Material Type Inconel 600				
Data Recording Equipment		OD X Wall (inch): 0 875 X 0 050				
Manuf /Media HP Hard Drive, 2.6 Gb Optical or Equiv.		Calibration Standard				
Software		Type EDM notches meeting Rev. 5 requirements				
Manufacturer. Zetec or Westinghouse latest approved version		Analog Signal Path				
		Probe Extension Manuf.: Zetec				
Examination Procedure		Extension Type & Length Universal 940-1760, 50 ft				
Number/Revision. ANL002/Rev. 3		Slip Ring Model Number: 508-2052 or equivalent				
Scan Parameters						
Scan Direction Pull or Push						
Digitization Rate, Samples Per Inch (minimum)			Axial Direction	30	Circ Direction 30	
Probe Speed	Sample Rate	RPM Set		RPM Min		RPM Max
0 5"/sec.	1391	900		750		1012
Probe/Motor Unit						
Description (Mode/Diameter/Coil Dimensions)			Manufacturer/Part Number		Length	
0 720(775) 3-C 115/+PT/080 HF (shielded), Mag-Bias			Zetec C700-4055-071			
.610(5-2)M/U-36 pin			Zetec 810-4077-001		83 ft	
Data Acquisition						
Calibration Coil 1 (115" Pancake) Channels						
Frequency Channel	400 kHz Ch 2	300 kHz Ch 5		200 kHz Ch 8	100 kHz Ch. 10	
Phase Rotation	40% ID Axial 15 degrees	40% ID Axial 15 degrees		40% ID Axial 15 degrees	TSP 90 Degrees	
Span Setting	40% ID Axial 3 divisions	40% ID Axial 3 divisions		40% ID Axial 3 divisions	TSP 3 divisions	
Calibration Coil 5 (+PT) Channels						
Frequency Channel	400 kHz Ch. 3	300 kHz Ch. 6		200 kHz Ch. 9	100 kHz Ch. 12	
Phase Rotation	40% ID Axial 15 degrees	40% ID Axial 15 degrees		40% ID Axial 15 degrees	40% ID Axial 15 degrees	
Span Setting	40% ID Axial 3 divisions	40% ID Axial 3 divisions		40% ID Axial 3 divisions	40% ID Axial 3 divisions	
			Calibration Coil 7		(080"HF Pan)	
Frequency Channel	600 kHz Ch 1	400 kHz Ch. 4		300 kHz Ch. 7		
Phase Rotation	40% ID Axial 15 degrees	40% ID Axial 15 degrees		40% ID Axial 15 degrees		
Span Setting	40% ID Axial 3 divisions	40% ID Axial 3 divisions		40% ID Axial 3 divisions		
			Calibration Coil 4		(Trigger)	
Frequency Channel		100 kHz Ch 11				
Phase Rotation		Trigger Pulse Main Pulse Up				
Span Setting		Trigger Pulse 4 Divisions				

Examination Technique Specification Sheet

ETSS#2 - 3-Coil RPC (.115/+PT/.080)

Revision 6

Page 2 of 7

Configuration Board Settings

trig off	down	configuration# 0	name	samples/sec:see page 1	rec.media = HD	
tester=		board#1	board#2	board#3	board#4	board#5
#of channels= 12		probe#1	probe#1	probe#3	probe#4	probe#5
		DRIVE A D B C	DRIVE A D B C	DRIVE A D B C	DRIVE A D B C	DRIVE A D B C
Drive Polarity		N N	N N N			
Group Number		1 1	1 1 1			
Coil Number		1 4	5 7 8			
freq#1	Time slot #1					
600kHz	G:x2 12 0V		D			
freq#2	Time slot#2					
400kHz	G:x2 12 0V	D	D D			
freq#3	Time slot#3					
300kHz	G x2 12 0V	D	D D			
freq#4	Time slot#4					
200kHz	G x2 12 0V	D	D			
freq#5	Time slot#5					
100kHz	G x2 12 0V	D D	D			

Special Instructions

- 1 One calibration standard may be recorded at the beginning and end of each cal group provided it is a successful scan of the standards complete length.
- 2 Data will be recorded on the PUSH when running top of tubesheet exams Data recorded on the PUSH is acceptable for other regions of the mock-up The operator shall state the direction of scanning in a message.
- 3 All locations shall be acquired from structure to structure unless an encoder is used When an encoder is used the location may be acquired from the respective structure to a few inches past the area of interest. Care should be taken to insure that the proper location is scanned with adequate data past the target location to account for any variations in probe speed or axial scaling.
- 4 Tubes that have been mis-encoded should be corrected by entering a message to void that entry and re-examining the tube with the proper encode.
5. Periodically monitor all channels for data quality and acceptability.

Examination Technique Specification Sheet						
ETSS#2-3 Coil RPC (.115/+PT/.080) Analysis				Revision 6		Page: 3 of 7
Data Analysis						
Calibration Coil 1 (.115" Pancake) Channels						
Channels &	Ch 2		Ch 5		Ch 8	
Frequency	400 kHz 115MR		300 kHz 115MR		200 kHz 115MR	
Phase Rotation	40% ID Axial		40% ID Axial		40% ID Axial	
	15±1°		15±1°		15±1°	
Span Setting	40% ID Axial		40% ID Axial		40% ID Axial	
Minimum	3 divisions		3 divisions		3 divisions	
Calibration Coil 5 (+PT) Channels						
Channel &	Ch 3		Ch 6		Ch 9	
Frequency	400 kHz+Axial		300 kHz+Axial		200 kHz+Axial	
Phase Rotation	40%ID Axial		40%ID Axial		40%ID Axial	
	15°±1°		15°±1°		15°±1°	
Span Setting	40% ID Axial		40% ID Axial		40% ID Axial	
Minimum	3 divisions		3 divisions		3 divisions	
Calibration Coil 7(.080" HF Pancake)						
Channels &	Ch 1		Ch 4		Ch 7	
Frequency	600 kHz 080HF		400 kHz 080HF		300 kHz 080HF	
Phase Rotation	40%ID Axial		40%ID Axial		40%ID Axial	
	15°±1°		15°±1°		15°±1°	
Span Setting	40%ID Axial		40%ID Axial		40%ID Axial	
Minimum	3 divisions		3 divisions		3 divisions	
Calibration Coil 4 (Trigger) Channels						
Channel &	Ch 11					
Frequency	100 kHz TRIG					
Phase Rotation	Trigger Pulse					
	Main Pulse Up					
Span Setting	Trigger Pulse					
Minimum	4 divisions					
Calibration Process Channels						
Channels &	Ch P1(Ch 3)		Ch P2(Ch 6)		Ch P3(Ch 9)	
Frequency	400 kHz + CIRC		300 kHz+CIRC		200 kHz +CIRC	
Adjust Parameters	N/A		N/A		N/A	
Phase Rotation	40%ID Circ		40%ID Circ		40%ID Circ	
	15°±1°		15°±1°		15°±1°	
Span Setting	40%ID Circ		40%ID Circ		40%ID Circ	
Minimum	3 divisions		3 divisions		3 divisions	
Voltage Normalization (See note #3)				Calibration Curve (See Note #11)		
CH	Signal	Set	Normalize	Type	CH	Set Points
1,5,6	100% Axial	20 Vpp	C 1 Chnls			
	EDM (Note 3)	(Note 3)	C 5 Chnls	Ph (Vpp) when req'd	6	Ax. OD 100,60 40/ID 100,60,20
P2	100%Circ 20 volts		Ch P1,P2	Ph (Vpp) when req'd	P2	Cir OD 100,60,40/ID 100,60,20
Data Screening						
Left Strip Chart			Right Strip Chart		Lissajous	
Ch P2			Ch 10 or Analyst Discretion		Ch 6	
Reporting Requirements						
Condition/Region	Report	Ch	Comment			
Single/Multi Ax Ind.	S/MAI	6	Report depth at max amplitude(I-Code Util 1field)			
Single/Multi Cir Ind	S/MCI	P2	Report depth at max amplitude(I-Code Util 1field)			
Single/Multi Vol Ind	S/MVI	6 or P2	Report depth at max amplitude(I-Code Util 1field)			
Volumetric	VOL	6 or P2	Report depth at max amplitude(I-Code Util 1field)			
Mixed mode	MMI	6 or P2	Report depth at max amplitude(I-Code Util 1field)			

Examination Technique Specification Sheet		
ETSS #2 - 3-Coil RPC (.115/+PT/.080) Analysis	Revision 6	Page: 4 of 7
Specific Instructions		
<p>1. Span, Phase, and Volts are to be set using the center of the notch. The above span settings are a minimum.</p> <p>2. Rotate data using "Data Slew Menu" so coils 5 and 7 are aligned with Coil 1. Label the coils using the acronyms shown in the "channel & frequency" column of the data analysis calibration section.</p> <p>3. When the 100% Axial EDM notch saturates, substitute the 60% ID Axial EDM notch for voltage normalization and set it to a value of seven (7) volts (Vpp).</p> <p>4. Use the tube outside diameter (0.875 in.) in user selects for tube diameter.</p> <p>5. The evaluation shall consist of reviewing Lissajous, strip chart, and C-Scan displays to the extent that all tube wall degradation and other conditions are reported.</p> <p>6. All data shall be screened using the 300 kHz plus point coil channel as a minimum.</p> <p>7. All indications indicative of degradation shall be reported, with no minimum voltage threshold. All types of degradation shall be reported with % TW estimate (% TW Field) and a characterization code in the Utility 1 field.</p> <p>8. To achieve accurate measurements, the axial scale should be set using a known distance of greatest length. Manual scales should be reset on each data record which provides structure to structure response.</p> <p>9. All reported indications shall have ID or OD in Util2.</p> <p>10. All coils must be producing acceptable data for all scans.</p> <p>Normalize voltage, set up Cal curves and report all indications in the main Lissajous window. Do not report signals within 1" of the test section. Use the axial and circumferential Lissajous windows provided in the C-Scan plot for determining ID or OD origination if necessary.</p>		

Examination Technique Specification Sheet						
ETSS#2-3 Coil RPC (.115/+PT/.080) Analysis				Revision 6		Page 5 of 7
Data Sizing						
Calibration Coil 1 (.115" Pancake) Channels						
Channels &	Ch 2		Ch 5		Ch 8	
Frequency	400 kHz 115MR		300 kHz 115MR		200 kHz 115MR	
Phase Rotation	40% ID Axial		40% ID Axial		40% ID Axial	
	15±1°		15±1°		15±1°	
Span Setting	40% ID Axial		40% ID Axial		40% ID Axial	
Minimum	3 divisions		3 divisions		3 divisions	
Calibration Coil 5 (+PT) Channels						
Channel &	Ch 3		Ch 6		Ch 9	
Frequency	400 kHz+Axial		300 kHz+Axial		200 kHz+Axial	
Phase Rotation	40%ID Axial		40%ID Axial		40%ID Axial	
	15°±1°		15°±1°		15°±1°	
Span Setting	40% ID Axial		40% ID Axial		40% ID Axial	
Minimum	3 divisions		3 divisions		3 divisions	
Calibration Coil 7(.080" HF Pancake)						
Channels &	Ch 1		Ch 4		Ch 7	
Frequency	600 kHz 080HF		400 kHz 080HF		300 kHz 080HF	
Phase Rotation	40%ID Axial		40%ID Axial		40%ID Axial	
	15°±1°		15°±1°		15°±1°	
Span Setting	40%ID Axial		40%ID Axial		40%ID Axial	
Minimum	3 divisions		3 divisions		3 divisions	
Calibration Coil 4 (Trigger) Channels						
Channel &	Ch 11					
Frequency	100 kHz TRIG					
Phase Rotation	Trigger Pulse					
	Mam Pulse Up					
Span Setting	Trigger Pulse					
Minimum	4 divisions					
Calibration Process Channels						
Channels &	Ch P1(Ch 3)		Ch P2 (Ch 6)		Ch P3 (Ch 9)	
Frequency	400 kHz + CIRC		300 kHz+CIRC		200 kHz +CIRC	
Adjust Parameters	N/A		N/A		N/A	
Phase Rotation	40%ID Circ		40%ID Circ		40%ID Circ	
	15°±1°		15°±1°		15°±1°	
Span Setting	40%ID Circ		40%ID Circ		40%ID Circ	
Minimum	3 divisions		3 divisions		3 divisions	
Voltage Normalization (See note #3)						
CH	Signal	Set	Normalize	Type	CH	Set Points
1,5,6	100% Axial	20 Vpp	C 1 Chnls			
	EDM		C 5 Chnls	Phase (Vpp)	6	Ax OD 100,60 40/ID 100,60,40
P2	100% Circ	20 Vpp	Ch P1,P2	Phase (Vpp)	P2	Cir OD 100,60,40/ID 100,60,40
Data Screening						
Left Strip Chart			Right Strip Chart		Lissajous	
Ch P2			Ch 10 or Analyst Discretion		Ch 6	
Reporting Requirements						
Condition/Region	Report	Ch		Comment		
Single/Multi Ax Ind	S/MAI	6		See next page		
Single/Multi Cir Ind	S/MCI	P2		See next page		
Single/Multi Vol Ind	S/MVI	6 or P2		See next page		
Volumetric	VOL	6 or P2		See next page		
Mixed mode	MMI	6 or P2		See next page		

Specific Instructions

These instructions apply to line-by-line sizing of all indications. The specific instructions for analysis as delineated in ETSS#2 still apply, as appropriate, to this ETSS.

For sizing circumferential indications:

Voltage normalization is performed in the axial Lissajous window and is set on the 100% circumferential notch at 20 volts. Adjust the span such that the 40% ID circ notch is 3 div for 300 kHz. Monitor the 300 kHz raw and process channels on the strip chart and scroll the region of interest while viewing the Lissajous. Terrain-plot the 300 kHz raw and process channels in the area of interest.

A phase curve is established on process channel P2 using 100%, 60%, 40% circumferential notches in the axial Lissajous window; in addition, set a zero percent value in the curve. All phase measurements are performed on the Lissajous response in the axial Lissajous window. Careful analysis should be performed, watching specifically for any change in the Lissajous signal. Record a zero percent call prior to the first call of the indication and after the last call unless the indication is 360 degrees. Record only those indications which provide a flaw-like Lissajous response at a maximum of 10 degree increments. Applying an axial "to-from" may be necessary to reduce the effect of geometry on the indication phase measurement. Filters are acceptable for detection but are not applied for sizing. Dent responses may also form in the same plane as the flaw response.

For sizing axial flaws:

Voltage normalization is performed in the circ. Lissajous window and is set on the 100% axial notch at 20 volts. Adjust the span such that the 40% OD axial notch is 3 div. at 300 kHz (channel 6). Set phase so that the 40% ID axial notch is 15 degrees at 300 kHz. A phase curve is established on the 300 kHz raw channel using 100%, 60%, and 40% ID axial notches. Terrain-plot the 300 kHz raw channel in the area of interest. Axial indications will form in the positive direction.

Dent responses may also form in the same plane as the flaw response. Careful analysis should be performed watching specifically for any change in the Lissajous signal. Phase and amplitude measurements are performed on the Lissajous response from the circumferential Lissajous window. Record only those indications which provide a flaw-like Lissajous response. Apply a circ. from-to to isolate the indication and minimize the number of data points in the Lissajous. Use the strip chart to step through one scan line at a time along the length of the indication. Record a call for each step along the length of the indication. Record a zero percent call prior to and as near the first call of the indication and after the last call.

Examination Technique Specification Sheet		
ETSS #3 - 3-Coil RPC (.115/+PT/.080) Analysis and Sizing	Revision 6	Page: 7 of 7
Specific Instructions		
<p>Filters are acceptable for detection but are not applied for sizing.</p> <p>Adjustment Procedure At the completion of the initial analysis process, adjustment for data points at the ends of the cracks is required. Data points within 0.2 in. of the indicated crack ends will be adjusted as follows:</p> <p>(a) Ignore all data points from the first reading to the point at which phase angles change from ID to OD. (Paragraph A does not apply if the crack exhibits primarily OD phase angles over its length)</p> <p>(b) Data points of less than 1 volt, with ID phases indicating 85% throughwall and greater, will be ignored from the first reading to that point provided within 0.2 in. of the first reading.</p> <p>c) ID phase data points of less than 1 volt, exhibiting depth increases of greater than 10% throughwall over approximately a 0.05 in. span, will be ignored.</p>		

The resolution analysts and independent QDAs were Level III or III-a. During the RR exercise, the primary and secondary analysts did not communicate with each other or the resolution analysts. Upon submitting their reports, the primary and secondary analysts could discuss the reports with the resolution analysts but the reports were not changed as a result. The resolution analysts provided the report used for establishing POD.

2.2.6 Review of Training Manual by Teams

Team members reviewed the training manual either the day before or the same day that the ANL proctor arrived with the mock-up data and site-specific tests. The analysts were able to review the types of degradation in the mock-up and typical EC signal responses. They also carefully reviewed the mock-up geometry and became familiar with the EC signal response from test-section ends, as well as from roll transitions, TSPs, and run-out section of the mock-up. The analysts reviewed the reporting procedure and could ask questions related to the training manual, to be answered by ANL staff.

2.2.7 Sequence of Events during Round-Robin Exercise

Before the RR exercise was started, a training manual, supplemental schematics, and final reports for the training data were sent to the teams for review. The training optical disk was either sent for review before the exercise was started or was provided by the proctor on his arrival. The ANL proctor arrived at the analysts' site with exams, documentation (analysts' guidelines, etc.), and optical disks containing all the data to be analyzed. The proctor provided nondisclosure agreements signed by all analysts participating in the RR and collected all analyst certifications. After the analysts finished studying the

training manual, analyst guidelines, training disk, and supplemental schematics, the ANL proctor gave and graded the written and practical site-specific exams. The passing grade for the written exam was 80%. For the bobbin coil practical exam, the analysts had to correctly call all "T" codes without excessive overcalling. For the MRPC data the analysts had to correctly indicate the presence of all cracks and their orientations (circumferential vs. axial). About 10% of the analysts had to take the second practical exam, which they passed. The ANL proctor retrieved the exam disk after testing was completed. The process of evaluating the analysts closely followed standard industry practice. After of the analysts completed the site-specific exam the proctor provided the third disk containing all bobbin coil data. The primary and secondary analysts analyzed the BC data and their reports were recorded on the disk. The resolution analysts resolve the primary/secondary discrepancies. A resolution analyst's report was provided along with primary and secondary analyst reports. The Argonne BC disk contained primary, secondary, and resolution analysts' reports for BC data at the conclusion of the BC analysis. The proctor collected hard copies of these reports and the data disk.

The ANL proctor then provided a fourth disk containing MRPC special-interest data. The primary and secondary analysts analyzed the MRPC data and their reports were recorded on the disk except for tube sheet data, which was analyzed later. Analysts reported depth at maximum amplitude and location information, following instructions in the training manual. The resolution analysts resolved the primary/secondary discrepancies. A resolution analyst's report is provided. Upon completion of the special-interest data, the special interest disk contained primary, secondary and resolution analysts' reports for MRPC data at other than the tube sheet level. The proctor collected hard copies of these reports and the data disk

The ANL proctor then provided a fifth disk containing only tube sheet (Level A) MRPC data from all 400 tubes. The primary and secondary analysts analyzed the data of the tube sheet level and provided their report. The resolution analysts resolved any discrepancies and provided their report. The completed tube sheet disk contains primary, secondary, and resolution analysts' reports for the tube sheet. The report was printed and the hard copy given to the ANL proctor, who also collected the data disk.

When the testing was completed, the proctor returned to ANL with all the optical disks containing the analysis reports for the team.

2.2.8 Data Analysis Procedures and Guidelines

All indications were evaluated. Indication types to be reported were characterized by using the frequencies or frequency mixes that were qualified. For indication types to be reported in terms of depth, a means of correlating the indication depth with the signal amplitude or phase was established and based on the basic calibration. Flaw depth was reported in terms of percentage of loss of tube wall. For axial and circumferential flaws reported with MRPC, depth was determined from the "hit" that provides the greatest amplitude. For circumferential cracks, maximum depth was determined from axial cuts through the crack. Reported indications, indicative of possible tube wall degradation, were described in terms of the following, as a minimum:

- (a) The location along the length of the tube with respect to the actual data point, as appropriate for the technique used. For MRPC data, the circumferential location was defined by the data point of the flaw called.
- (b) The depth of the indication through the tube wall, when applicable.

- (c) The signal amplitude.
- (d) The frequency or frequency mix from which the indication was evaluated.

In addition to the ANL documents, the analysts were given an errata sheet with eight corrections and two procedure changes. The errata sheet indicated additional three letter codes to be used, clarifications regarding setting of span and inputting of data, and corrections to references in documentation provided. The changes involved clarification regarding how to input MRPC data for complex flaws (maximum of four indications were recorded for a given axial position) and a channel change for the voltage normalization of the high-frequency coil of the three-coil MRPC probe.

2.3 Comparison of Round-Robin Data Acquisition and Analysis to Field ISI

The RR exercise very closely mimics a field ISI. Procedures, equipment used, and documentation are based on those used by industry for inspection of steam generators. Similar to field inspections, a Zetec MIZ30 instrument, along with a 10-D pusher-puller and EddyNet 98 software, were used to collect the data. A standard magnetically biased bobbin coil and an MRPC with 0.115 pancake, +Point and 0.080 shielded high-frequency pancake coils were used. Round-robin teams used EddyNet98 software to analyze the data. While flaws and flaw responses have been shown to be representative of field flaws, the mock-up is mechanically different from a steam generator. There are no U-bends in the mock-up. Test sections are in contact with each other, resulting in strong EC signals similar to a 360° 100%TW circumferential crack at the test section ends. The analysts, through training and practice, easily adjusted to these signals and there is no indication that the PODs reported are compromised by this mechanical arrangement. Another physical difference is the presence of a circumferential marker at the bottom of each test section. Again, through review of training examples, the analysts quickly became adjusted to the marker signals and their presence appears to have had no effect on the POD results.

Noise levels in the mock-up are generally lower than those in field data. Although many of the test sections had sludge and magnetite on the OD, many test sections with flaws did not. Noise as severe as that in the U-bends of plants such as at Indian Point 2 was not present in the mock-up freespan and TSP levels. A review of BC field data from seven plants provided a general idea of the noise from a bobbin coil field inspection. Baseline noise in the bobbin coil voltage trace of field data of about 0.7 V was generally seen (excluding U-bends and tube sheet). The mock-up BC base-line noise level was less, about 0.3 to 0.4 V. This low noise suggests that the results from the mock-up are an upper limit on POD for the TSP and freespan levels for flaws with low-voltage bobbin coil signals. While it is possible to have a deep crack with a low BC voltage, the difference in baseline noise levels between field and the mock-up would affect the POD only somewhat for shallow cracks and is not expected to have a significant effect on the logistic fit. Noise in the mock-up tube sheet level, however, was significant and did play a role in the ability of analysts to detect and correctly characterize the flaws in and around the roll transition zone (RTZ). The tube sheet noise is present in the mechanically expanded portion and in the roll transition. Variation in the geometry of the RTZ contribute to the difficulty of analyzing data from the tube sheet and can be seen in the three examples of flaw-free tube sheet mock-up test sections presented in Figures 2.52-2.54. For comparison, an isometric plot from McGuire field data is presented in Figure 2.55. The McGuire and mock-up RTZ geometries are similar.

As in field inspections, the analyst involved with the RR decides whether the quality of the data is sufficient to analyze for flaws. In one example from the field (Callaway), the bobbin coil is replaced when the V_{pp} exceeds twice the initial control level (from a reference tube). In the RR, the quality of the

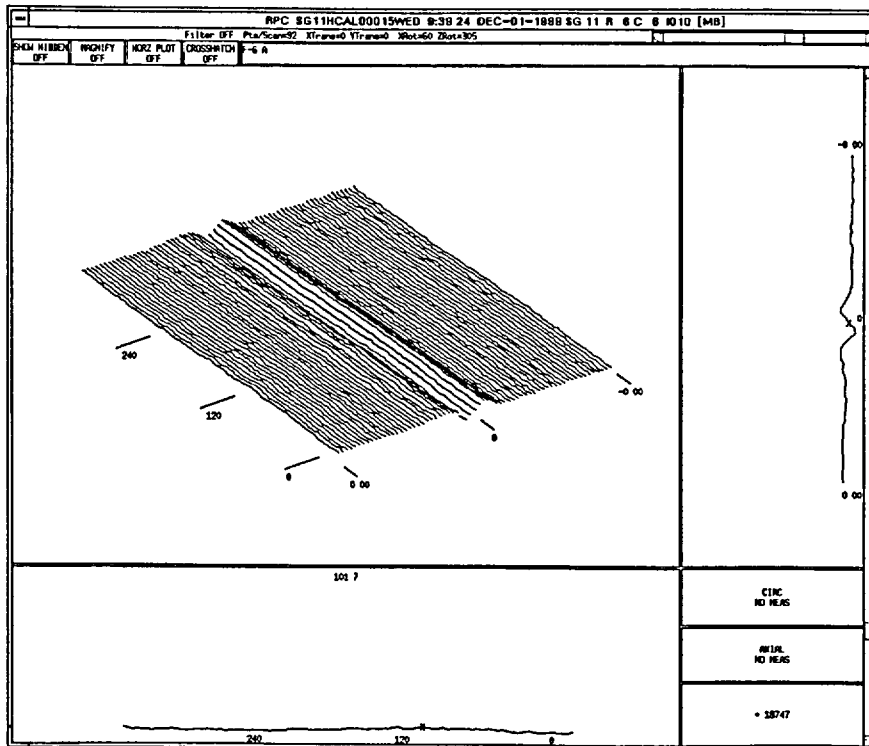


Figure 2.52 Isometric plot of mock-up tube sheet level roll transition from data collected by rotating +Point coil at 300 kHz (example 1).

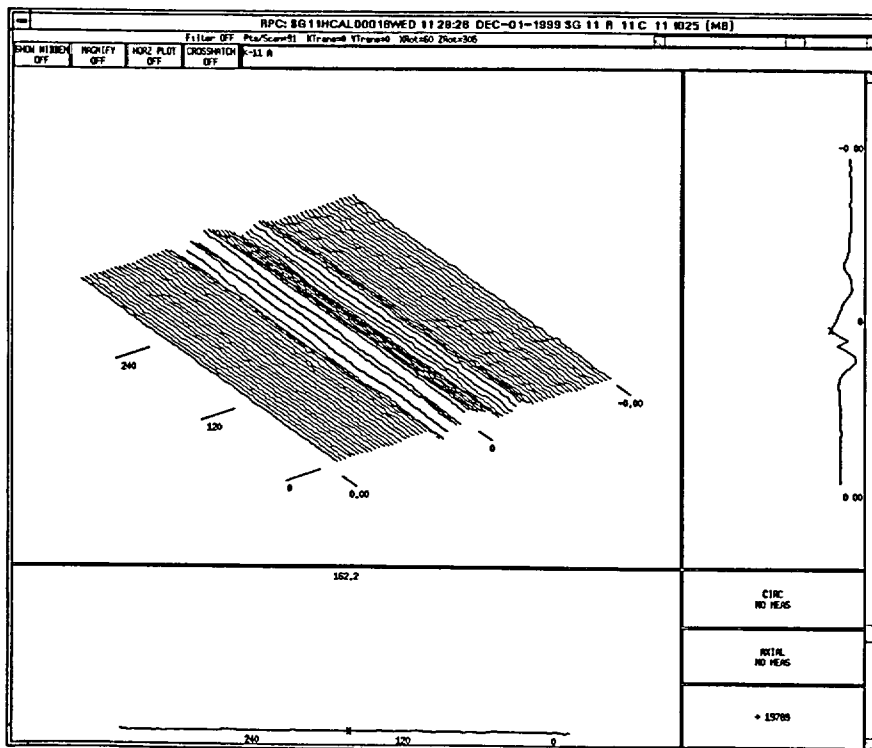


Figure 2.53 Isometric plot of mock-up tubesheet level roll transition from data collected by rotating +Point coil at 300 kHz (example 2).

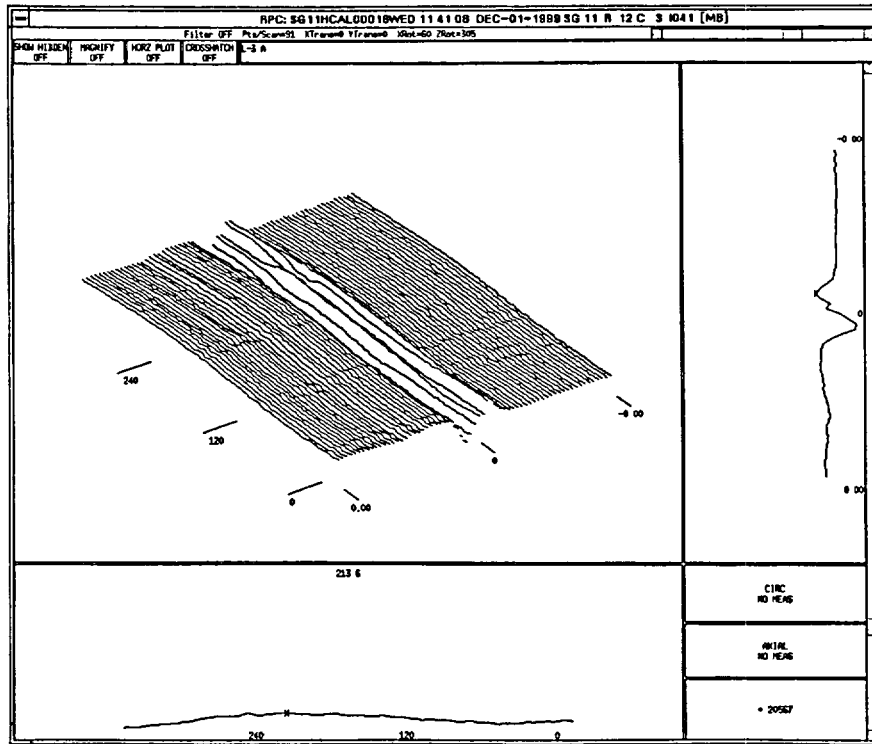


Figure 2.54 Isometric plot of mock-up tubesheet level roll transition from data collected by rotating +Point coil at 300 kHz (example 3).

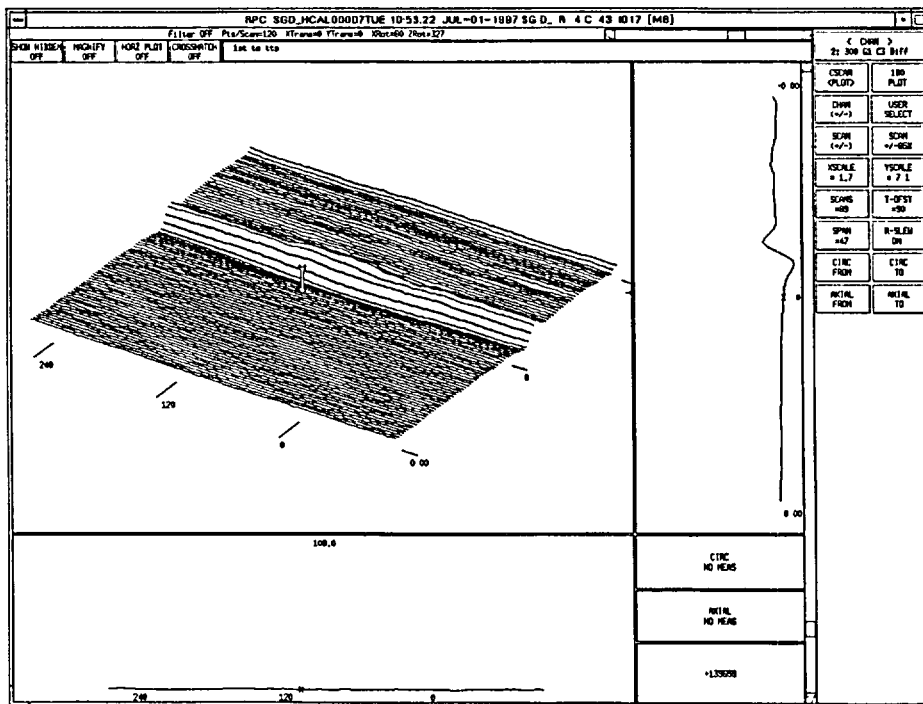


Figure 2.55 Isometric plot of roll transition in tube sheet from McGuire steam generator

bobbin coil data did not vary during the time BC data was collected. At Callaway, for example, the signals from notches in the standard must be clearly discernible from background noise when MRPC data are collected; otherwise the probe is replaced. A similar protocol was followed for the RR, except that if the MPRC probe could not be nulled it was replaced. This procedure led to high-quality MRPC data from the mock-up test sections.

Parameters set for the probes are typical of ISI and are detailed in the earlier section (2.2.4) on Examination Technique Specification Sheets. The 100, 200, 300, and 400 kHz frequencies used for the BC are standard for the industry and allow use of the conventional 100-400 kHz mix to suppress the TSP indication. The range of frequencies used for the MPRC data covers the requirements of the EPRI ETSSs for flaws present in the mock-up. The mock-up may have a greater variety of flaws than might be present in any given steam generator. Nevertheless, the analysts are familiar with the EC responses to all types of flaws in the mock-up, as demonstrated by the analysts' passing the EPRI personnel qualification exams. The variety of flaws in the mock-up does not impact the POD results. Examples of EC data (BC as well as MRPC) using EddyNet 98 software are presented for a variety of flaws in the mock-up in Figures 2.56 to 2.62.

Reporting requirements are slightly different than for a field ISI. In the analyst reports for the mock-up, there is an extra column showing whether the flaw indication is OD or ID. In addition, the location of an indication is given by data point, not number of inches from a physical reference. Another variation from conventional reporting is the requirement to report no more than four flaws (two axial and two circumferential) at any given axial location. These variations were necessary to provide an exercise that could be completed in a reasonable time (7-8 days) and provide as much information as possible while not negatively affecting the work of the analysts. These variations from standard practice are

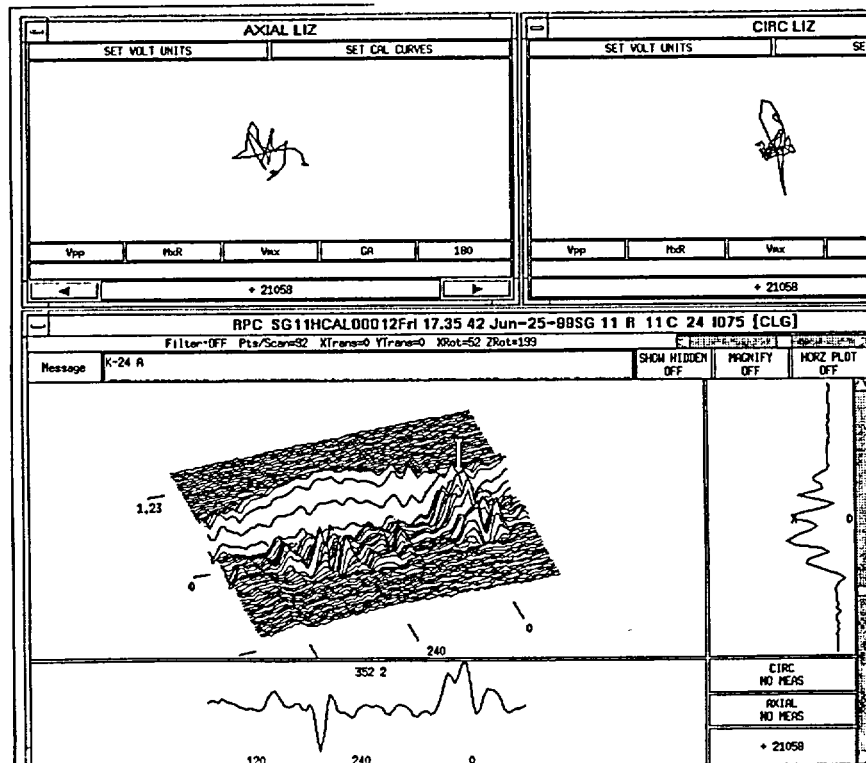


Figure 2.56 LODSCC at TS with sludge (MRPC).

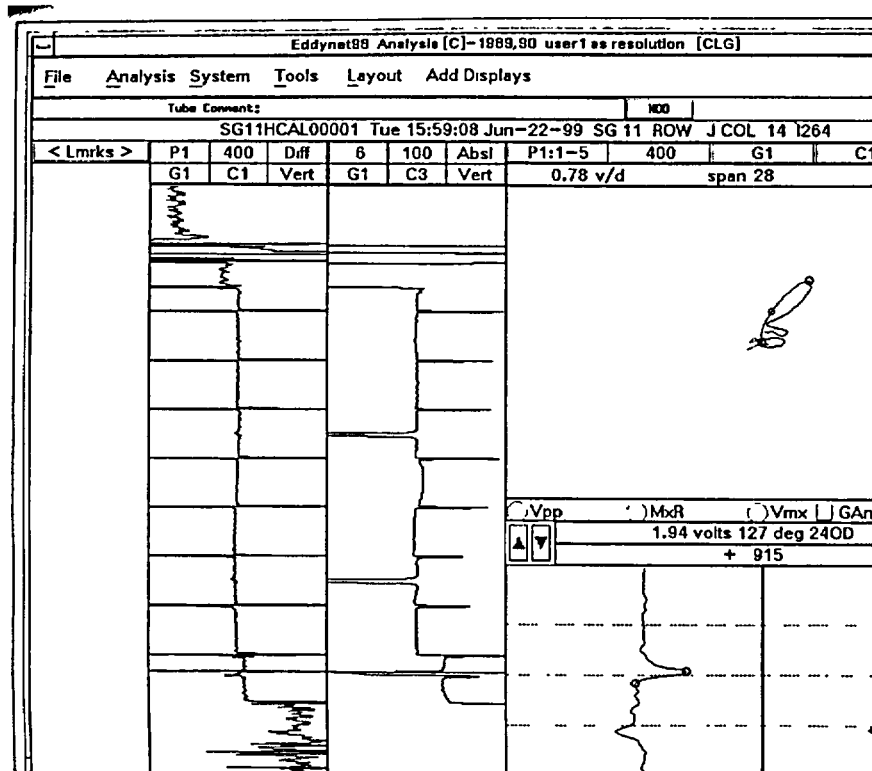


Figure 2.57 LODSCC at a TSP (BC)

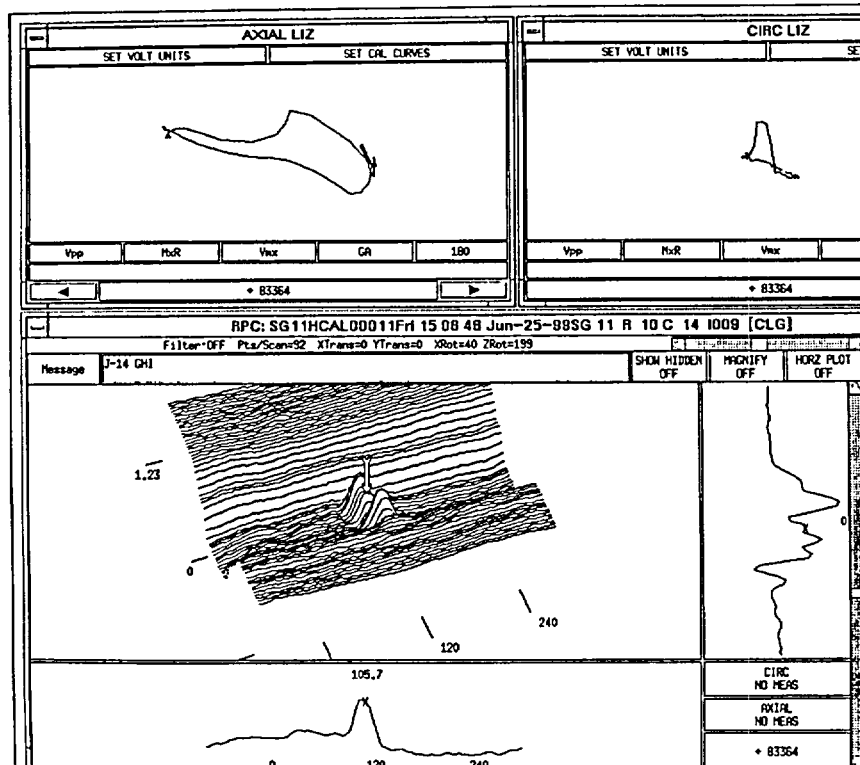


Figure 2.58 LODSCC at TSP (MRPC)

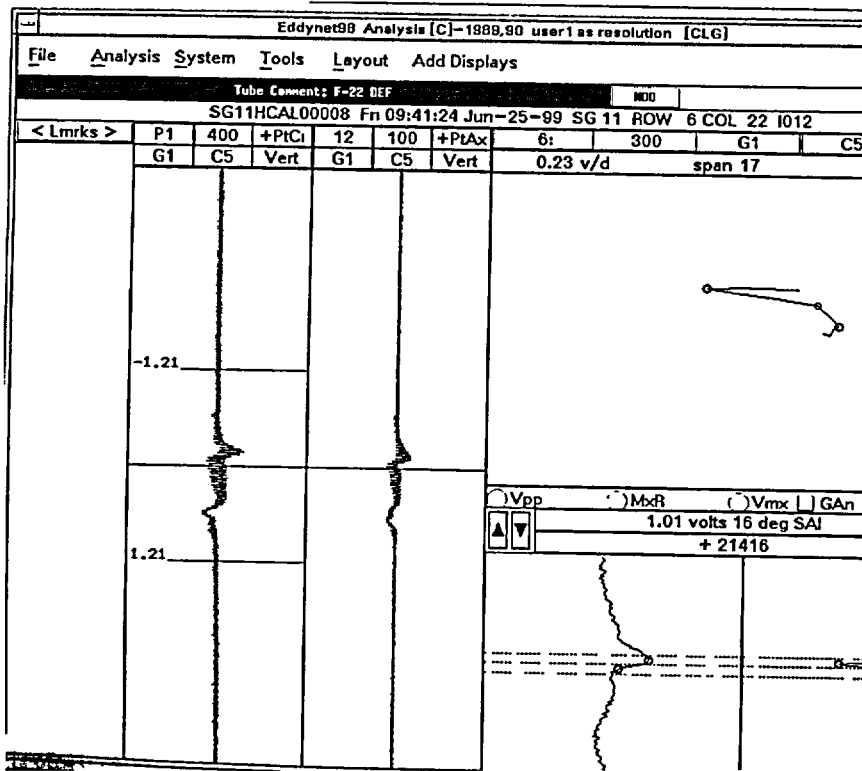


Figure 2.59 LIDSCC in dent at TSP (bobbin coil).

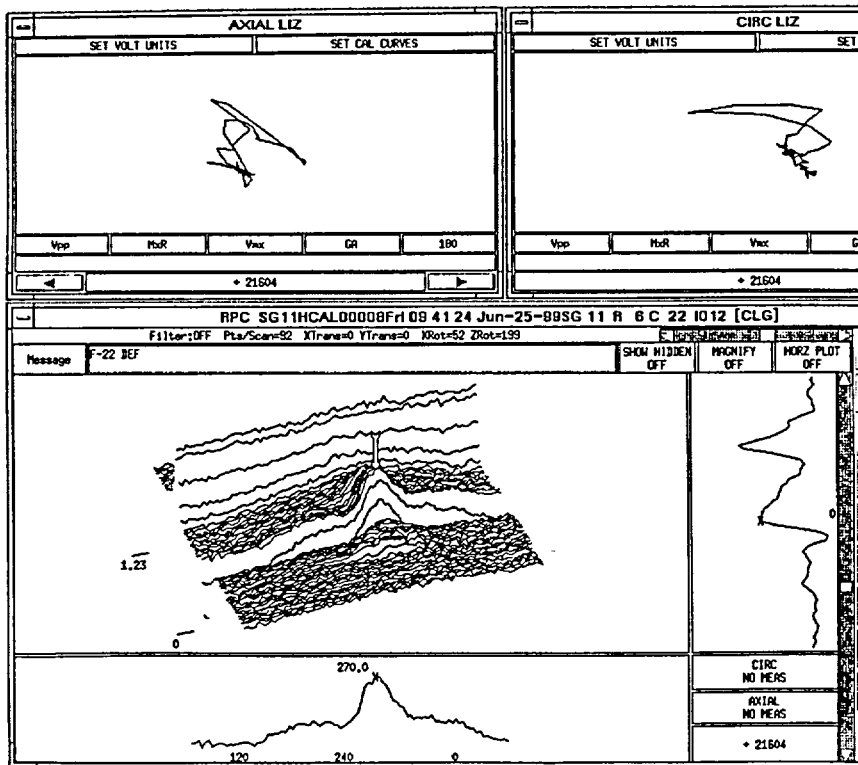


Figure 2.60 LIDSCC in dent at TSP (isometric plot).

Figure 2.62

IGA at TSP (RPC).

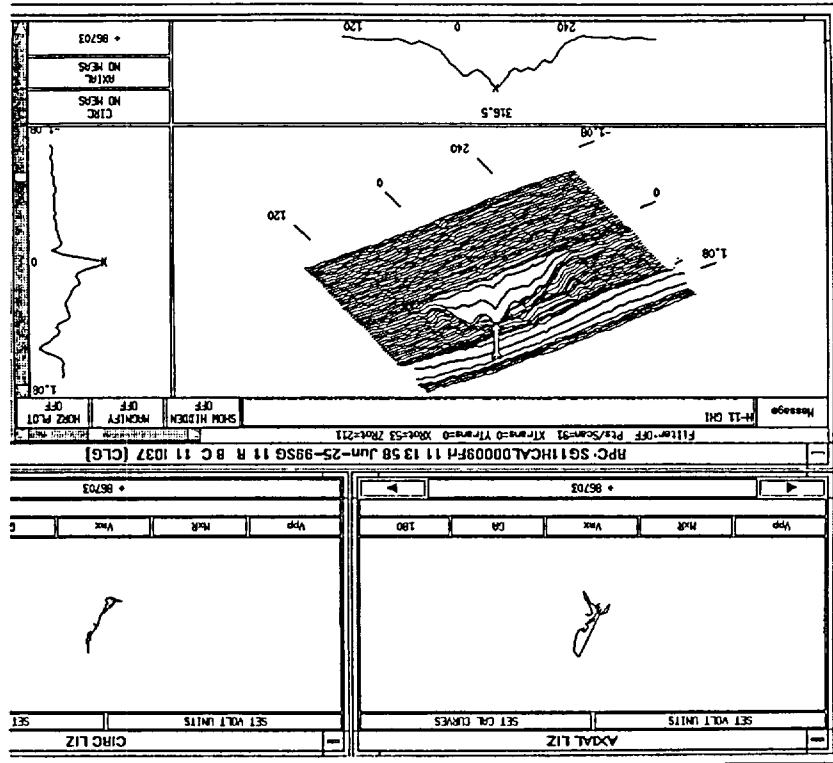
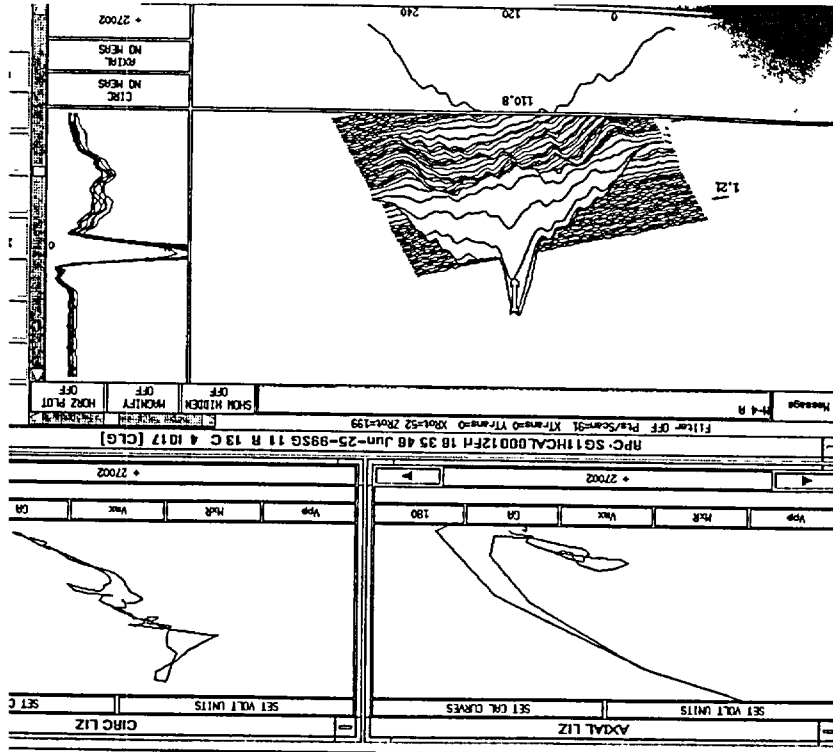


Figure 2.61

CIDSCC at TS with sludge.



carefully described in the training manual and analyst guidelines. The analysts made the adjustment to the mock-up reporting requirements quickly. A primary objective of the RR is to establish the POD for deep flaws. While some deep flaws may result in relatively low EC signal amplitude, the deep flaws generally have high signal amplitudes. As a result, although the voltage histogram for the mock-up flaws looks reasonable, there are more high-voltage signals than would be expected from a field inspection. A review of field data, such as from McGuire (a better than average plant), shows that while BC signals from TTS can be many volts in amplitude (i.e. >10 V), the signals from the TSP regions are primarily less than 3 V, with most less than 1 V in the 100-400 kHz mix channel. Stronger TSP flaw signals can be found in the mock-up because of the emphasis on deep flaws.

Analysis training and testing for the RR is comparable to that for a field ISI. For example, in a recent outage at the Union Electric Callaway Plant, a training class was presented on examples of Callaway's active degradation as well as potential degradations: ding and freespan OD cracking. This protocol is virtually the same as for the mock-up except that a formal class was not arranged. At Callaway, personnel performing the data analysis were required to successfully complete a site specific performance demonstration involving bobbin coil and MRPC data prior to performing any data analysis. The written exam covered design, data acquisition, and analysis. The practical exam covered in-situ tubes with calls based on expert opinion. Overcalls were allowed for up to 10% of all intersections. Passing required a correct call as to whether a crack is axial or circumferential. For rotating probe data, 100% on detection and orientation is required to pass the test. This protocol on testing is identical in every respect to that for the ANL mock-up.

2.4 Strategy for Evaluation of Results

2.4.1 General Principles

POD has been determined for the flaws in the mock-up as a function of flaw type and flaw location (i.e., freespan, TSP, and tubesheet). The PODs have been plotted against maximum depth, m_p , average depth, and, for the case of circumferential cracking, area. Logistic fits have been calculated and include errors in depth sizing and false call rates. Upper and lower 95% confidence limits are included in the logistic fit curves. An analyst is given credit for detecting a flaw if the call is an "I" code (e.g., NQI, DNI, DTI for BC calls, MAI, SAI, SCI, MCI, and MMI for MRPC calls) and the location is within 25 mm of the ends of the flaw.

2.4.2 Tolerance for Errors in Location

The location error allowed for calls made from bobbin coil data is 25 mm from either end of the flaw along the tube axis. This allowed error converts to 30 data points for bobbin coil data. For MRPC data the error allowed in the axial direction is also 25 mm from the ends of the flaw along the tube axis. This allowed error converts to 3000 data points for the MRPC data.

2.4.3 Handling of False Calls

Analysts' reports were used to determine the false call rate. The rate was determined from a review of randomly selected flaw-free test sections in the mock-up and the number of "I" codes called in those test sections. An "I" code call (NQI, DTI, DNI) indicates that a flaw indication was present in the section even though no flaw was present. A total of 522 test sections were analyzed. No known stress corrosion cracks (SCC) were in any of the test sections. With 11 teams, there were 5742 chances to make a false

call. The result was 6% for the tubesheet level using MRPC data, 1.7% for the TSP with BC data, and 0.1% for the freespan with BC data. These rates are low enough to avoid any consideration of penalizing the analysts for false calls. The false call rates for the TSP and freespan are lower than found in field inspections because of lower noise levels found in the mock-up. The false call rate for the tube sheet is of the same order found in the field. The use of higher false call rates would lead to higher POD curves and thus the results presented in this report could be considered conservative. However, even doubling the false call rate would have no discernible effect on the POD curves presented in this report.

2.4.4 Procedures for Determining POD

Data from the eleven teams participating in the RR exercise are first handled by using the EPRI “Shell” program, which had been loaded into an ANL computer. The optical disks used by the analysts contain the analysts’ reports and are read by the “Shell” Program. The program sorts the data. Calls from primary, secondary, and resolution analysts can be compared to the results of expert opinion. Note that the result of the comparison to expert opinion is not the result sought because expert opinion does not always provide the true state of the flaws. The reference state of the flaws is provided by the ANL flaw characterization algorithm, which uses a multiparameter approach to analyzing the EC data taken at multiple frequencies. All POD curves are presented by using the depth estimates from the analysis of EC data using the multiparameter algorithm. Three reports are analyzed for each team for each of the three parts of the RR; the bobbin coil data, the MRPC tube sheet data, and the MRPC special-interest (spin call) data. The “Shell” program sorts the data by degradation and, for LODSCC at the tube support plate, by voltage. The principal advantage of using the “Shell” program is the ability to transfer the analysts’ reports into an Excel file, which could then be used to carry out the statistical analysis. Table 2.8 provides the number of teams analyzing the three data disks. One team was not able to complete the Special Interest MRPC disk. Table 2.9. summarizes the reporting format for the EPRI “Shell” program.

Tables 2.10 and Table 2.11 show simulated inputs to the Flaw Table and the Flaw Indication Table for a bobbin coil inspection. Table 2.10 shows a flaw in row A, column 7, at TSP level D. The maximum BC voltage is at data point 1865 (as noted in the column “Flaw ID”). The flaw is a longitudinal ID with a BC voltage of 2.04 and phase angle of 25 degrees. The flaw begins at data point 1839 and ends at 1873. About 3600 data points are stored for each tube examined with the bobbin coil

Table 2.8 Number of round-robin analyst reports for the three data sets from the first eleven participating teams.

Mock-up Data Set	Number of Primary Analyst Reports To Date	Number of Secondary Analyst Reports To Date	Number of Resolution Analysts Reports To Date
Bobbin Coil (All Tubes)	11	11	11
MRPC (All Tube Sheet Test Sections)	11	11	11
MRPC (All Special Interest; i.e., Spin Calls)	10	10	10

Table 2.9 Information provided by the EPRI "Shell" program using results from round-robin analysts' reports.**

Flaw Type	2	3	4	5	6	7	8	9	10	11	12	13	14	26	27	28	Total	31	32	Total	33	34	Total	
No. of Expert Opinion Calls	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
No Analyst Calls	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
RMSE Volts	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
No of Overcalls	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*

*Data Generated

**Note that analysts' reports are compared to expert opinion not to true state of the mock-up.

2	TSP/BC/ODSCC 0 25-0 49 v.	12	TSP/BC/IGA/Freespan
3	TSP/BC/ODSCC 0 50-0 74 v.	13	BC/ODSCC/Sludge Pile
4	TSP/BC/ODSCC 0 75-0 99 v.	14	Expansion/BC/PWSCC
5	TSP/BC/ODSCC 1.00-.1.49 v.	26	BC/ All Dents
6	TSP/BC/ODSCC 1.50-2.99 v.	27	BC/Other
7	TSP/BC/ODSCC > 3.00 v.	28	SP/BC/Thinning-Wastage/Freespan
8	TSP/BC/PWSCC-Dent < 2.0 v.	31	+Point/PWSCC
9	BC/ODSCC/Freespan	32	+Point/ODSCC
10	BC/PWSCC-Ding/Freespan	33	+Point/Expansion/PWSCC
11	TSP/BC/Wear/Freespan	34	+Point/Expansion/ODSCC

Table 2.10 Simulated input to flaw table for bobbin coil inspection

Flaw ID	Flaw	BC Volts	BC Phase	ID/OD	Beg Pt.	End Pt.	Depth (%TW)	Expert BC Call	True State Call
A07D18 65	LID	2.04	25	ID	1839	1873	40	NQI	SAI
M14F31 77	LOD	2.61	70	OD	3157	3192	90	NQI	SAI

Table 2.11 Simulated Bobbin Coil Input to Flaw Indication Table.

Indication	BC Volts	BC Phase	ID/OD	Depth Est.	Call
AO7 1855	2.14	29	ID	50	DTI
M14 3157	2.68	60	OD	80	NQI

(nine test sections). Table 2.10 shows a depth estimated to be 40%TW. This depth is determined by application of a multiparameter algorithm to MRPC data for the flaw. An “I” code triggers an inspection with an MRPC. The reference-state three-letter code is SAI, single axial indication. A second example is also provided. The second flaw, a longitudinal ODSCC, is at row M, column 14, and at freespan level F. The result for the bobbin coil inspection is shown in Table 2.11. An indication was found in row A, column 7, at data point 1855, close to the correct flaw location. The ID/OD call is correct and an “I” code is also called, although in this case it is DTI (distorted TSP indication). The DTI call also requires MRPC data to be acquired. The second indication would also be graded as a correct call. Indication tables are generated for both bobbin coil and MRPC data and compared with the Flaw Indication Table, which contains all information needed to estimate POD.

2.4.4.1 Converting SSPD Result to Text Files and Excel Files

The Eddynet software provides a series of files that contain the reports of results from each analyst who participated in the RR. These data are saved under an Eddynet environment and are identified by extensions that refer to primary, secondary, and resolution analysts’ reports. These files were then read by a text editor and converted into a format useable for off-line manipulation. The text files were then imported into Excel. Excel macros were written to sort the results and carry out the grading.

2.5 Statistical Analysis

2.5.1 Determination of Logistic Fits

To obtain an analytical form for the probability of detection curve, we assume that the probability of detection as a function of depth can be expressed as a linear logistic function of x :

$$p(x) = \frac{1}{1 + e^{a+bx}}, \quad (3)$$

or

$$p(x) = \text{logistic}(a + bx)$$

where a and b are parameters that will be determined by comparison with the observed results. Other forms for the POD curve can be chosen, but the linear logistic curve has been widely used for this purpose, and is widely used in other fields to describe binomial responses (detected or not detected) [4].

The Method of Maximum Likelihood [5] is widely used to estimate statistical parameters such as a and b . For quantities that are normally distributed, it can be shown to be equivalent to the familiar method of least squares [5–6]. It is more generally applicable, however, and can be applied to events such as detection of cracks that are not normally distributed.

If $p(x)$ is the probability that a crack of depth x will be detected by an inspection team, the probability that the crack will not be detected is $1-p(x)$. The probability that n out of N teams of inspectors will detect a crack of depth x is

$$\binom{N}{n} p^n (1-p)^{N-n}, \quad (4)$$

where $\binom{N}{n} = \frac{N!}{n!(N-n)!}$ is the combinatorial symbol. Equation 4 assumes that the teams are equally capable and are independent of each other.

The probability L that a collection of K cracks of depth x_1, x_2, \dots, x_K will be detected successfully n_1, n_2, \dots, n_K times is just the product of the probabilities for the individual cracks:

$$L = \prod_{k=1}^K \binom{N_k}{n_k} p_k^{n_k} (1-p_k)^{N_k-n_k}, \quad (5)$$

where $p_k = p(a, b, x_k)$ and a, b are the parameters of the logistic fit. The Method of Maximum Likelihood seeks to determine a, b such that the probability of the observed outcome, L , is maximized. It is more convenient to deal with the log of Eq. 5:

$$\ln(L) = \sum_{k=1}^K \ln\left(\binom{N_k}{n_k}\right) + \sum_{k=1}^K [n_k \ln(p_k) + (N_k - n_k) \ln(1-p_k)] \quad (6a)$$

$$D = \sum_{k=1}^K [n_k \ln(p_k) + (N_k - n_k) \ln(1-p_k)]. \quad (6b)$$

The first summation in Eq. 6a is a constant that is independent of the choice of a and b . Defining D as the second summation in Eq. 6a, we can determine the choice of a and b that maximizes D or L by solving

$$\frac{\partial D}{\partial a} = 0$$

$$\frac{\partial D}{\partial b} = 0$$

or

$$\sum_{k=1}^K \frac{n_k - N_k p_k}{p_k (1-p_k)} \frac{\partial p_k}{\partial a} = 0$$

$$\sum_{k=1}^K \frac{n_k - N_k p_k}{p_k (1-p_k)} \frac{\partial p_k}{\partial b} = 0 \quad (7)$$

Differentiating Eq. 7, we find that

$$\frac{\partial p_k}{\partial a} = -p_k (1-p_k)$$

$$\frac{\partial p_k}{\partial b} = -p_k (1-p_k) x_k \quad (8)$$

Using Eqs. 5-6, Eqs. 7 –8 reduce to

$$\begin{aligned}\sum_{k=1}^K (n_k - N_k p_k) &= 0 \\ \sum_{k=1}^K (n_k - N_k p_k) x_k &= 0\end{aligned}\tag{9}$$

Equations 8-9 are a pair of simultaneous nonlinear equations for a, b. For computation, it is generally more convenient to determine a, b by algorithms that directly maximize the expiation D rather than attempting to solve these equations. Excel spreadsheets were developed to do this and benchmarked against the commercial statistical software package STATA.

2.5.2 Uncertainties in the POD Curves

Eqs. (9) can be solved for a and b. These values depend on the round robin results, i.e, on $n_1, n_2,$ etc. If the round robin was repeated with a different set of teams or a different set of cracks, different values would be obtained for a and b, i. e, there will be a distributions of values for a and b. Similarly, the depths of the cracks, $x_k,$ are not known exactly, instead we have a measured value $\hat{x}_k = x_k + \epsilon_k$ where ϵ_k is the error in the measured value of $x_k.$ The errors will be random variables. The distributions for a and b can be characterized by mean values and variances. The mean values can be found by solving Eqs. (9), although it is generally easier to obtain a and b by direct maximization of D (Eq. 6b). However, Eqs. (9) involve the unknown quantities x_k where in reality only the measured values, $\hat{x}_k,$ are known. If we denote the solution of the approximate equations,

$$\begin{aligned}\sum_{k=1}^K (n_k - N_k \hat{p}_k) &= 0 \\ \sum_{k=1}^K (n_k - N_k \hat{p}_k) \hat{x}_k &= 0\end{aligned}\tag{10}$$

which involve only the measured values, \hat{x}_k as \hat{a} and $\hat{b},$ then the shift or bias in the mean values due to the errors in the measured depths $x_k,$ Δa and $\Delta b,$ can be determined by expanding Eqs. (9) in terms of $\epsilon_k,$ $\Delta a,$ and $\Delta b.$ Thus

$$p_k = \hat{p}_k + \frac{\partial \hat{p}_k}{\partial a} \Delta a + \frac{\partial \hat{p}_k}{\partial b} \Delta b + \frac{\partial \hat{p}_k}{\partial x_k} \epsilon_k + \frac{\partial^2 \hat{p}_k}{\partial x_k^2} \epsilon_k^2 + O(\Delta a^2, \Delta b^2, \epsilon_k^3)\tag{11}$$

where $\hat{p}_k,$ etc. are evaluated at $\hat{a}, \hat{b},$ and $\hat{x}_k.$ The derivatives $\frac{\partial p_k}{\partial a}$ and $\frac{\partial p_k}{\partial b}$ are given by Eq. (8). The other derivatives are

$$\begin{aligned}\frac{\partial \hat{p}_k}{\partial x_k} &= -\hat{p}_k(1 - \hat{p}_k)\hat{b} \\ \frac{\partial^2 \hat{p}_k}{\partial x_k^2} &= -\frac{\partial \hat{p}_k}{\partial x_k}(1 - \hat{p}_k)\hat{b} + \hat{p}_k \frac{\partial \hat{p}_k}{\partial x_k} \hat{b} \\ &= \hat{p}_k(1 - 3\hat{p}_k + 2\hat{p}_k^2)\hat{b}^2\end{aligned}\tag{12}$$

It can be shown that if only first order terms in Δa , Δb , and ϵ_k are retained in the expansion of Eqs. (10), then Δa and Δb vanish. Thus Δa and Δb are $O(\epsilon_k^2)$. Substituting from Eq. (11) into Eq.(9), and using Eqs. (10) and retaining only terms $O(\epsilon_k^2)$, one can obtain equations for Δa and Δb . The values ϵ_k are not known, since they vary randomly. The average values of Δa and Δb can, however, be obtained in terms of the variance of ϵ_k , which is known from studies on NDE sizing errors. The final equations for the average values of Δa and Δb are

$$\begin{aligned} \left[\sum_{k=1}^K N_k \hat{p}_k (1 - \hat{p}_k) \right] \Delta a + \left[\sum_{k=1}^K N_k \hat{x}_k \hat{p}_k (1 - \hat{p}_k) \right] \Delta b &= \left[\sum_{k=1}^K N_k (\hat{p}_k + 2\hat{p}_k^2)(1 - \hat{p}_k) \hat{b}^2 \right] \sigma_{x_k}^2 \\ \left[\sum_{k=1}^K N_k \hat{x}_k \hat{p}_k (1 - \hat{p}_k) \right] \Delta a + \left[\sum_{k=1}^K N_k \hat{x}_k^2 \hat{p}_k (1 - \hat{p}_k) \right] \Delta b &= \left[\sum_{k=1}^K N_k x_k \hat{p}_k (1 + 2\hat{p}_k)(1 - \hat{p}_k) \hat{b}^2 - N_k \hat{p}_k (1 - \hat{p}_k) \hat{b} \right] \sigma_{x_k}^2 \end{aligned} \quad (13)$$

where $\sigma_{x_k}^2$ is the estimated variance of the errors in the measured depths. The variance $\sigma_{n_k}^2$ can be determined from comparisons of the NDE and destructive data. It will vary with the depth of the crack.

Eqs. (10) and (13) gives estimates of the mean values of a and b . To estimate the variance in a and b we note that variances in dependent variables like a and b are related to the variances of the independent variables n_k and x_k through the propagation of error equations

$$\begin{aligned} \sigma_a^2 &= \sum_{k=1}^K \left[\sigma_{n_k}^2 \left(\frac{\partial a}{\partial n_k} \right)^2 + \sigma_{x_k}^2 \left(\frac{\partial a}{\partial x_k} \right)^2 \right] \\ \sigma_b^2 &= \sum_{k=1}^K \left[\sigma_{n_k}^2 \left(\frac{\partial b}{\partial n_k} \right)^2 + \sigma_{x_k}^2 \left(\frac{\partial b}{\partial x_k} \right)^2 \right] \\ \sigma_{ab}^2 &= \sum_{k=1}^K \left[\sigma_{n_k}^2 \left(\frac{\partial a}{\partial n_k} \right) \left(\frac{\partial b}{\partial n_j} \right) + \sigma_{x_k}^2 \left(\frac{\partial a}{\partial x_k} \right) \left(\frac{\partial b}{\partial x_j} \right) \right] \end{aligned} \quad (14)$$

The variance $\sigma_{n_k}^2$ for a binomial process is

$$\sigma_{n_k}^2 = N_k p_k (1 - p_k).$$

The array $\begin{bmatrix} \sigma_a^2 & \sigma_{ab}^2 \\ \sigma_{ab}^2 & \sigma_b^2 \end{bmatrix}$ is generally referred to as the covariance matrix C .

The derivatives $\frac{\partial a}{\partial n_k}$, $\frac{\partial a}{\partial x_k}$, $\frac{\partial b}{\partial n_k}$, and $\frac{\partial b}{\partial x_k}$ can be obtained from Eq. (9). Differentiating Eqs. 9 with respect to n_j gives

$$\begin{aligned} 1 - \sum_{k=1}^K N_k \frac{\partial p_k}{\partial n_j} &= 0 \\ x_j - \sum_{k=1}^K N_k x_k \frac{\partial p_k}{\partial n_j} &= 0 \end{aligned} \quad (15)$$

Differentiating Eqs. 9 with respect to x_j gives

$$\sum_{k=1}^K N_k \frac{\partial p_k}{\partial x_j} = 0 \quad (16)$$

$$n_j - N_j p_j - \sum_{k=1}^K N_k x_k \frac{\partial p_k}{\partial x_j} = 0$$

The partial derivatives of p_k can be expressed in terms of the derivatives of a , b :

$$\frac{\partial p_k}{\partial n_j} = \frac{\partial p_k}{\partial a} \frac{\partial a}{\partial n_j} + \frac{\partial p_k}{\partial b} \frac{\partial b}{\partial n_j} \quad (a)$$

$$= -p_k(1-p_k) \frac{\partial a}{\partial n_j} - p_k(1-p_k) x_k \frac{\partial b}{\partial n_j} \quad (b)$$

$$\frac{\partial p_k}{\partial x_j} = \frac{\partial p_k}{\partial x} \frac{\partial x}{\partial x_j} + \frac{\partial p_k}{\partial a} \frac{\partial a}{\partial x_j} + \frac{\partial p_k}{\partial b} \frac{\partial b}{\partial x_j} \quad (c)$$

$$= -p_k(1-p_k) b \delta_{kj} - p_k(1-p_k) \frac{\partial a}{\partial x_j} - p_k(1-p_k) x_k \frac{\partial b}{\partial x_j} \quad (d)$$

Substituting Eq. 20b into Eqs. 18 gives

$$-\alpha_0 \frac{\partial a}{\partial n_j} - \alpha_1 \frac{\partial b}{\partial n_j} = 1 \quad (18)$$

$$-\alpha_1 \frac{\partial a}{\partial n_j} - \alpha_2 \frac{\partial b}{\partial n_j} = x_j$$

where

$$\alpha_0 = - \sum_{k=1}^K N_k p_k (1-p_k)$$

$$\alpha_1 = - \sum_{k=1}^K N_k p_k (1-p_k) x_k \quad (19)$$

$$\alpha_2 = - \sum_{k=1}^K N_k p_k (1-p_k) x_k^2$$

Eqs. 18 are easily solved for the partial derivatives of a , b with respect to n_j :

$$\frac{\partial b}{\partial n_j} = \frac{x_j - \frac{\alpha_1}{\alpha_0}}{\frac{\alpha_1^2}{\alpha_0} - \alpha_2} \quad (20)$$

$$\frac{\partial a}{\partial n_j} = \frac{-1}{\alpha_0} - \frac{\alpha_1}{\alpha_0} \frac{\partial b}{\partial n_j}$$

Similar expressions can be obtained for the partial derivatives of a, b with respect to x_j .

Defining

$$\begin{aligned}\eta(x) &= \ln\left(\frac{1-p}{p}\right) \\ &= a + bx\end{aligned}$$

The variance of η_j corresponding to the j^{th} crack is

$$\begin{aligned}\sigma_{\eta_j}^2 &= \sigma_a^2 \left(\frac{\partial \eta_j}{\partial a}\right)^2 + \sigma_b^2 \left(\frac{\partial \eta_j}{\partial b}\right)^2 + 2\sigma_{ab} \left(\frac{\partial \eta_j}{\partial a}\right) \left(\frac{\partial \eta_j}{\partial b}\right) \\ &= \sigma_a^2 + x_j^2 \sigma_b^2 + 2x_j \sigma_{ab}\end{aligned}$$

The confidence limits for p_j can be expressed in terms of σ_{η_j} :

$$p_j = \frac{1}{1 + e^{\eta_j \pm Z\sigma_{\eta_j}}},$$

where Z is a constant that depends on the confidence level desired.

2.5.3 Significance of Difference between Two POD Curves

There are a several ways to test whether two POD curves are the same. The test described below is the easiest to carry out, because it can be performed using only the logistic regression results. A logistic regression is run on two sets of data. Each regression fit has as a result a set of parameter estimates $u=(a,b)$ and an associated covariance matrix C . The two data sets are designated by letters α and β and the two regression fits are described by

$$p_{\alpha,i} = \text{logistic}(a_{\alpha,1} + b_{\alpha,2} x_{\alpha,i}) \quad (21)$$

$$p_{\beta,i} = \text{logistic}(a_{\beta,1} + b_{\beta,2} x_{\beta,i}) \quad (22)$$

The regression fits produce the estimates u_a and u_b , along with the covariance matrices C_a and C_b . To test whether $u_a = u_b$, one forms a chi-squared statistic:

$$\chi^2 = (u_\alpha - u_\beta)^T [C_\alpha + C_\beta]^{-1} (u_\alpha - u_\beta) \quad (23)$$

and compares χ^2 to a critical value obtained from a chi-squared table. The degree of freedom associated with the critical value equals the number of model parameters; in this case, two. The two sets of parameters are equal when χ^2 is less than the critical value. For example, to conduct the test at a 10% level of significance, the critical value would be 4.61.

A chi-squared table can also be used to assign a p-value to the statistic χ^2 . When performing this test, a less stringent level of significance than typical can be used, such as 10% or 20% instead of the typical 5%. This approach has been used to determine if POD curves by different teams using the same data are different by chance or if the difference is significant.

2.6 Results of Analysis Round-Robin

The lack of reliability in estimating the maximum depth of an SCC with either voltage or phase angle from bobbin coil data, a well known problem in field inspections, can be illustrated for the mock-up with results from the RR. Figure 2.63 shows the relationship of BC voltage and maximum depth (determined from the multiparameter algorithm) for LODSCC and LIDSCC. While very high voltages (>10 V) indicate deep flaws (>80%TW), lower amplitudes do not correlate with depth. The results for TSP and freespan are similar. Figure 2.64 shows the relationship of BC phase angle to maximum depth of LODSCC at the TSP. For LODSCC, ideally the phase angle should increase monotonically from 40° as the depth increases. The scatter indicates the difficulty in using BC phase angle to estimate depth. Figure 2.65 shows a similar result for LIDSCC at the TSP. For LIDSCC, the phase should increase from 0 to 40° as the depth increases from 0 to 100%TW.

2.6.1 POD Logistic Fits with 95% Lower Confidence Bounds

An analysis of bobbin coil voltages reported for LODSCC at tube support plates by teams analyzing the mock-up data has been carried out. In most cases, voltage variations identified by the teams were fairly small. For each LODSCC, an average BC voltage and a corresponding standard deviation were computed. The cumulative distribution of the normalized standard deviations (i.e., the standard deviation divided by the corresponding value of the average voltage) can be fit well by a Weibull distribution (the RMS difference between the observed distribution and the Weibull fit is <0.03). The fitted distribution is shown in Figure 2.66. For almost 90% of the indications, the normalized standard deviation in the reported voltages is < 0.15. This result is consistent with Generic letter 95-05 which assumes a 15 percent cutoff for the voltage response variability distribution is acceptable. The indications with larger variations are not associated with particularly high or low voltages (i.e., approximately half the signals with standard deviations of >0.1 have voltages of >2), but rather are associated with the complexity of the signal and the difficulty in identifying the peak voltage.

2.6.1.1 Bobbin Coil Results

The reference table shows the flaw parameters, max depth, m_p , average depth, and for circumferential cracks the crack area and the observed POD. The flaw characterization parameters were determined from the profiles generated by the multiparameter algorithm. The results reported here are derived from the bobbin coil reports of resolution analysts from the eleven teams participating in the RR. Figures are shown for tube support plate and freespan flaws. Analysts are given credit for calling a flaw if their reported flaw location is within 25 mm (1 in.) of the ends of the flaw. The analyst's estimate of depth was not a factor in calculating POD.

Figure 2.67 shows the maximum likelihood logistic fit for POD for LODSCC and LIDSCC at the TSP as a function of maximum depth (as determined from the multiparameter algorithm). The NDE uncertainty in depth is included in the one-sided 95% lower confidence limit (OSL). In general, the curves have a reasonable shape, providing plausible PODs. As expected, the POD for ID cracks is higher than for OD cracks (99% with 98%OSL at 60%TW vs. 75% with 65%OSL at 60% TW). Figure 2.68 shows raw data and the logistic fit curve for the BC POD for one of the RR teams. As can be seen, the probability of a hit is very high for the deepest flaws, which are dominant in this set of cracks.

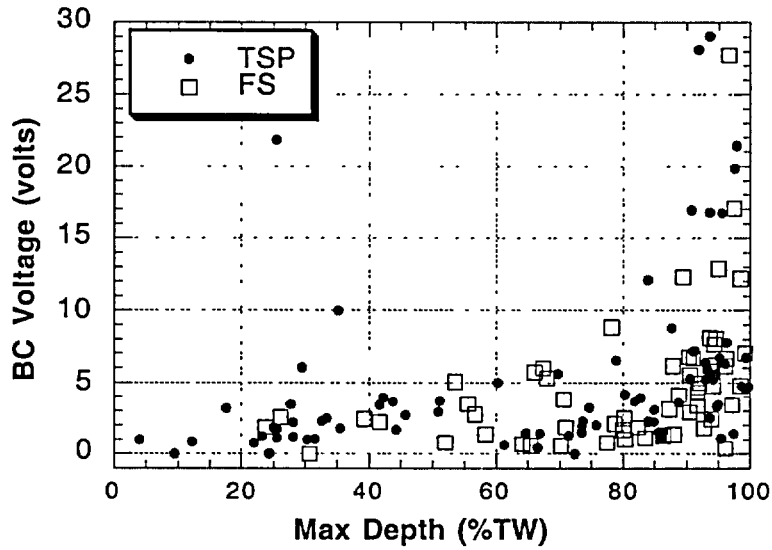


Figure 2.63
Relationship of BC voltage to maximum depth for LODSCC and LIDSCC. Depths are determined with the multiparameter algorithm.

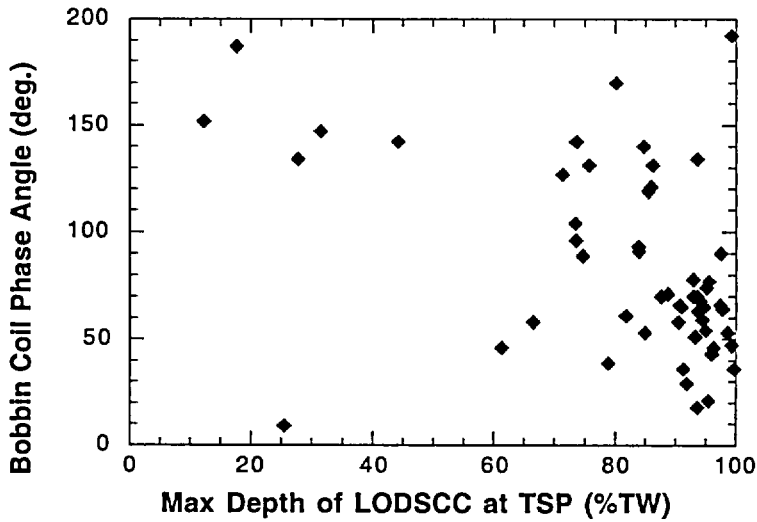


Figure 2.64
Relationship of BC phase angle to maximum depth of LODSCC at the TSP. Depths are determined with the multiparameter algorithm.

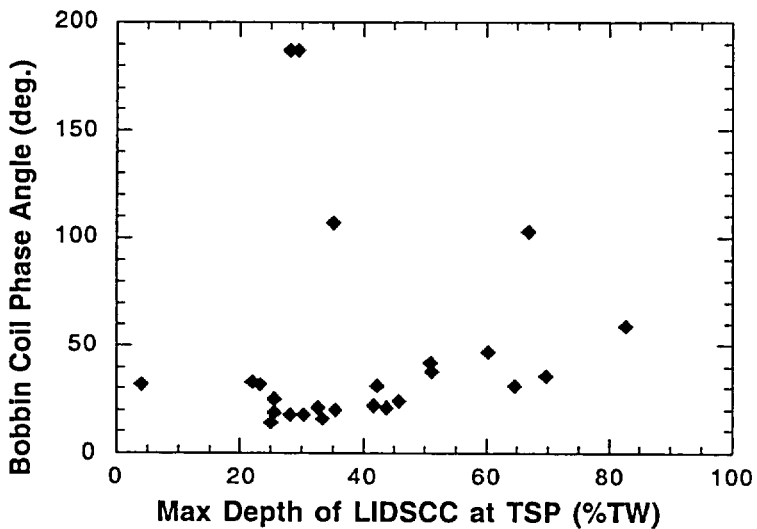


Figure 2.65
Relationship of BC phase angle to maximum depth of LIDSCC at the TSP. Depths are determined with the multiparameter algorithm.

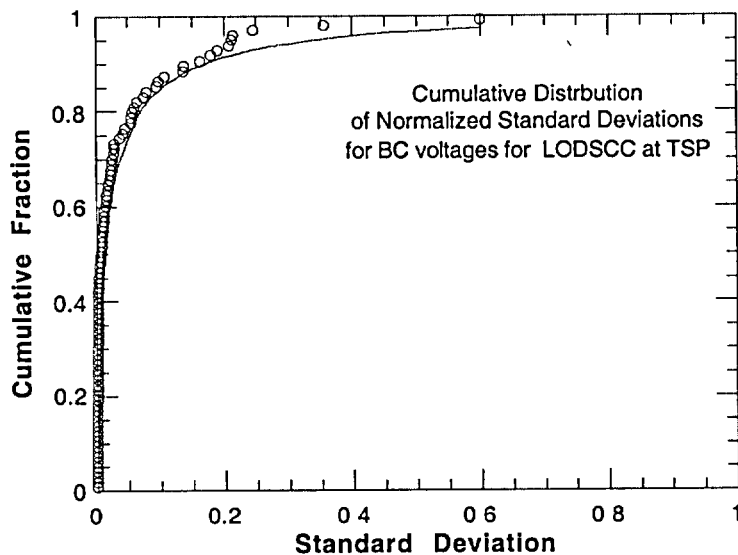


Figure 2.66
Cumulative distribution of normalized standard deviations for bobbin coil voltages for LODSCC at tube support plates

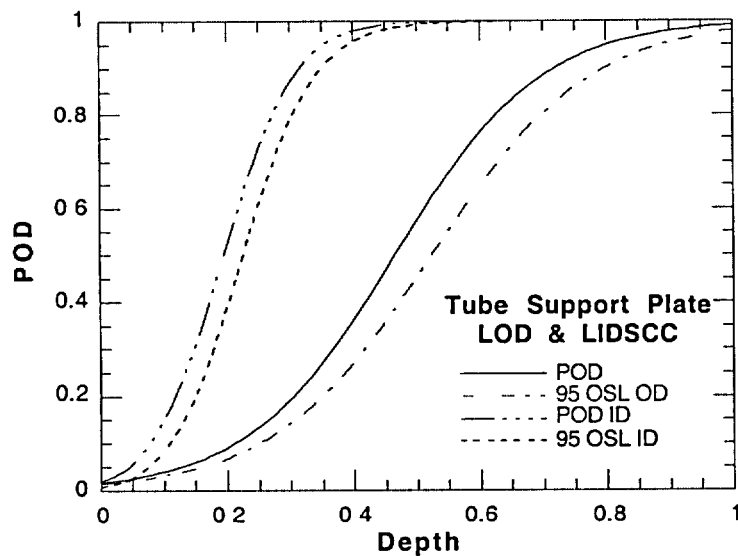


Figure 2.67
BC POD for TSP data as a function of maximum depth (as fraction throughwall) for LODSCC and LIDSCC using maximum likelihood fit with the one-sided 95% confidence limit. Maximum depth uncertainty is included in the OSL. Depths are determined with the multiparameter algorithm.

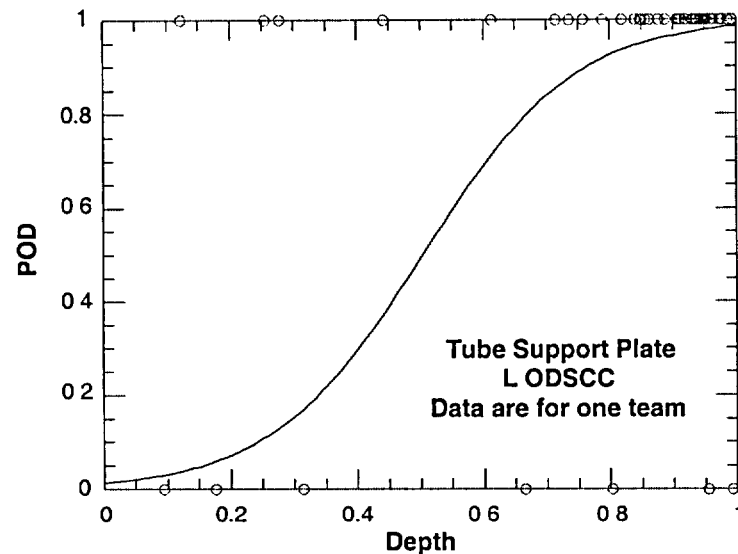


Figure 2.68
BC POD for TSP data as a function of maximum depth (as fraction through-wall) for LODSCC using maximum likelihood fit (solid line). The logistic fit is to data from one team only. The circles show the raw data from which the curve is generated. Depths are determined with the multiparameter algorithm.

Figure 2.69 compares the POD results (with OSL) for the TSP cracks with the results for freespan cracks. While as expected the POD for freespan LODSCC (95% at 60% TW) is higher than the POD for TSP LODSCC (75% at 60% TW), it is lower than the POD for TSP LIDSCC (99% at 60% TW). Figure 2.70 shows the result when combining freespan and TSP data.

Figure 2.71 (for TSP and freespan combined) compares the logistic fit when depths are estimated by ANL's multiparameter algorithm against the fit when the +Point maximum depth estimates are used. Use of the +Point data results in a more conservative POD curve. Figure 2.72 compares the maximum depth estimates from the multiparameter algorithm with the maximum depth from the +Point data for a variety of flaws. This type of variation is the cause for the variation in the logistic fits to the POD data shown in Figure 2.71

In addition to examining the RR data as a function of flaw depth, the POD has been evaluated as a function of BC voltage for TSP SCC. The results are shown in Figure 2.73. A pattern similar to that found for POD versus depth is observed for the POD vs. TSP bobbin coil voltage. In this figure, the percentage of correctly calling a flaw is plotted against binned data as indicated in the graph. Figure 2.74 shows the logistic fits to the POD vs. voltage data for LODSCC and LIDSCC, along with the 95% one-sided confidence limits. In contrast to case when the POD is considered as a function of depth, when the POD is considered as a function of voltage, the POD curve for LIDSCC at the TSP is lower than that for LODSCC. The lower POD curve for LIDSCC vs. POD for LODSCC, when POD is plotted against voltage, is possibly the result of missing shallow cracks that are in dents with high voltages.

The results were analyzed by the teams to determine whether there were strong team-to-team variations in the POD. For this exercise, all teams were given optical disks containing the same data sets to analyze. All analysts were given the same instructions and documents related to analyzing the data. Team-to-team variations are the result of variations in analyst interpretation of the same signals. The results as a function of team for freespan and TSP LODSCC combined are shown in Figure 2.75. The performance of most of the teams cluster rather tightly, although there is a significant variation between best and worst. Figure 2.76 shows team-by-team variation for freespan LODSCC alone. Figure 2.77 shows team-by-team variation for TSP LIDSCC alone. The high solid line represents the best team, while the symbols and dashed lines represent the remaining teams.

Based on the procedure discussed in 2.5.2, the probability that team-to-team variations in logistic fits to data are due to chance can be estimated. For LIDSCC at the TSP, the variation from best to worst (Figure 2.77) is very significant. There is <0.1% probability that the difference is due to chance (DTC). For FS OD, the variation from best to worst (Figure 2.76) is probably significant (DTC is <20%). For TSP OD, the variation from best to worst DTC is >60% and thus is probably not significant.

Figure 2.78 shows the logistic fits for POD for LODSCC at the TSP as a function of m_p . Figure 2.79 shows the corresponding results for LIDSCC at the TSP. Figure 2.80 shows the logistic fits for POD for axial SCC in freespan test sections as a function of m_p . The errors in calculating m_p by using the NDE characterization of the crack geometry compared to using fractography data have been determined with the 23-tube set (Tables 2.2 and 2.3 and Figure 2.46). Because only one value of m_p per crack is obtained, there is less data than in case of depth (multiple points per crack), and hence estimates of m_p have greater uncertainty. In all three graphs, the 95% one-sided lower confidence limit includes the error due to the use of NDE data to calculate m_p , as well as the statistical uncertainties associated with finite samples. In the TSP and FS regions, the POD for cracks that would fail or leak under $3\Delta p$ internal pressure (corresponding to $m_p \approx 2.3$) is >95%, even when depth uncertainties are accounted for.

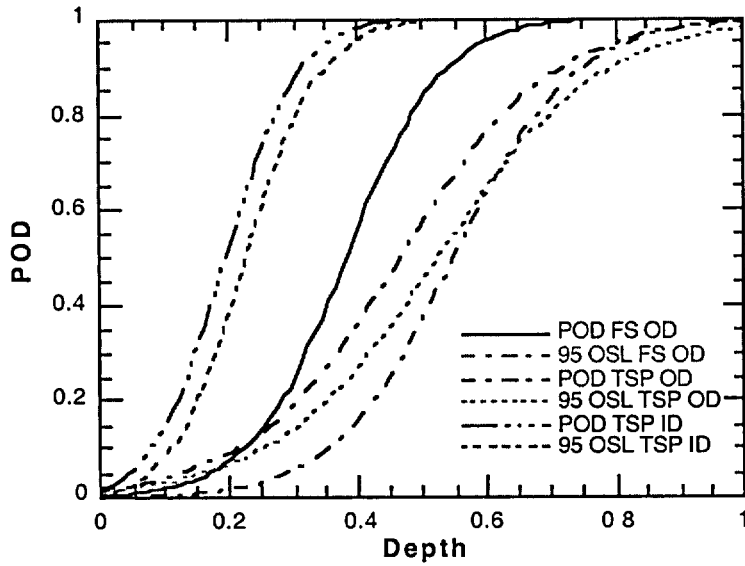


Figure 2.69
 BC POD for freespan and TSP data as a function of maximum depth (as fraction throughwall) for LODSCC and LIDSCC by using maximum likelihood fit with the one-sided 95% confidence limit. Maximum depth uncertainty is included. Depths are determined with the multiparameter algorithm.

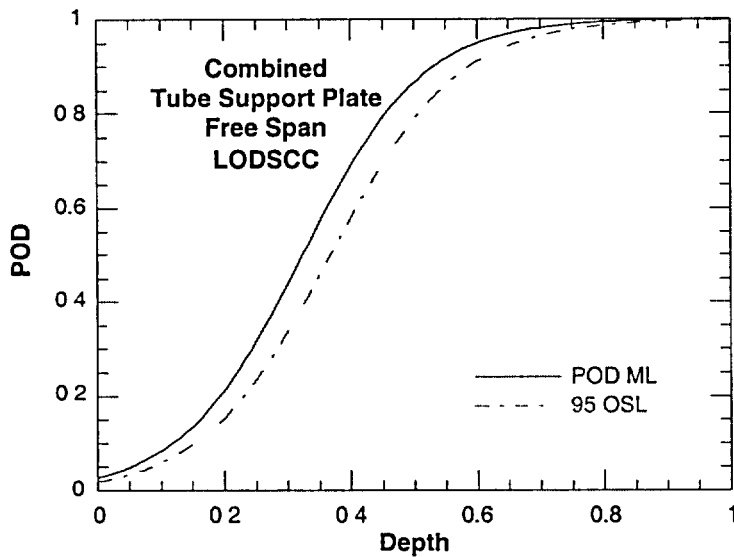


Figure 2.70
 Logistic fit to BC POD as a function of maximum depth (as fraction through-wall) when combining freespan and TSP data (solid line). The one-sided 95% confidence limit (dotted line) includes the uncertainty in depth. Depths are determined with the multiparameter algorithm.

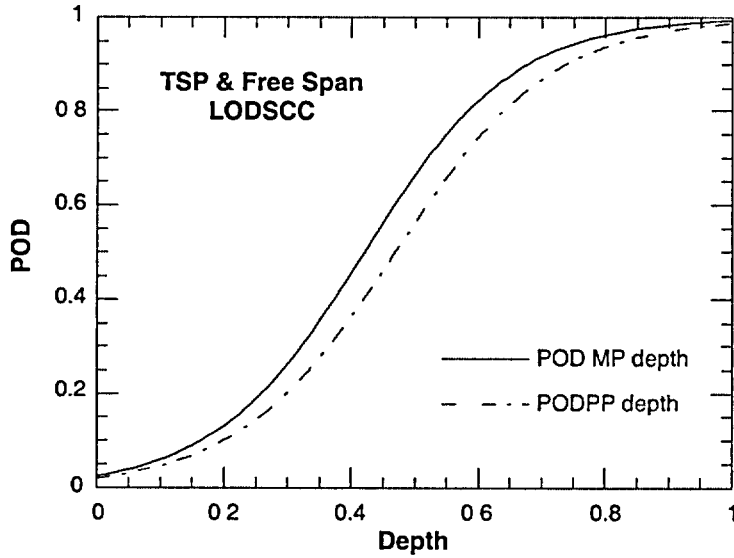


Figure 2.71
Comparison of the BC POD for TSP and freespan LODSCC when depths (as fraction throughwall) are estimated by multiparameter algorithm (MP) with the POD based on +Point maximum depth estimates (PP).

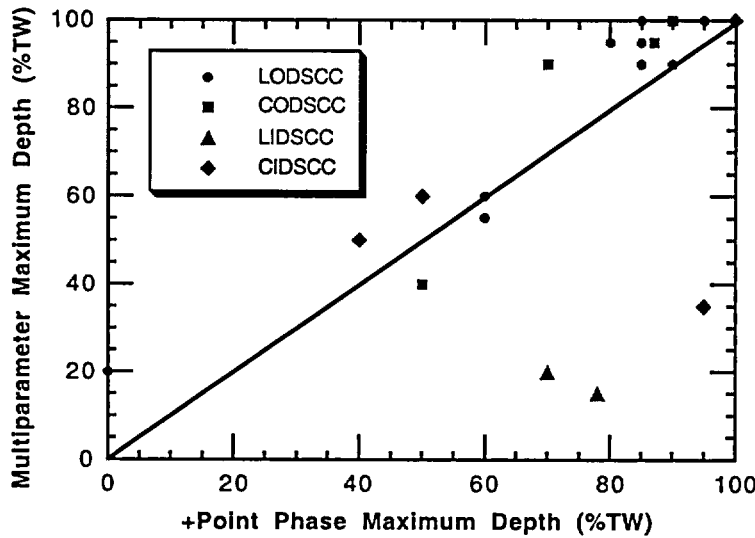


Figure 2.72
Maximum crack depth as determined by the multiparameter algorithm vs. the maximum crack depth as determined by phase analysis of +Point data at 300 kHz. Data are sorted by type of SCC.

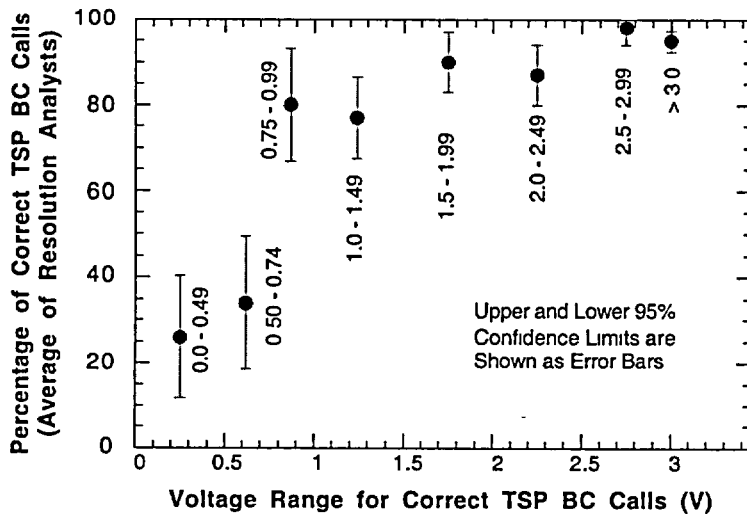


Figure 2.73
Round-robin TSP bobbin coil resolution analysts' results as a function of BC voltage. The BC POD has been evaluated for LODSCC at the TSP. Depths are determined with the multiparameter algorithm.

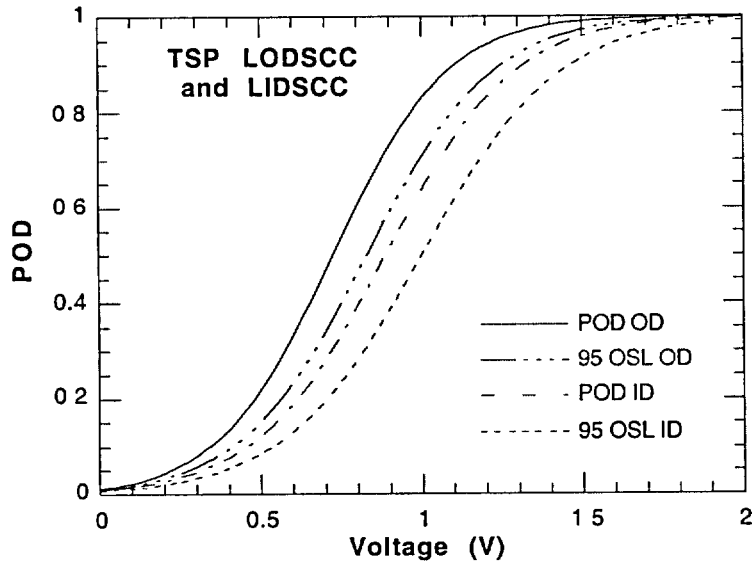


Figure 2.74
Logistic fit curves for TSP BC POD as a function of voltage for LODSCC and LIDSCC.

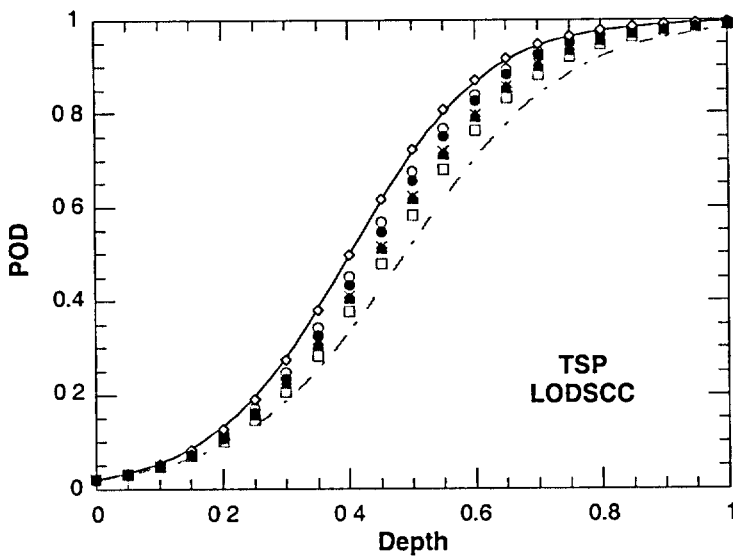


Figure 2.75
TSP LODSCC BC POD by team. The maximum crack depth (as fraction of wall) was determined by the multiparameter algorithm. The highest solid line represents the best team, the lowest dashed line represents the worst team, and the other symbols represent the remaining teams.

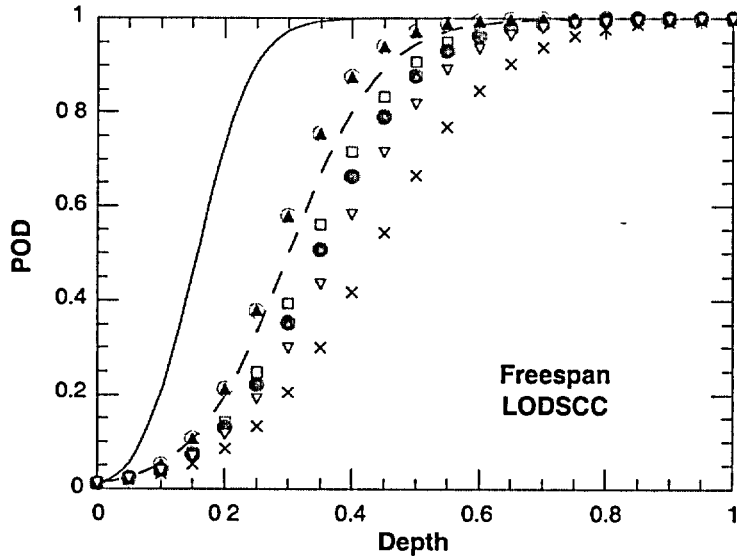


Figure 2.76
BC POD by team for freespan LODSCC. The maximum crack depth (as fraction of wall) was determined by the multiparameter algorithm. The solid line represents the best team, while the symbols and dashed line represent the remaining teams.

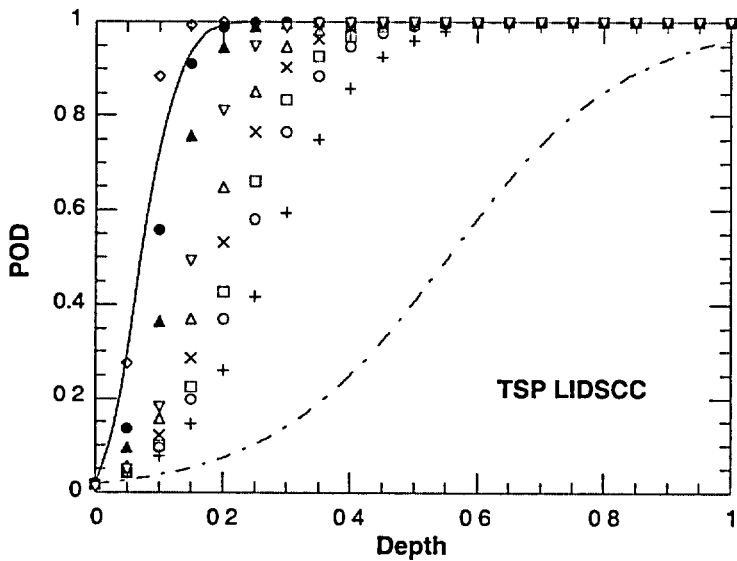


Figure 2.77
BC POD by team for TSP LIDSCC. The maximum crack depth (as fraction of wall) was determined by the multiparameter algorithm. The solid line represents the best team, the dashed line represents the worst team, and the symbols represent the remaining teams.

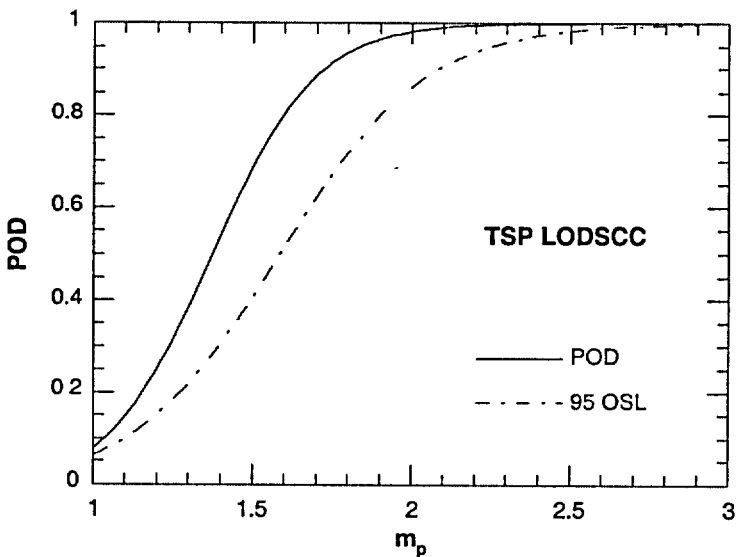


Figure 2.78
BC POD for TSP LODSCC as a function of m_p by using maximum likelihood fit with an estimate of the one-sided 95% confidence limit. The values of m_p are derived by using depths from the multiparameter algorithm.

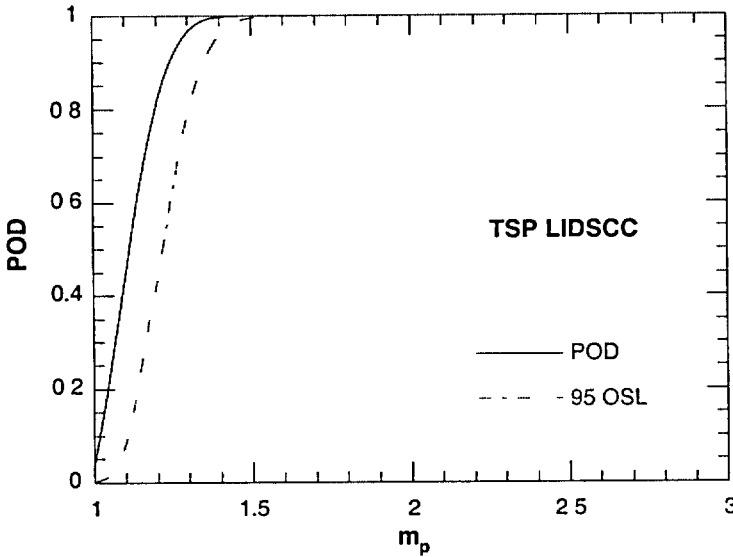


Figure 2.79
BC POD for TSP LIDSCC as a function of m_p by using maximum likelihood fit with an estimate of the one-sided 95% confidence limit. The values of m_p are derived by using depths from the multiparameter algorithm.

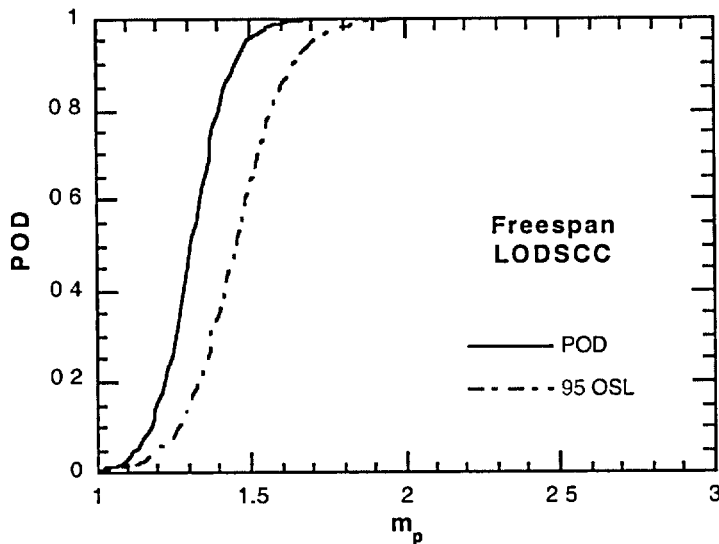


Figure 2.80
BC POD for freespan data for LODSCC as a function of m_p by using maximum likelihood fit with an estimate of the one-sided 95% confidence limit. The values of m_p are derived by using depths from the multiparameter algorithm.

2.6.1.2 MRPC Tube Sheet Results

An evaluation has been conducted of the adequacy of detecting SCC in the tube sheet level of the mock-up with an MRPC. The maximum depths are from multiparameter analysis of the MRPC data. Table 2.12 presents results from four test sections to show the general format for tabulating the results. Each flaw is indicated by row, column, and level (A for tube sheet). The three-letter code and flaw type is recorded along with the estimated depth. The teams participating (11 for tube sheet analysis) are numbered 1, 2, ... If the analyst recognizes that a crack is present within 25 mm (1 in.) of the correct location, a "1" is recorded in the column corresponding to the analyst/team, otherwise a "0" is recorded. Figure 2.81 shows the resolution analysts, 11-team average for MRPC POD as a function of maximum depth for combined axial and circumferential, ID, and OD SCC in the tube sheet. A maximum likelihood fit is used with an estimate of the one-sided 95% confidence limit (OSL) that includes the uncertainty in maximum depth. The false call rate for the tube sheet was 6%. The POD at 60% TW is $\approx 80\%$ with an OSL of 60%. Figure 2.82 shows the TS MRPC POD as a function of maximum depth for LIDSCC and CIDSCC combined and LODSCC and CODSCC combined. The POD for IDSCC is higher than for ODSCC, as expected. The POD for IDSCC is $\approx 90\%$ with an OSL of $\approx 75\%$. Figure 2.83 shows the POD

as a function of maximum depth for axial and circumferential SCC in the tube separated into a POD curve for all TS SCC, a curve for LIDSCC only, and a curve for LIDSCC combined with CIDSCC. The highest POD curve is for LIDSCC where the POD at 60% TW is 95%. Figure 2.84 shows MRPC POD by team as a function of maximum depth (as estimated by the multiparameter algorithm) for axial and circumferential, IDSCC, and ODSCC in the tube sheet. The POD at 60%TW ranges from 90% to 70%. Based on the discussion in Section 2.5.1, the probability that team-to-team variations in logistic fits to data are due to chance can be estimated.

Figure 2.85 compares MRPC POD as a function of maximum depth for all SCC in the tube sheet with that for the combined freespan and tube support plate SCC BC POD. The MRPC POD for TS SCC is slightly lower for the deeper flaws (0.87 vs. 0.92). This result is reasonable in view of the difficulty the roll transition presents for flaw detection in the tube sheet.

The logistic fits to the data depend, as previously discussed, on the estimates of crack depth. Figure 2.86 compares differences in logistic fits to the tube sheet POD data when the depths from the multiparameter algorithm and those from +Point phase analysis at 300 kHz are used. The difference is significant. The logistic curve fit to the data using maximum likelihood is higher for the depths estimated by the multiparameter algorithm.

Comparisons are made between the tube sheet BC POD and tube sheet MRPC POD in Figures 2.87-2.89. Figure 2.87 shows, for all SCC, a higher POD curve for the MRPC (80% vs. 40% at 60% TW).

Table 2.12 Format for tabulating MRPC TS results (11 teams analyzed MRPC data from the tube sheet).

Flaw ID	MRPC Location	Three Letter Code	Flaw Type	Depth %TW	Depth									
					1	2	3	4	5	6	7	8	9	
H21A	14314	MAI	LOD	51	0	1	1	1	1	1	0	1	1	1
N18A	20550	MCI	COD	85	1	1	1	1	1	1	1	1	1	1
N08A	20286	MAI	LID	87	1	1	1	1	1	1	1	1	0	1
K24A	21870	MMI	LOD	90	1	1	0	1	0	1	1	1	0	1

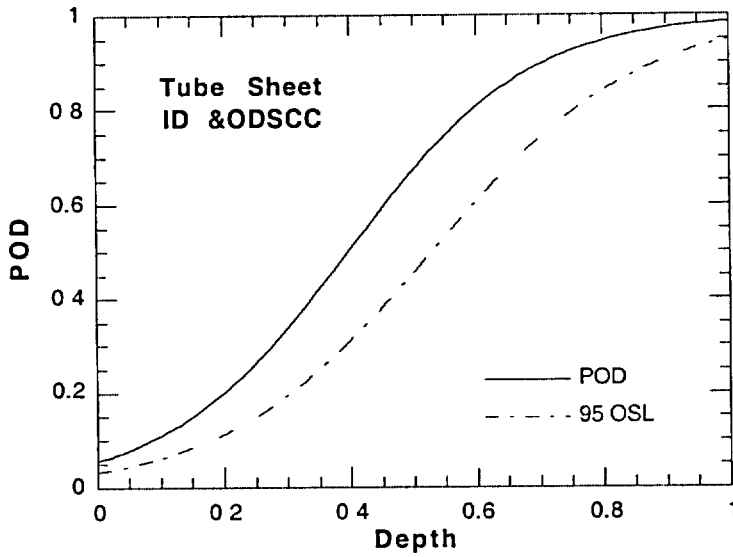


Figure 2.81
MRPC POD as a function of maximum depth (as fraction of wall) for combined axial and circumferential, IDSCC, and ODSCC in the tube sheet. ID and OD combined should not be used except for comparison of relative effectiveness of probes and teams.

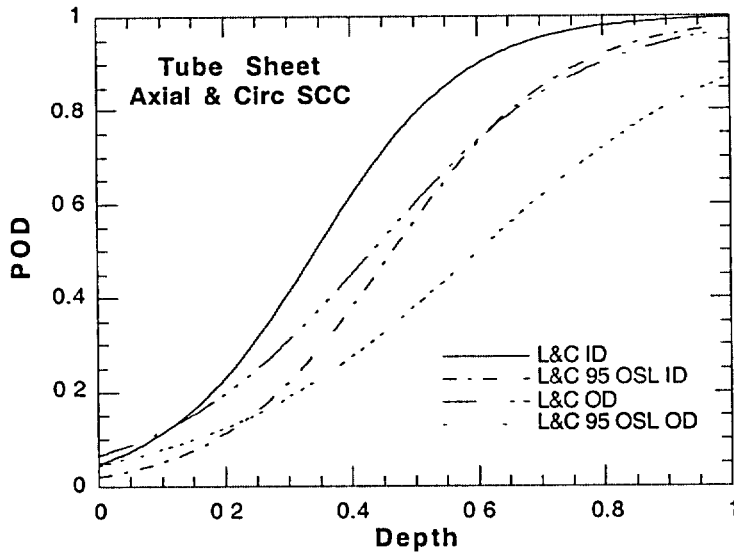


Figure 2.82
TS MRPC POD as a function of maximum depth (as fraction of wall) for LIDSCC and CIDSCC combined and LODSCC and CODSCC combined. Maximum likelihood fit is used with an estimate of the one-sided 95% confidence limit that includes uncertainty in maximum depth. Depths are determined with the multiparameter algorithm.

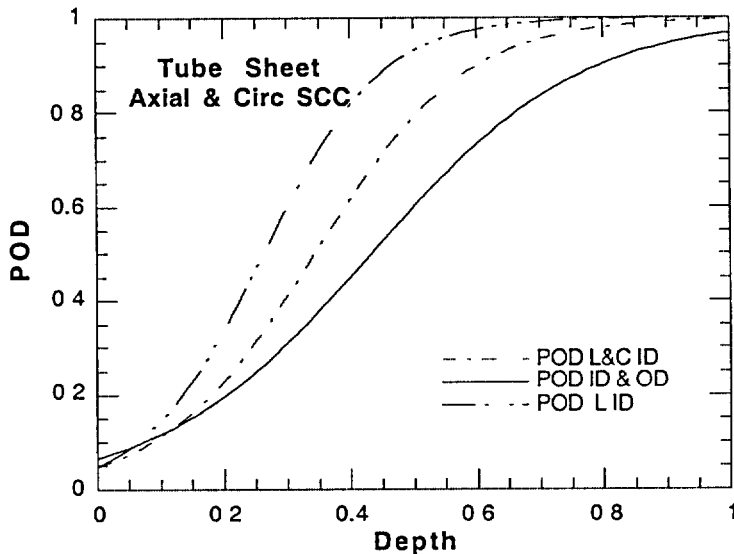


Figure 2.83
MRPC POD as a function of maximum depth (as fraction of wall) for axial and circumferential, IDSCC, and ODSCC in the tube sheet. The upper dashed line is for all-LIDSCC only, the lower dashed line is for LIDSCC and CIDSCC. Depths are determined with the multiparameter algorithm. ID and OD combined should not be used except for comparison of relative effectiveness of probes and teams.

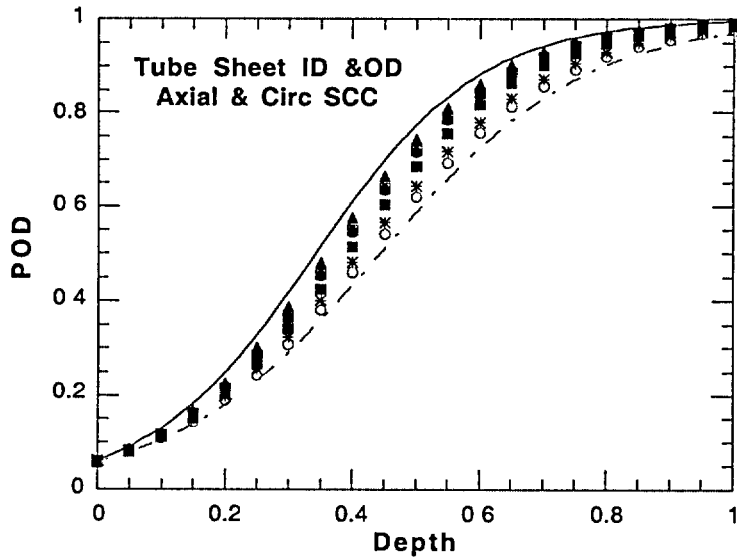


Figure 2.84
MRPC POD by team as a function of maximum depth (as fraction of wall) for axial and circumferential, IDSCC, and ODSCC in the tube sheet. Maximum depth is estimated by the multiparameter algorithm. The solid line represents the best team, the dashed line represents the worst team, and the symbols represent the remaining teams.

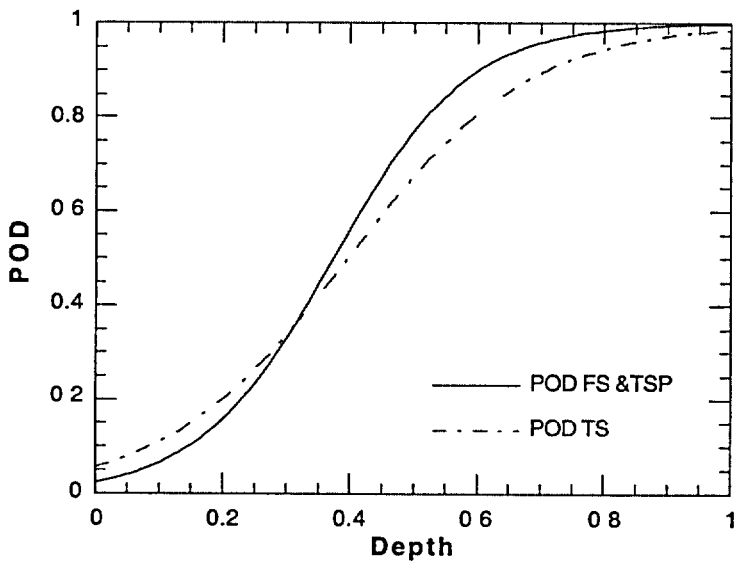


Figure 2.85
Comparison of the PODs as a function of maximum depth (as fraction of wall) for all axial and circumferential SCC in the tube sheet (MRPC results) with that for the combined freespan and tube support plate (BC results). Depths are determined with the multiparameter algorithm. ID and OD combined should not be used except for comparison of relative effectiveness of probes.

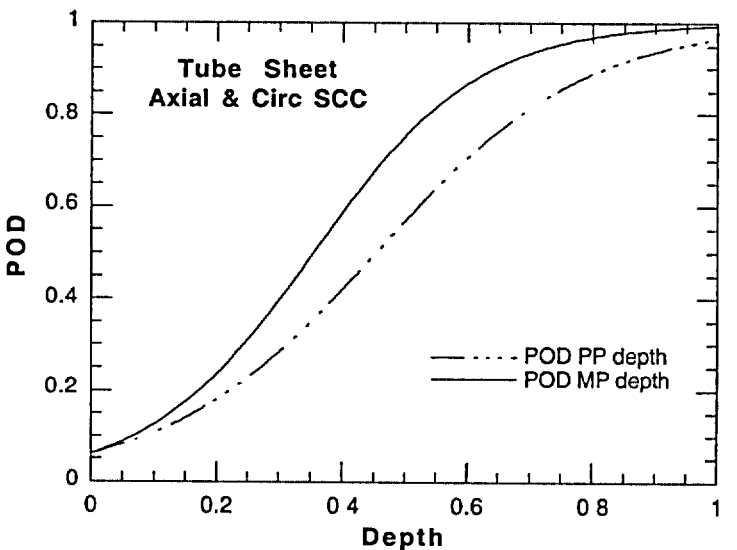


Figure 2.86
Comparison of the MRPC POD as a function of maximum depth (as fraction of wall) for all SCC in the tube sheet based on depths estimated by conventional phase analysis with a +Point™ probe (PP) and depths estimated by the multiparameter method (MP). ID and OD combined should not be used except for comparison of relative effectiveness of probes and teams.

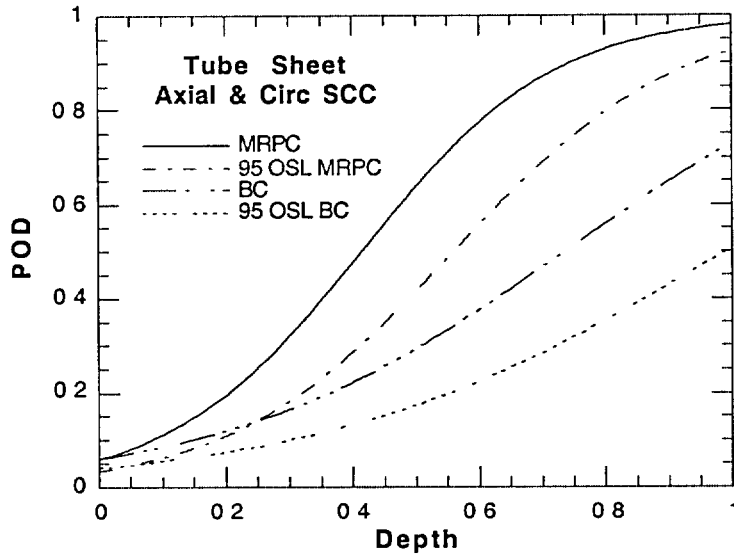


Figure 2.87
Comparison of BC and MRPC POD for tube sheet axial and circumferential IDSCC and ODSCC. The lower 95% one-sided confidence limits (OSL) are shown (includes uncertainties in depths). Depths (as fraction of wall) are determined with the multiparameter algorithm. ID and OD combined should not be used except for comparison of relative effectiveness of probes and teams.

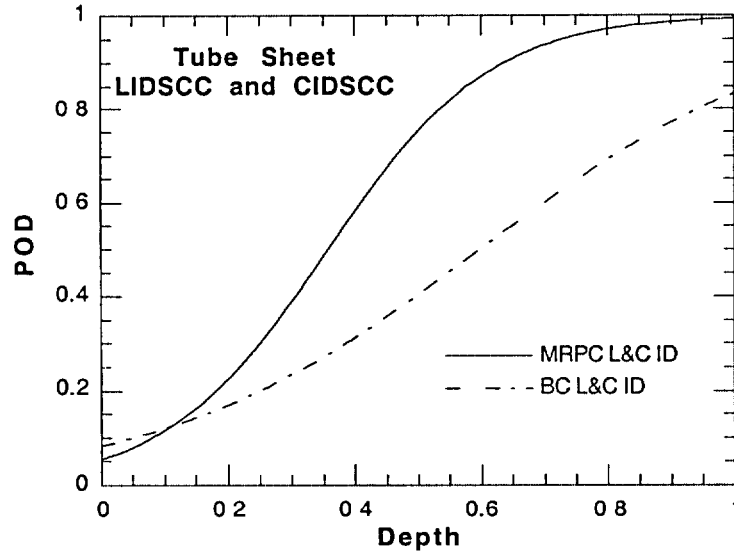


Figure 2.88
Comparison of BC and MRPC POD for tube sheet CIDSCC and LIDSCC. Depths are determined with the multiparameter algorithm.

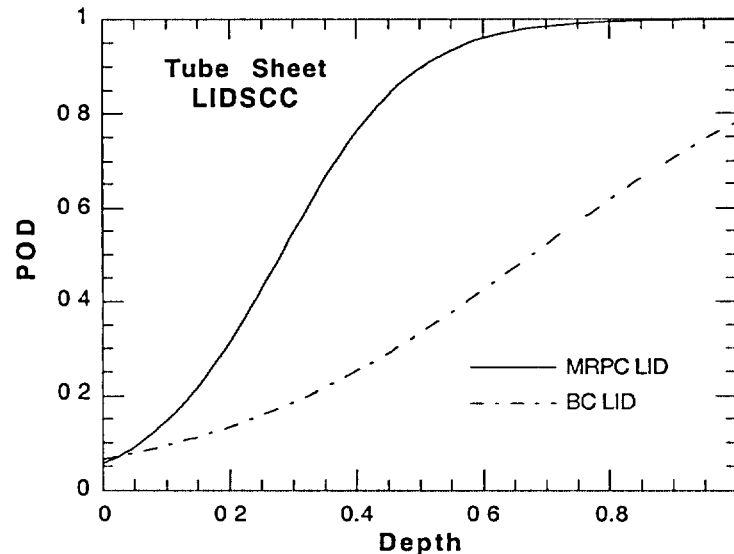


Figure 2.89
Comparison of BC and MRPC POD for tube sheet LIDSCC. Depths (as fraction of wall) are determined with the multiparameter algorithm.

Figure 2.88 compares BC and MRPC PODs for tube sheet LIDSCC and CIDSCC with the MRPC curve substantially higher. Figure 2.89 compares BC and MRPC POD for tube sheet LIDSCC only. The MRPC POD at 60% TW is 95%, while the BC POD is only 40%.

2.6.1.3 MRPC Special Interest Results

A review of MRPC results for TSP LODSCC BC voltages between 2.0 and 5.6 was carried out. Such calls are normally reviewed to confirm or dismiss the BC call. There are 17 TSP LODSCC flaws with BC voltages in the range 2.0 to 5.6 and maximum depths estimated to be > 70% TW (by multiparameter algorithm). The average correct call using the MRPC data for this set of cracks is 98% (with a 96% lower 95% confidence limit). One other LODSCC in the TSP with BC voltage in the 2.0–5.6 volts range had an estimated maximum depth of 28% TW. None of the teams called this flaw with the MRPC data.

The possibility of a crack with a high BC voltage being missed by the subsequent MRPC data analysis could arise when a flaw is shallow and long, shallow and volumetric in nature, or deep and short. An example is shown in Figure 2.90. The crack profile in this case is generated from mock-up data with the multiparameter algorithm. An axial TSP LODSCC with maximum depth of 99%TW was missed by teams analyzing MRPC data. In this case, the MRPC +Point voltage at 300 kHz was only ≈ 0.2 V. The largest part of the segmented crack has a length of about 10 mm. The lower part of the figure shows the crack along the test section axis. The m_p for this flaw is ≈ 4.5 , indicating that the tube would leak at pressures well below $3\Delta p$. The BC voltage for this crack can, depending on analyst, vary from 4.5 to 8. The dye penetrant image of the crack intersection with the tube OD is consistent with the isometric image generated by the multiparameter algorithm.

These results suggest that flaws detected correctly by bobbin coil could subsequently be dismissed upon further examination of MRPC data even when flaws are relatively deep. The MRPC probes are very effective in characterizing defects, compared to bobbin coils, but may be less effective than bobbin coils in recognizing that a crack is present.

2.7 Nature of Missed Flaws

The primary cause of missing a flaw is that the flaw signal is distorted by geometry or deposits and the flaw signal is no longer recognized. A tight crack that does not generate a significant EC signal is another cause for missing a flaw. Another possibility is that the signal from an EC coil does not conform to what is expected (i.e., the signal could be out of the flaw plane or could be generated by multiple cracks). Very long flaws may be missed because the analysts may concentrate on just a small portion of the flaw, thereby missing the overall response. Confusion could also arise from conflicting behavior of two or more coils. For example, there could be a clear bobbin coil signal but nothing reportable from an MRPC. Analysts have a preconceived idea of what flaw responses at various locations should be like and might not pursue anomalous indications that are actually from a flaw. A few cracks in the mock-up have been called by the bobbin coil and dismissed following an MRPC analysis. Some cracks detectable with an MRPC are not detected by the bobbin coil. The reasons vary as described above but in the case where there is a crack and a bobbin coil indication, the crack is not called because the indication has a very high phase angle or is out of the flaw plane.

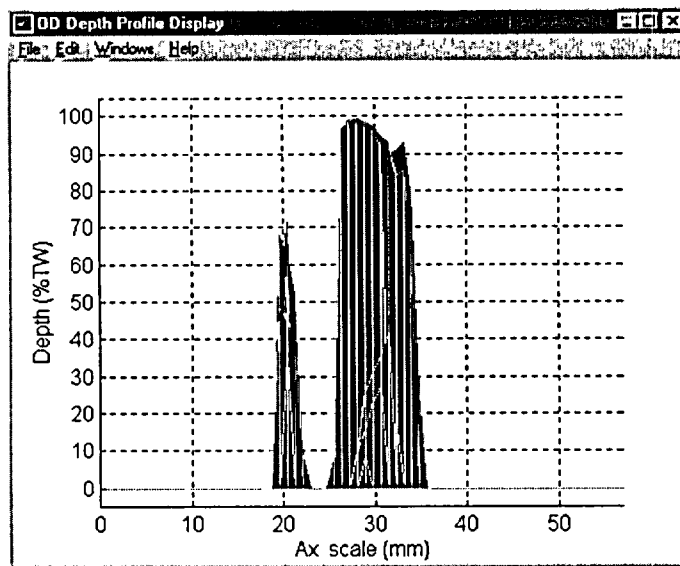
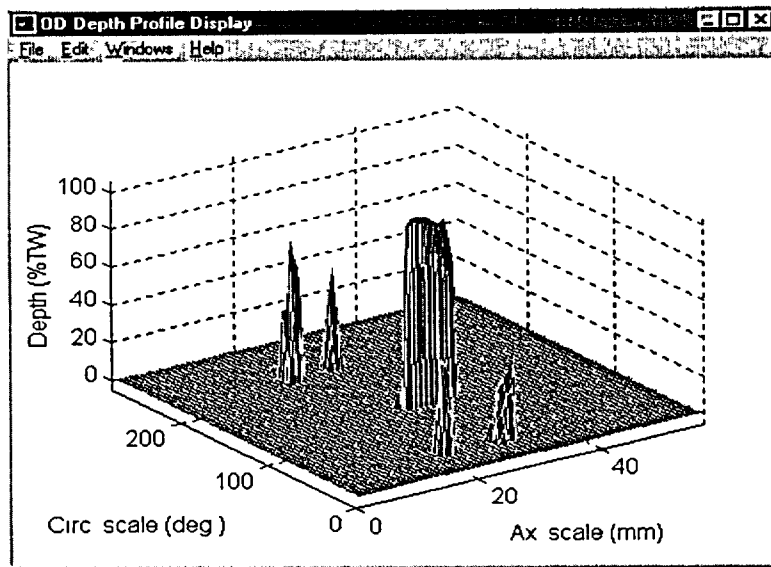


Figure 2.90

TSP LODSCC with maximum depth of 99%TW that was missed by teams analyzing MRPC data. The largest piece of the segmented crack has a length of about 10 mm. The lower part of the figure shows the crack along the test section axis.

2.8 Nature of Overcalls

Overcalls are the result of signals from certain coils that tend to generate flaw-like signals from geometrical distortions and deposits. Overcalls could also be the result of confusion from conflicting behavior of two or more coils. In a round-robin exercise, there is a tendency to make calls that might not be made under field conditions because there is no penalty for overcalling as long as the overcalling is not abused. In fact, the reports from resolution analysts show a reasonably low overcalling rate for the freespan (0.1%) and TSP (1.7%). The overcalling in the tube sheet level is significantly higher (6%). The complex nature of the roll transition is probably the root cause of the tube sheet overcalling, although upon further review and destructive analysis, it is possible that unintentional flaws may have been introduced to the tube sheet level during tube expansion, flaw fabrication, and assembly.

3 Summary

The mock-up has been shown to have flaws similar to those in operating steam generators, and the round-robin (RR) exercise has successfully mimicked an in-service inspection from preparation of documentation, to collection of bobbin coil and motorized rotating pancake coil (BC and MRPC) data to analysis of the data by qualified teams. Eleven teams have participated in the steam generator RR exercise. The resolution analysts' reports have been used to provide estimates of probability of detection (POD) for some flaw morphologies. The feasibility of determining the reference state, that is, estimating the maximum depth, average depth, area, and m_p from the eddy current profile of mock-up flaws has been validated through fractography of laboratory samples containing cracks with various morphologies similar to those in the mock-up. Nevertheless, for the final analysis, the "true" size of some flaws will be determined through destructive examination (NDE). The current NDE study validation effort has led to POD estimates for axial and circumferential inner and outer diameter stress corrosion cracking (ID and OD SCC), shallow to deep. For the flaws analyzed, the mock-up POD is generally high for the deeper freespan and tube support plate (TSP) SCC. However, as noted previously, noise levels in the mock-up are generally less than can be found in field data. Noise as severe as that in the U-bends of plants such as Indian Point 2 was not present in the mock-up freespan and TSP levels.

The possibility of a flaw being detected by BC and dismissed as a flaw by further MRPC evaluations has been demonstrated in this exercise. This situation can occur even when flaws are relatively deep. The MRPC probes are more effective in characterizing defects than are BCs, but the results of the RR exercise do not show any improvement in POD by supplemental rotating probe examinations when following "I" code calls made with the bobbin coil. This is logical because the POD for bobbin calls requiring a supplemental MRPC analysis is simply the probability determined from the two PODs, both of which are less than 1. The combined POD (BC followed by MRPC) = (POD BC) x (POD supplemental MRPC). The flaws missed by the BC examination are not reviewed by an MRPC. Because some of the flaws correctly called by the bobbin coil are now going to be incorrectly dismissed by the MRPC examination, the combined POD is less than the BC POD alone. Note that for the tube sheet where all test sections were examined by MRPC and BC, the MRPC POD is higher than the BC POD (see Figs. 2.87-2.89) Also, signals from geometry in the tube sheet area can lead to significant overcalling although generally the number of overcalls was not particularly high.

Most of the cracks in the mock-up are deep as determined by the application of the multiparameter algorithm. The uncertainty in depth and the skewing toward deeper cracks is accounted for in the confidence limits associated with POD curves.

3.1 Bobbin Coil Results

Estimates of maximum depth from crack profiles and false call rates were used to establish POD as a function of crack depth and m_p and to generate logistic curve fits to the data. The NDE uncertainty in depth is included in the one sided 95% lower confidence limit (OSL). In general, the curves have a reasonable shape and thus provide plausible PODs (increasing POD with increasing depth). As expected, the POD for TSP ID cracks is higher than for OD cracks (99% with 98% OSL at 60% TW vs. 75% with 65% OSL at 60% TW). While as expected, the POD for freespan LODSCC (95% at 60% TW) is higher than the POD for TSP LODSCC (75% at 65% TW), it is lower than the POD for TSP LIDSCC (98% at 60% TW). The logistic fit when depths are estimated by ANL's multiparameter algorithm were compared with the fit when the +Point maximum depth estimates are used. Use of the +Point data results in a more conservative POD curve.

In addition to examination of the RR data as a function of flaw depth, the POD has been evaluated as a function of BC voltage for TSP LODSCC. A pattern similar to that found for POD versus depth is observed for the POD vs. TSP bobbin coil voltage. In this case (POD vs. voltage), the POD curve for LIDSCC at the TSP is lower than that for LODSCC. The lower POD curve for LIDSCC vs. POD for LODSCC, when POD is plotted against voltage, is possibly the result of missing shallow cracks that are in dents with high voltages.

The results were analyzed by team to determine whether there were strong team-to-team variations in the POD. The performances of most of the teams cluster rather tightly, although in some cases there is a significant variation between best and worst. The probability that team-to-team variations in logistic fits to data are due to chance can be estimated. For LIDSCC at the TSP, the variation from best to worst is very significant statistically. There is <0.1% probability that the difference is due to chance (DTC). For FS OD, the variation from best to worst is probably significant (DTC is <20%). For TSP OD, the probability that the variation from best to worst is DTC > 60% and thus the variation is probably not significant.

3.2 Tube Sheet MRPC Results

The POD for SCC in the tube sheet level of the mock-up with an MRPC has been calculated. The maximum-likelihood logistic fit as a function of depth is presented in this report. For all TS POD curves, a false call rate of 6% was used. One-sided 95% OSLs that included uncertainties in maximum depth were also presented.

For MRPC in the tube sheet, the POD for IDSCC is $\approx 90\%$, with an OSL of $\approx 75\%$. The highest POD curve is for LIDSCC where the POD at 60% TW is 95%. MRPC POD by team was presented for axial and circumferential, IDSCC, and ODSCC in the tube sheet. The POD at 60% TW ranges from 90 to 70%.

Comparisons were made between the tube sheet BC POD and tube sheet MRPC POD. For all SCC, there is a higher POD curve for the MRPC (80 vs. 40% at 60% TW). For tube sheet LIDSCC only, the MPRC POD at 60% TW is 95%, while the BC POD is only 40%. For the tube sheet, the MPRC is clearly the probe of choice for detection of SCC. The complication of the roll transition and the presence of circumferential SCC make separating the crack signals from geometry difficult when using a bobbin coil.

3.3 MRPC Analysis of TSP Signals.

A review of MRPC results for BC voltage between 2.0 and 5.6 was carried out. Such calls are normally reviewed to confirm or dismiss the BC flaw call. The result for LODSCC >74% TW is an average correct call of 98%. All teams missed an LODSCC at the TSP with an estimated maximum depth of 28% TW. There is a possibility of having a strong BC signal and a weak MRPC signal that would not be called a crack by analysts. The example presented had an estimated maximum depth of 99% TW with only a few tenths of a volt generated by the +Point coil at 300 kHz. This situation could arise when a flaw is shallow and long or shallow and volumetric in nature or short and tight.

3.4 Accuracy of Maximum Depth for Mock-Up Cracks

Accuracy in estimating the maximum depth of cracks in the mock-up was determined from a comparison of crack profiles generated by using ANL's multiparameter algorithm with profiles determined from fractography. The overall RMSE for all cracks of all depths is 15.1%, but there is a significant variation in the RMSE with depth. The RMSE value is significantly better for 80–100% TW cracks than for cracks with other depths.

In Table 2.3, two sets of RMSE values are given. One set is based on the values obtained directly from the multiparameter algorithm and the other on "corrected" values obtained from the regression fit shown in Fig. 2.41. For the shallowest cracks, the "corrected" values give a significantly lower RMSE value, but when all the data are considered the differences in the RMSE for corrected and uncorrected predictions are small. This indicates that there is little systematic bias in the predictions of the multiparameter algorithm, i.e., the errors are random.

These sizing-accuracy results can be used to estimate the uncertainty in POD curves if the multiparameter algorithm is used to determine the "true" state of the mock-up for the NDE round-robin. Instead of characterizing the error in the depths in terms of the overall average for all depths ($\approx 15\%$), the error was taken as a function of depth. Analytically, the values of RMSE given in Table 2.3 are assumed to apply at the midpoint of the depth range for each bin. The error at other depths is then estimated by linear interpolation of these values.

3.5 Overall Capability

The detection capability of current in service inspection (ISI) technology and procedures has been assessed by carrying out an eddy current round-robin (RR) exercise with a steam generator tube bundle mock-up. Inspection of the mock-up and analysis of the data mimicked industry ISI practices conducted on operating steam generators. All documentation for conducting the inspection was prepared with input from an industry-based NDE Task Group, and the realism of the mock-up was established. Data were acquired in June and August 1999 and analysis of the data by 11 commercial teams was completed in December 2000. Each team consisted of five qualified analysts. The exercise took seven to eight working days per team.

The conclusion from the analysis of round-robin results is that good POD can be achieved for deep flaws when commercial techniques are used in a similar manner to that of the RR exercise. The level of success in detection of SCC did vary with flaw location. Estimates of maximum depth from eddy current crack profiles and false call rates were used to establish POD as a function of depth and m_p . Logistic fits to the data were generated. The BC POD for TSP ID cracks is higher than for OD cracks (99% with 98% OSL at 60% TW vs. 75% with 65% OSL at 60% TW). The BC POD for freespan LODSCC is $\approx 95\%$ at 60% TW. For MRPC in the tube sheet, the POD for IDSCC is $\approx 90\%$ with an OSL of $\approx 75\%$. The highest POD curve is for LIDSCC where the POD at 60% TW is 95%. A review of MRPC results for BC voltage between 2.0 and 5.6 was carried out. Such calls are normally reviewed to confirm or dismiss the BC flaw call. The result, for LODSCC $> 74\%$ TW is an average correct call of 98%. All teams missed an LODSCC at the TSP with an estimated maximum depth of 28% TW. There is a possibility of having a deep crack with a weak MRPC signal that would not be called a crack by analysts. The example presented had an estimated maximum depth of 99% TW with only a few tenths of a volt generated by the +Point coil at 300 kHz.

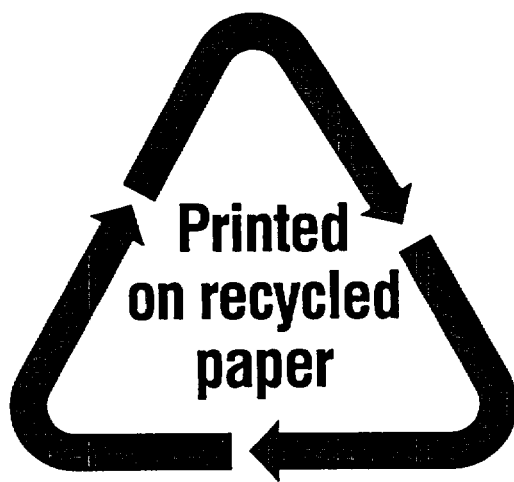
No useful correlation was found between signal amplitude or phase and the maximum depth of the mock-up flaws. When the PODs are considered as a function of m_p , it is found that in the TSP and FS regions the POD for cracks that would fail or leak under $3\Delta p$ internal pressure (corresponding to $m_p \approx 2.3$) is >95% even when uncertainties are accounted for.

The adequacy of the multiparameter algorithm for obtaining profiles and maximum depth was established. The results of POD as a function of depth or m_p were based on the profiles generated with the multiparameter algorithm.

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11. ABSTRACT <i>(200 words or less)</i> This report presents an independent assessment of steam generator (SG) inspection reliability that was developed through a nondestructive evaluation round-robin on a steam generator mock-up at Argonne National Laboratory (ANL). The report does not establish regulatory position. The purpose of the round-robin was to assess the current state of SG tubing in-service inspection reliability, determine the probability of detection (POD) as function of flaw size or severity, and to assess the capability for sizing of flaws. Eleven teams participated in analyzing bobbin and rotating coil mock-up data collected by qualified industry personnel. The mock-up contains hundreds of cracks and simulations of artifacts such as corrosion deposits and tube support plates that make detection and characterization of cracks more difficult in operating steam generators than in most laboratory situations. An expert Task Group from industry, Argonne National Laboratory, and the NRC have reviewed the signals from the laboratory-grown cracks used in the mock-up to ensure that they provide reasonable simulations of those obtained in the field. The number of tubes inspected and the number of teams participating in the round-robin are intended to provide better statistical data on the POD and characterization accuracy than is currently available EPRI qualification programs.						
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